

LOSSES AND EFFICIENCIES OF TRANSFORMERS

by

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2. Pender's Handbook for Electrical Engineers,  
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5. J. E. Crowder's Thesis.



## INTRODUCTION

This Thesis was written to show the losses of a home build transformer as compared to a factory built transformer. The home built transformer was built by J. E. Crowder in 1927. The factory built transformer was built by Westinghouse Electric & Manufacturing Company, and is an old model which has recently been junked by the Knoxville Power & Light Company, because of new design and construction in transformers which make this type obsolete. The home built transformer was designed for a 3 K.V.-A. capacity and voltage ratio of 1 to 2. The primary voltage is 110 and the secondary 220. Four coils were used.

The factory built transformer is a  $2\frac{1}{2}$  K V.-A capacity with voltage ratio of 10 to 1. It has four coils giving the voltage ratios of 2200 to 220 or 1100 to 110 volts. Frequency of 50 - 140 cycles per second.



# HIGH POTENTIAL COILS

## HOME BUILT

220 Volts

3 K V.-A.

$$\text{Current} = \frac{3000}{220} = 13.6 \text{ Amps.}$$

## FACTORY BUILT

1,100 Volts

2.5 K V.-A.

$$\text{Current} = \frac{2500}{1100} = 2.28 \text{ Amps.}$$

# LOW POTENTIAL COILS

110 Volts

$$\text{Current} = \frac{3000}{110} = 27.2 \text{ Amps.}$$

110 Volts

$$\text{Current} = \frac{2500}{110} = 22.8 \text{ Amps.}$$

## CORE

$$E = \sqrt{2} \pi N \phi 10^{-8}$$

$$\phi = \frac{E \times 10^8}{\sqrt{2} \pi \times N}$$

$$\text{Flux} = \frac{110 \times 10^8}{4.44 \times 110} = 380,000$$

$$\text{Flux density} = 60,000$$

$$380,000 \div 60,000 = 6.3 \text{ sq." Core Area.}$$



LOSSES AT FULL LOAD

$$I^2R$$

HOME BUILT

$$\text{Primary } R = .07 \text{ ohm}$$

$$\text{Primary } I^2R = (27.2)^2 \times .07 = 51 \text{ Watts}$$

$$\text{Secondary } R = .51 \text{ ohms}$$

$$\text{Secondary } I^2R = (13.6)^2 \times .51 = 94 \text{ Watts}$$

$$\text{Total } I^2R \text{ Losses}$$

$$51 + 94 = 145 \text{ Watts}$$

$$\text{Percent Loss} = \frac{145 \times 100}{3000} = 4.88$$

FACTORY BUILT

$$\text{Primary } R = .054 \text{ ohms}$$

$$\text{Primary } (I)^2R = (22.8)^2 \times .054 = 28.1$$

$$\text{Secondary } R = 4.67 \text{ ohms}$$

$$\text{Secondary } I^2R = (22.8)^2 \times .054 = 28.1$$

$$\text{Total } I^2R \text{ Losses}$$

$$28.1 + 24.2 = 52.3$$

$$\text{Percent Loss} = \frac{52.3 \times 100}{2500} = 2.1$$

CORE LOSS

$$\text{Total Core Loss}$$

$$= 135 \text{ Watts}$$

$$135 - 35 = 100 \text{ Watts}$$

$$\text{Total Core Loss}$$

$$= 35 \text{ Watts}$$



EFFICIENCY, CORE LOSS CONSTANT

HOME BUILT

FACTORY BUILT

1/4 Load

$$\text{Secondary } I^2R = 3 \text{ Watts}$$

$$\text{Primary } I^2R = 6$$

$$\text{Core Loss} = 135$$

$$\text{Total Loss} = 144 \text{ Watts}$$

$$\text{Eff. } \frac{750}{750 + 144} = 84.1\%$$

$$\text{Secondary } I^2R = 1.50 \text{ Watts}$$

$$\text{Primary } I^2R = 1.35$$

$$\text{Core Loss} = 35.00$$

$$\text{Total Loss} = 37.85$$

$$\text{Eff. } \frac{625}{625 + 37.85} = 94.5\%$$

1/2 Load

$$\text{Secondary } I^2R = 12$$

$$\text{Primary } I^2R = 24$$

$$\text{Core Loss} = 135$$

$$\text{Total Loss} = 171$$

$$\text{Eff. } \frac{1500}{1500 + 171} = 90\%$$

$$\text{Secondary } I^2R = 6.00$$

$$\text{Primary } I^2R = 7.45$$

$$\text{Core Loss} = 35.00$$

$$\text{Total Loss} = 48.45$$

$$\text{Eff. } \frac{1250}{1250 + 48.45} = 96.3\%$$

3/4 Load

$$\text{Primary } I^2R = 29$$

$$\text{Secondary } I^2R = 53$$

$$\text{Core Loss} = 135$$

$$\text{Total Loss} = 217$$

$$\text{Eff. } \frac{2250}{2250 + 217} = 91\%$$

$$\text{Primary } I^2R = 15.60$$

$$\text{Secondary } I^2R = 13.60$$

$$\text{Core Loss} = 35.00$$

$$\text{Total Loss} = 64.20$$

$$\text{Eff. } \frac{1875}{1875 + 64.20} = 96.9\%$$



EFFICIENCY TEST (CONTINUED)

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HOME BUILT

Full Load

$$\text{Primary } I^2R = 51$$

$$\text{Secondary } I^2R = 94$$

$$\text{Core Loss} = \underline{135}$$

$$\text{Total Loss} = 280 \text{ Watts}$$

$$\text{Eff. } \frac{3000}{3000 + 280} = 91.4\%$$

FACTORY BUILT

$$\text{Primary } I^2R = 28.1$$

$$\text{Secondary } I^2R = 24.2$$

$$\text{Core Loss} = \underline{35.0}$$

$$\text{Total Loss} = 87.3 \text{ Watts}$$

$$\text{Eff. } \frac{2500}{2500 + 87.3} = 96.8\%$$

1/8 Load

$$\text{Secondary } I^2R = 0.38$$

$$\text{Primary } I^2R = 0.43$$

$$\text{Core Loss} = \underline{35.00}$$

$$\text{Total Loss} = 35.81 \text{ Watts}$$

$$\text{Eff. } \frac{312}{312 + 35.81} = 90.6\%$$

5/8 Load

$$\text{Secondary } I^2R = 9.5$$

$$\text{Primary } I^2R = 10.82$$

$$\text{Core Loss} = \underline{35.00}$$

$$\text{Total Loss} = 55.32 \text{ Watts}$$

$$\text{Eff. } \frac{1564}{1564 + 55.32} = 96.5\%$$

7/8 Load

$$\text{Secondary } I^2R = 18.5$$

$$\text{Primary } I^2R = 21.3$$

$$\text{Core Loss} = \underline{35.0}$$

$$\text{Total Loss} = 74.8 \text{ Watts}$$

$$\text{Eff. } \frac{2186}{2186 + 74.8} = 96.8\%$$



EFFICIENCY TEST

| <u>E</u> | <u>I</u> | <u>P</u> | <u>E<sub>2</sub></u> | <u>I<sub>2</sub></u> | <u>P<sub>2</sub></u> | <u>Eff.</u> |
|----------|----------|----------|----------------------|----------------------|----------------------|-------------|
| 111      | 12.5     | 350      | 231                  | 0                    | 0                    | 0           |
| 109.5    | 13.2     | 1080     | 225                  | 1.7                  | 750                  | 69.5        |
| 108      | 16.5     | 1530     | 221                  | 2.6                  | 1150                 | 75          |
| 107.5    | 17.5     | 1600     | 220                  | 2.73                 | 1200                 | 75          |
| 107      | 18.5     | 1700     | 219                  | 2.9                  | 1260                 | 74          |
| 106.5    | 18.8     | 1750     | 219                  | 3.1                  | 1360                 | 77.5        |
| 105.5    | 16.8     | 2080     | 216                  | 3.97                 | 1750                 | 84          |
| 106.5    | 15.6     | 2130     | 217                  | 4.2                  | 1840                 | 86.4        |
| 106.5    | 15.8     | 2240     | 217                  | 4.4                  | 1940                 | 86.6        |
| 105.5    | 16.4     | 2480     | 215                  | 5                    | 2150                 | 87          |
| 105      | 17.5     | 2870     | 211                  | 6                    | 2600                 | 90.5        |
| 104      | 18.2     | 3200     | 210                  | 6.8                  | 2950                 | 92.5        |
| 103.5    | 18.9     | 3450     | 208                  | 7.4                  | 3180                 | 92.4        |
| 103.3    | 20.7     | 3520     | 206                  | 8                    | 3250                 | 92.4        |
| 102.5    | 22.4     | 3940     | 203                  | 9.15                 | 3650                 | 92.7        |
| 101      | 25.5     | 4650     | 198                  | 10.1                 | 4250                 | 91.5        |
| 100      | 27       | 5000     | 196                  | 11                   | 4650                 | 93          |
| 102      | 22.1     | 3800     | 204                  | 9                    | 3570                 | 94          |
| 100.5    | 24.5     | 4350     | 199                  | 10.5                 | 4080                 | 93.5        |
| 100      | 25.8     | 4600     | 198                  | 11                   | 4300                 | 93.5        |
| 97.5     | 29.5     | 5300     | 185                  | 13                   | 4950                 | 91.5        |
| 97       | 31.3     | 5550     | 189                  | 13.7                 | 5190                 | 93.5        |
| 96       | 32.4     | 5000     | 186                  | 14.5                 | 5450                 | 94          |
| 95       | 33.5     | 6050     | 184                  | 15.1                 | 5550                 | 92          |
| 94       | 35.4     | 6300     | 180                  | 16.1                 | 5900                 | 94          |



(Efficiency Test Continued)

| <u>E</u> | <u>I</u> | <u>P</u> | <u>E</u> <sub>2</sub> | <u>I</u> <sub>2</sub> | <u>P</u> <sub>2</sub> | <u>Eff.</u> |
|----------|----------|----------|-----------------------|-----------------------|-----------------------|-------------|
| 93.5     | 36.5     | 6450     | 178                   | 16.6                  | 6000                  | 93          |
| 92       | 38.3     | 6750     | 174                   | 17.6                  | 6220                  | 92.3        |
| 90.5     | 41.9     | 7400     | 168                   | 19.5                  | 6600                  | 89          |



HEAT TEST

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Home Built Transformer

Load 3000 Watts

| Temp. (cent.) | Time (Min.) |
|---------------|-------------|
| 28            | 0           |
| 31            | 10          |
| 37.5          | 20          |
| 43            | 30          |
| 48            | 40          |
| 52            | 50          |
| 56            | 60          |
| 59            | 70          |
| 62            | 80          |
| 64.5          | 90          |
| 68            | 100         |
| 70            | 110         |
| 72.5          | 120         |
| 75            | 130         |
| 77            | 140         |
| 78.5          | 150         |
| 79            | 155         |



RESISTANCE MEASUREMENTS

HOME BUILT

Primary

| <u>E</u> | <u>I</u> | <u>R</u> |
|----------|----------|----------|
| .5       | 7        | .071     |
| 1.1      | 15.3     | .072     |
| 1.6      | 21.5     | .074     |
| 1.9      | 26       | .073     |

Mean R = .073 ohms

Secondary

| <u>E</u> | <u>I</u> | <u>R</u> |
|----------|----------|----------|
| 2.05     | 3.5      | .585     |
| 2.95     | 5        | .590     |
| 3.9      | 6.5      | .600     |
| 4.9      | 8.5      | .585     |

Mean R = .589 ohms

FACTORY BUILT

| <u>E</u> | <u>I</u> | <u>R</u> |
|----------|----------|----------|
| .3       | 5.5      | .054     |
| .9       | 16       | .056     |
| 1.5      | 27.3     | .055     |
| 2.0      | 37       | .054     |

Mean R = .054 ohms

| <u>E</u> | <u>I</u> | <u>R</u> |
|----------|----------|----------|
| 12.5     | 2.6      | 4.65     |
| 14.5     | 3.2      | 4.54     |
| 22.0     | 4.7      | 4.68     |
| 24.0     | 5.0      | 4.80     |

Mean R = 4.67 ohms



REGULATIONHOME BUILT

Full Load

$$E_1 = 93.5$$

$$E_2 = 178$$

$$E_1^0 = 112$$

$$112 - 93.5 = 28.5$$

$$E_2^0 = 232$$

$$28.5 \div 112 = .248$$

$$178 \times 1.248 = 222 \text{ corrected}$$

Value of  $E_2$ 

$$\text{Reg.} = \frac{232 - 222}{232} \times 100 = 4.3\%$$

 $\frac{3}{4}$  Full Load

$$E_1 = 100.5 \quad E_2 = 199$$

$$112 - 100.5 = 11.5$$

$$11.5 \div 112 = .103$$

$$199 \times 1.103 = 220$$

$$\text{Reg.} = \frac{232 - 220}{232} \times 100 = 5.17\%$$

 $\frac{1}{4}$  Full Load

$$E_1 = 88 \quad E_2 = 160$$

$$112 - 88 = 24 \text{ volts}$$

$$24 \div 112 = .214$$

$$160 \times 1.214 = 194$$

$$\text{Reg.} = \frac{232 - 194}{232} \times 100 = 16.4\%$$



# REGULATION

## FACTORY BUILT

| Full Load | I    | E   | W   |
|-----------|------|-----|-----|
|           | 2.27 | 128 | 245 |

$$\text{Equiv. } R = \frac{P}{I^2} = \frac{245}{(2.27)^2} = 47.6 \text{ ohms}$$

$$E_R = IR = 2.27 \times 47.6 = 108 \text{ volts}$$

$$\begin{aligned} \text{Equiv. } X_L &= \sqrt{(EI)^2 - (R I)^2} = \sqrt{(128)^2 - (108)^2} \\ &= 21.2 \text{ volts} \end{aligned}$$

$$\begin{aligned} \text{N.L. Voltage } E &= \sqrt{(2308)^2 + (21.2)^2} \\ &= 2310 \end{aligned}$$

$$\text{Reg.} = \frac{2310 - 2200}{2200} \times 100 = 5.0\%$$

| $\frac{3}{4}$ Full Load | I    | E   | W   |
|-------------------------|------|-----|-----|
|                         | 1.71 | 106 | 155 |

$$\text{Equiv. } R = \frac{P}{I^2} = \frac{155}{(1.71)^2} = 55 \text{ ohms}$$

$$E_R = IR = 1.71 \times 55 = 94 \text{ volts}$$

$$\begin{aligned} \text{Equiv. } X_L &= \sqrt{(106)^2 - (94)^2} \\ &= 41.8 \text{ volts} \\ \text{N.L. Voltage } E &= \sqrt{(2294)^2 + (41.8)^2} \\ &= 2298 \end{aligned}$$

$$\text{Reg.} = \frac{2298 - 2200}{2200} \times 100 = 4.46\%$$



| $\frac{1}{2}$ Full Load | I    | E   | W   |
|-------------------------|------|-----|-----|
|                         | 1.14 | 108 | 108 |

$$\text{Equiv. } R = \frac{P}{I^2} = \frac{108}{(1.14)^2} = 83 \text{ ohms}$$

$$E_R = IR = 1.14 \times 83 = 94.5 \text{ volts}$$

$$\begin{aligned} \text{Equiv. } XI &= \sqrt{(108)^2 - (94.5)^2} \\ &= 43.8 \text{ volts} \end{aligned}$$

$$\begin{aligned} \text{N.L. Voltage } E &= \sqrt{(2294)^2 + (43.8)^2} \\ &= 2299 \end{aligned}$$

$$\text{Reg.} = \frac{2299 - 2200}{2200} \times 100 = 4.5\%$$

| $1\frac{1}{4}$ Full Load | I    | E   | W   |
|--------------------------|------|-----|-----|
|                          | 2.85 | 142 | 332 |

$$\text{Equiv. } R = \frac{P_2}{I^2} = \frac{332}{(2.85)^2} = 41 \text{ ohms}$$

$$E_R = IR = 2.85 \times 41 = 115 \text{ Volts}$$

$$\begin{aligned} \text{Equiv. } XI &= \sqrt{(142)^2 - (115)^2} \\ &= 82.5 \text{ volts} \end{aligned}$$

$$\begin{aligned} \text{N.L. Voltage } E &= \sqrt{(2315)^2 + (82.5)^2} \\ &= 2319 \end{aligned}$$

$$\text{Reg.} = \frac{2319 - 2200}{2200} \times 100 = 5.4\%$$



CALIBRATION OF VOLTMETER (STD.)

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| <u>Voltmeter</u> | <u>Potentiometer</u> | <u>Error</u> |
|------------------|----------------------|--------------|
| 0                | 0                    | 0            |
| .10              | 0.10094              | 0.00094      |
| .20              | 0.20086              | 0.00086      |
| .30              | 0.30200              | 0.00200      |
| .40              | 0.40184              | 0.00184      |
| .50              | 0.50266              | 0.00266      |
| .60              | 0.60334              | 0.00334      |
| .70              | 0.70250              | 0.00250      |
| .80              | 0.80100              | 0.00100      |
| .90              | 0.90294              | 0.00294      |
| 1.00             | 1.00254              | 0.00254      |
| 1.10             | 1.10443              | 0.00443      |
| 1.20             | 1.20350              | 0.00350      |

CALIBRATION VOLTMETER

| <u>Std.</u> | <u>Voltmeter</u> | <u>Ave.</u> | <u>Error</u> |
|-------------|------------------|-------------|--------------|
| 30          | 26 - 30          | 28          | 2            |
| 40          | 38 - 40          | 39          | 1            |
| 50          | 48 - 52          | 50          | 0            |
| 60          | 49 - 61          | 60          | 0            |
| 70          | 70 - 71.2        | 70.6        | - .6         |
| 80          | 79.2 - 80.2      | 89.7        | .3           |
| 90          | 89.8 - 90.4      | 90.1        | - .1         |
| 100         | 100.8 - 100.5    | 100.6       | - .6         |
| 110         | 111.7 - 110      | 110.8       | - .8         |
| 120         | 120 - 122        | 121         | - 1.         |



CALIBRATION OF WATTMETER

| <u>Rev. S</u> | <u><math>\frac{W}{M}</math></u> | <u>T</u> | <u><math>\frac{W}{S}</math></u> | <u>Error</u> |
|---------------|---------------------------------|----------|---------------------------------|--------------|
| 4.88          | 98                              | 60 Sec.  | 97.0                            | -1           |
| 5.82          | 100                             | 60       | 99.0                            | -1           |
| 9.9           | 195                             | 60       | 191.0                           | -4           |
| 13.04         | 290                             | 60       | 291.0                           | -1           |
| 15.54         | 370                             | 60       | 371.2                           | -1.2         |
| 16.8          | 400                             | 60       | 401.1                           | 1.1          |
| 23.13         | 455                             | 60       | 456                             | -1           |
| 23.17         | 460                             | 60       | 461                             | -1           |



CALIBRATION OF AMMETER

| <u>W</u> | <u>E</u> | <u>I<sub>M</sub></u> | <u>I<sub>M</sub></u> | <u>Ave.</u> | <u>I<sub>C</sub></u> | <u>Error</u> |
|----------|----------|----------------------|----------------------|-------------|----------------------|--------------|
| 40       | 114      | .4                   | .42                  | .41         | .352                 | -.05         |
| 60       | 114      | .6                   | .58                  | .59         | .525                 | -.06         |
| 87       | 114      | .8                   | .82                  | .81         | .764                 | -.04         |
| 107      | 114      | 1.0                  | .98                  | .99         | .94                  | -.05         |
| 134      | 116      | 1.2                  | 1.23                 | 1.2         | 1.16                 | -.04         |
| 153      | 116      | 1.4                  | 1.37                 | 1.39        | 1.32                 | -.07         |
| 180      | 117      | 1.6                  | 1.59                 | 1.6         | 1.59                 | -.01         |
| 202      | 117      | 1.8                  | 1.78                 | 1.79        | 1.73                 | -.06         |
| 223      | 117      | 2.0                  | 1.98                 | 1.99        | 1.91                 | -.08         |



### CONCLUSION

From this thesis we see that the factory built transformer has a much better efficiency and regulation, for all loads, than the home built one has. The efficiencies range from five to nine percent better, while the regulation ranges from one to four percent better.

The  $I^2R$  losses at full load, are twice as high in the home built transformer. And the core losses for the transformers show a difference of one hundred watts in favor of the factory built one.

This comparison gives an idea of what has been gained, in transformer design and construction by years of study and construction, up to the time of this transformer. Since that <sup>time</sup> newer points of design and construction have been worked out, and today they are able to build transformers of even better efficiency and regulation than was shown in this thesis.



APPROVAL

The foregoing thesis is hereby approved as a credit-  
able study of an engineering subject, carried out and presented  
in a manner sufficiently satisfactory to warrent its acceptance  
as a prerequisite to the degree for which it has been submitted.  
It is to be understood that by this approval the undersigned  
does not necessarily endorse or approve any statement made,  
opinions expressed, or conclusions drawn therein, but approves  
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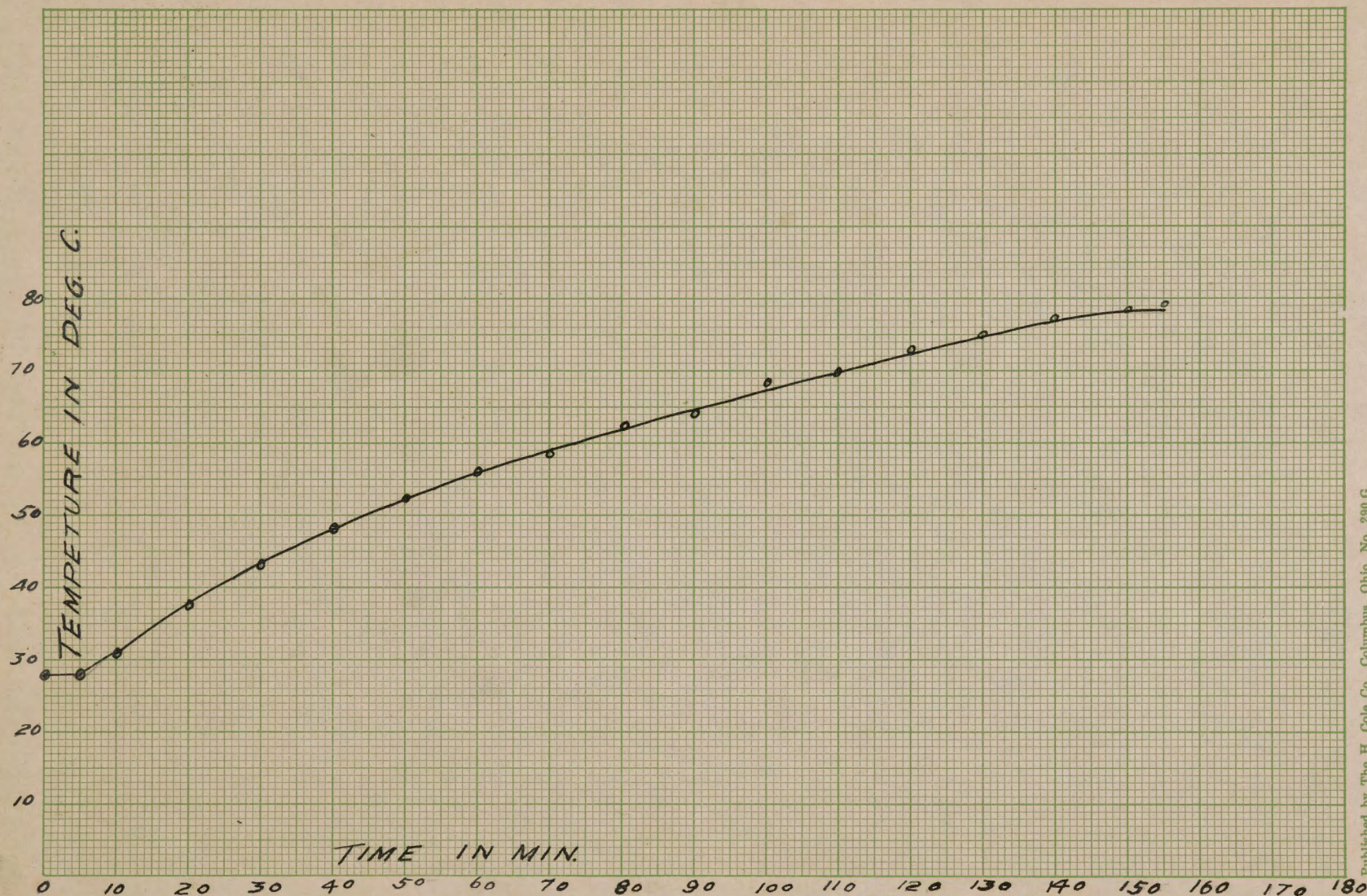
Name

Chas A Perkins

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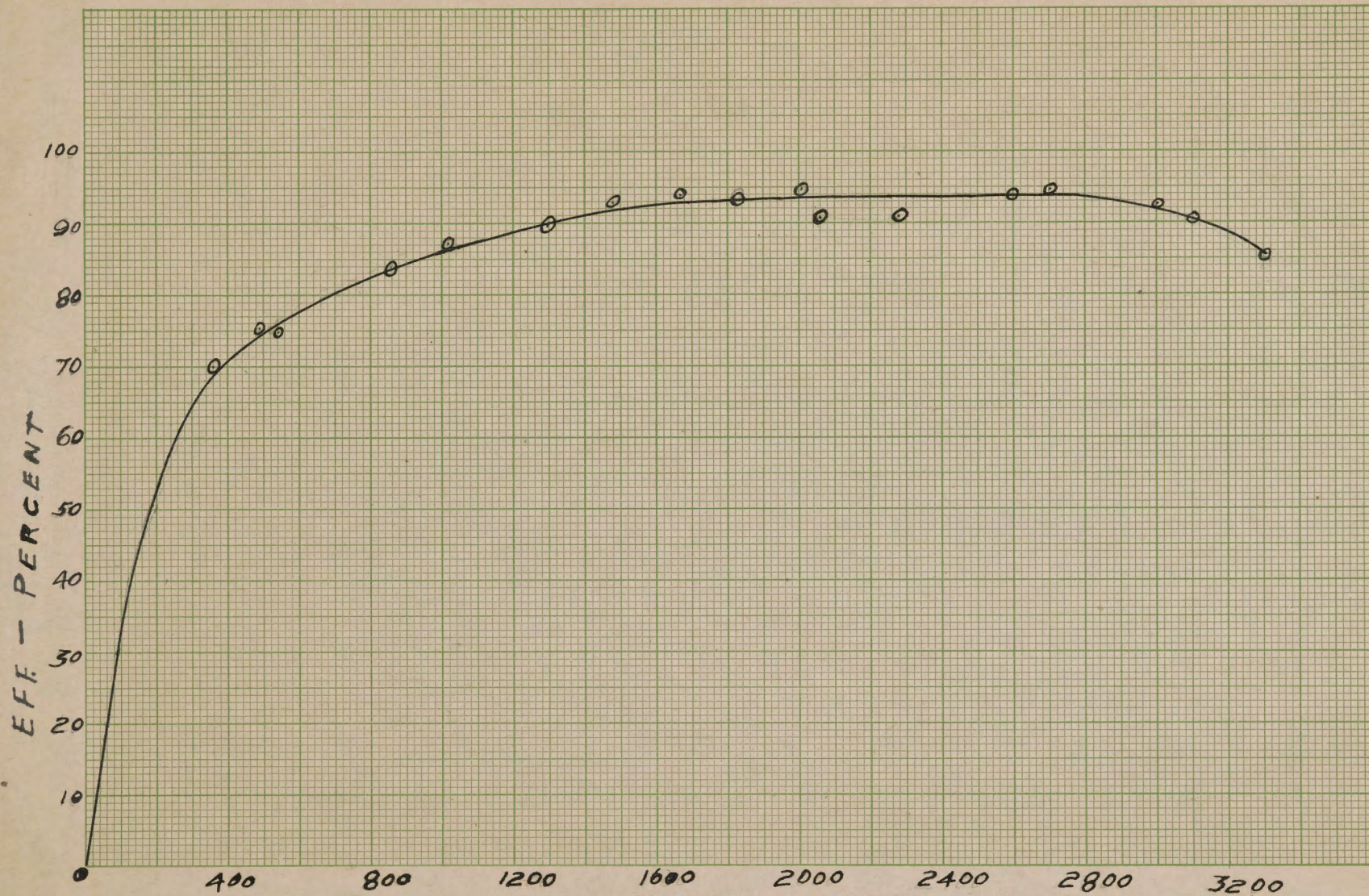
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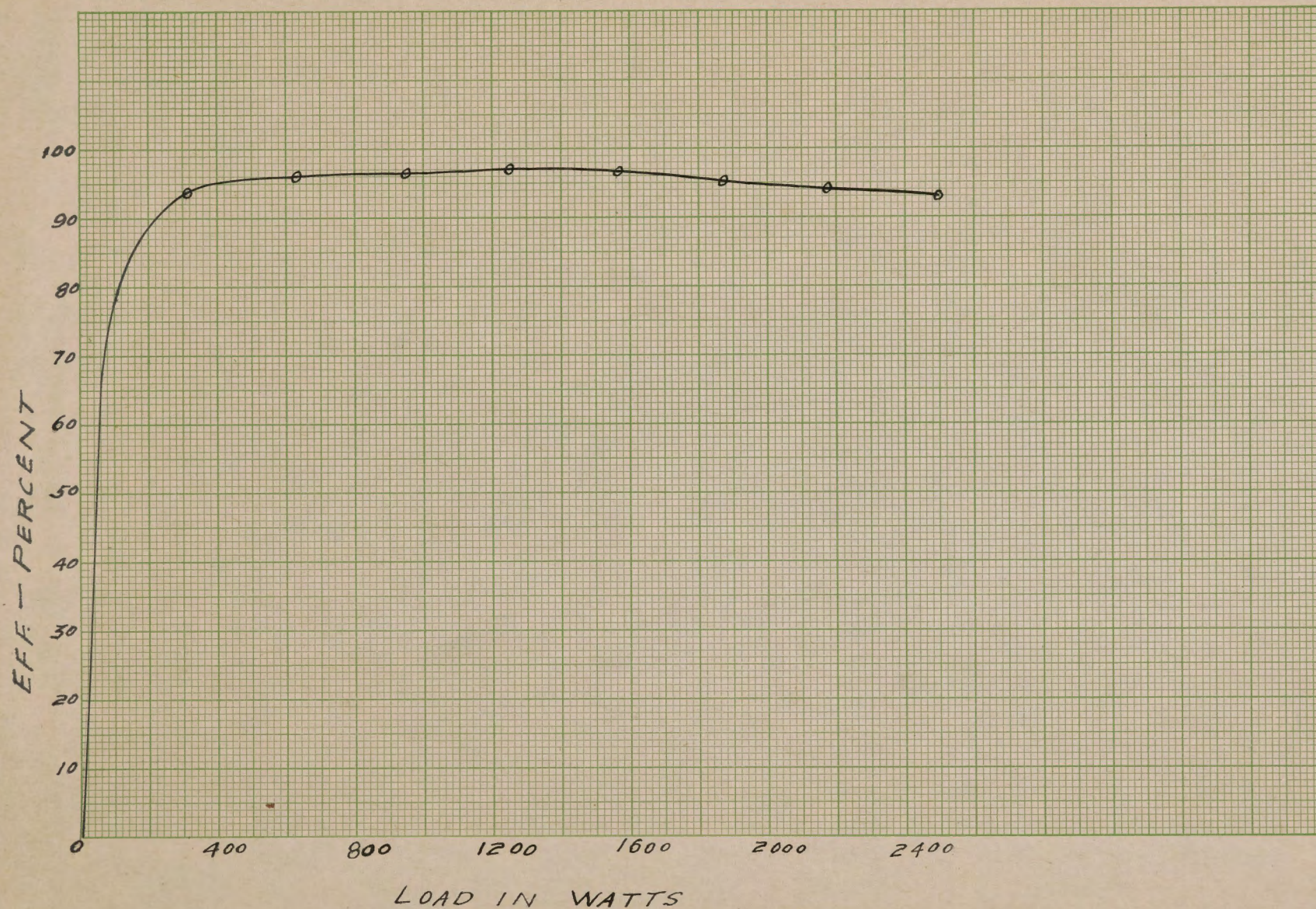
HEAT TEST FOR HOME BUILT TRANSFORMER





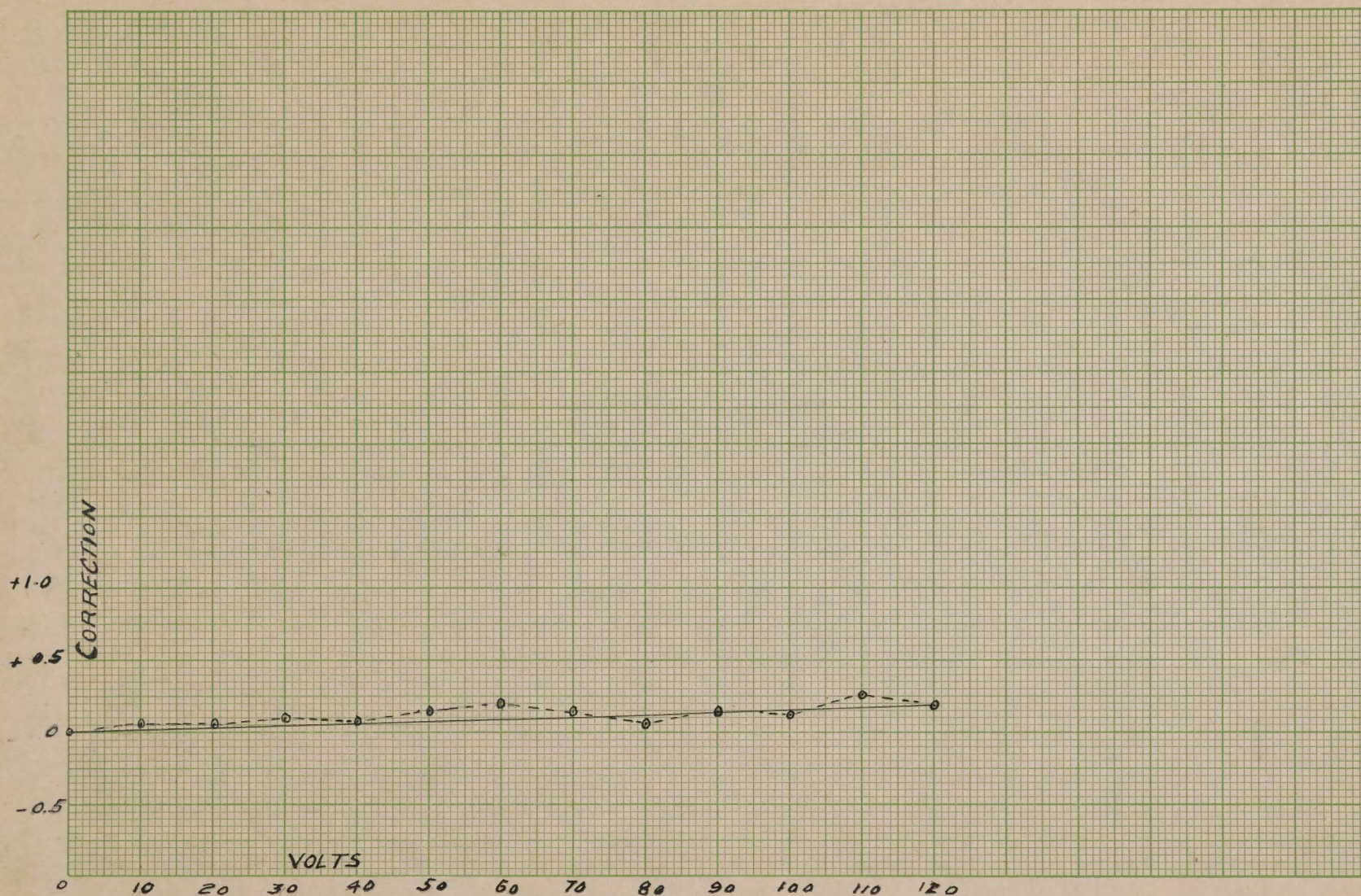
LOAD IN WATTS  
HOME BUILT TRANSFORMER





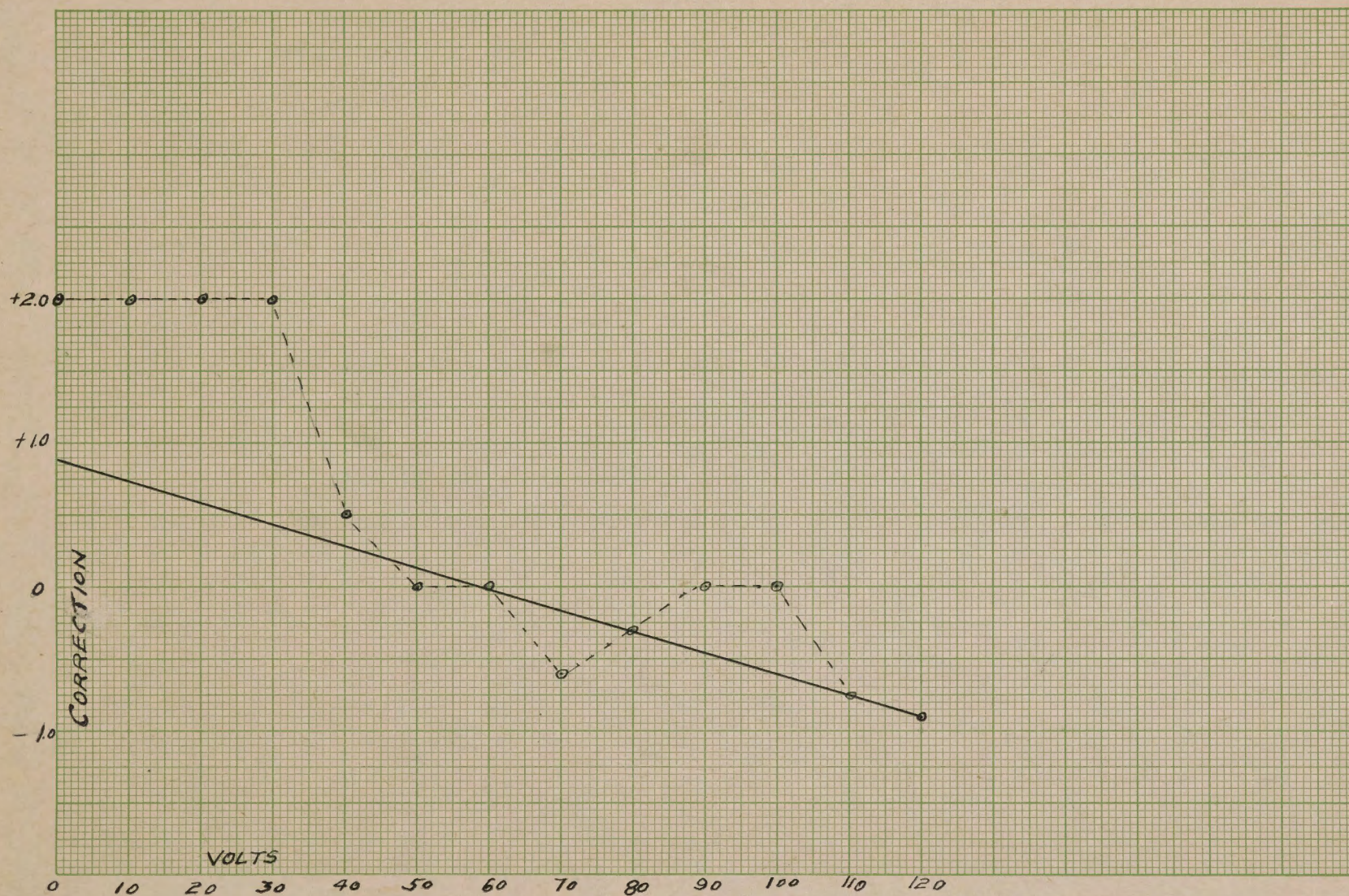
FACTORY BUILT TRANSFORMER





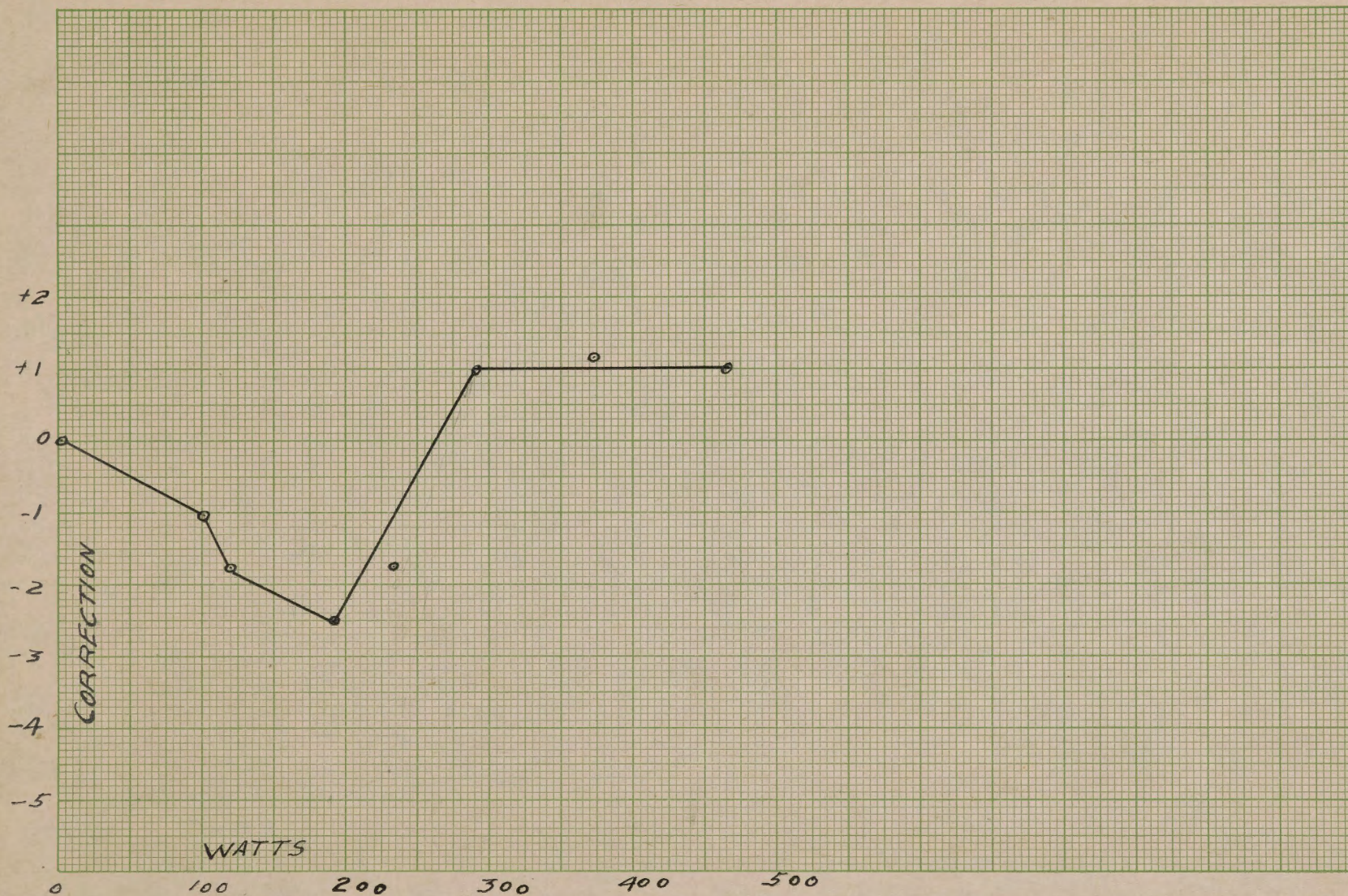
CALIBRATION CURVE FOR STANDARD VOLTMETER





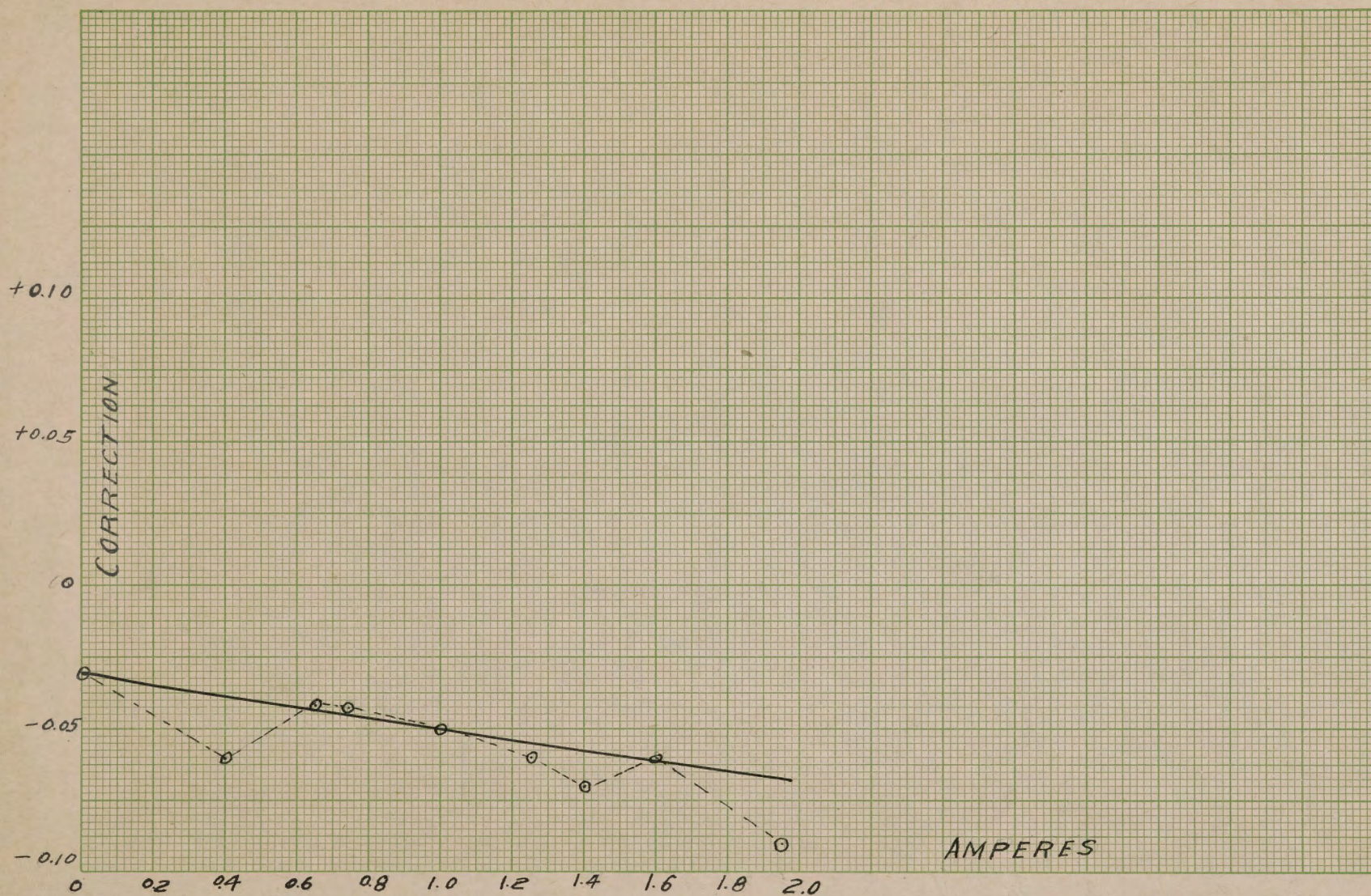
CALIBRATION CURVE FOR THOMPSON A-C VOLTMETER #3





CALIBRATION CURVE FOR G.E. WATTMETER #14





CALIBRATION CURVE FOR AMMETER #7 0-2 A-C