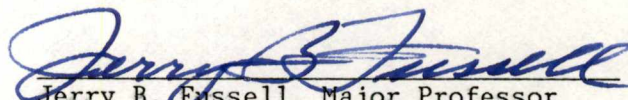
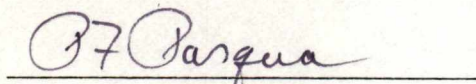
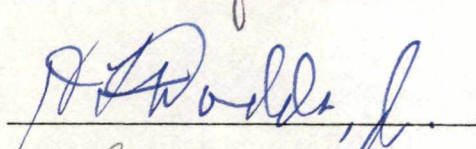
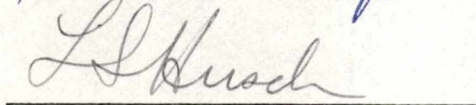


To the Graduate Council:

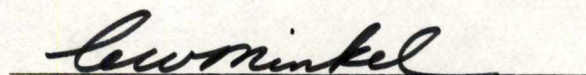
I am submitting herewith a dissertation written by Henrique Martini Paula entitled "A Methodology for Time-Dependent Reliability Analysis of Accident Sequences and Complex Reactor Systems." I have examined the final copy of this dissertation for form and content and recommend that it be accepted in partial fulfillment of the requirements for the degree of Doctor of Philosophy, with a major in Nuclear Engineering.


Jerry B. Fussell, Major Professor

We have read this dissertation
and recommend its acceptance:

Accepted for the Council:


The Graduate School

A METHODOLOGY FOR TIME-DEPENDENT RELIABILITY
ANALYSIS OF ACCIDENT SEQUENCES AND
COMPLEX REACTOR SYSTEMS

A Dissertation
Presented for the
Doctor of Philosophy
Degree
The University of Tennessee, Knoxville

Henrique Martini Paula

December 1984

I dedicate this work to my wife Célia, our daughters Daniela and Larissa, and to my late father Camilo.

ACKNOWLEDGMENTS

In the course of this dissertation research, a number of scholars have assisted me generously. I am particularly indebted to my Professor Advisor Jerry Bernard Fussell for his consultation and criticism. I extend my sincere appreciation to Professors P. F. Pasqua (head of the department of nuclear engineering), H. L. Dodds, and L. S. Husch, all from the University of Tennessee. I am also indebted to Dr. Jussi K. Vaurio, from the Argonne National Laboratory, for his consultation. Although the participation of these scholars has improved the quality of this dissertation research, they share no responsibility for whatever errors remain in my work. I also express my gratitude for the support of Professor Pedro Bento de Camargo, from the "Instituto de Pesquisas Energéticas e Nucleares (IPEN)," Brazil.

Funding for this research has been provided by IPEN and the "Comissão Nacional de Energia Nuclear," Brazil.

I greatly appreciate the encouragement and support of my beloved wife, Célia Maria.

ABSTRACT

The work presented here is of direct use in Probabilistic Risk Assessment (PRA) and is of value to Utilities as well as the Nuclear Regulatory Commission (NRC).

Specifically, this report presents a methodology and a computer program to calculate the expected number of occurrences for each accident sequence in an event tree. The methodology evaluates the time-dependent (instantaneous) and the average behavior of the accident sequence. The methodology accounts for standby safety system and component failures that occur (a) before they are demanded, (b) upon demand, and (c) during the mission (system operation). With respect to failures that occur during the mission, this methodology is unique in the sense that it models components that can be repaired during the mission. The expected number of system failures during the mission provides an upper bound for the probability of a system failure to run -- the mission unreliability. The basic event modeling includes components that are continuously monitored, periodically tested, and those that are not tested or are otherwise nonrepairable.

The computer program ASA allows practical applications of the method developed. This work represents a required extension of the presently available methodology and allows a more realistic PRA of nuclear power plants.

TABLE OF CONTENTS

CHAPTER	PAGE
I. INTRODUCTION.....	1
I.1 Purpose and Scope.....	2
I.2 Structure of the Dissertation.....	6
I.3 Important Definitions.....	7
I.4 Existing Methodologies and Computer Programs for Quantitative Reliability Analysis.....	12
I.5 Reliability Analysis.....	22
II. A METHODOLOGY FOR THE TIME-DEPENDENT ANALYSIS OF ACCIDENT SEQUENCES.....	33
II.1 The Accident Sequence's Expected Number of Failures.....	33
II.2 The Accident Sequence's Time-Dependent Undependability.....	37
II.3 An Expression for the Accident Sequence's Undependability.....	43
II.4 An Expression for the System Undependability.....	47
II.5 The Basic Event Unavailabilities.....	54
II.6 The ASA Computer Program.....	58
II.7 Application of the ASA Computer Program.....	62
III. SUMMARY, CONCLUSIONS, AND RECOMMENDATIONS.....	68
LIST OF REFERENCES.....	71
APPENDIXES.....	80

A. Input to the ASA Computer Program.....	81
B. Example of an Input to the ASA Computer Program.....	93
C. Example of an Output of the ASA Computer Program.....	96
D. The Listing of the ASA Computer Program.....	104
VITA.....	174

LIST OF TABLES

TABLE	PAGE
I.1 Factors Affecting the Basic Event and the Accident Sequence Unavailabilities.....	10
I.2 Some Computer Programs for Quantitative System Reliability Analysis.....	13
I.3 Some Sources of Nuclear Component Reliability Data.....	27
I.4 Data Sources and Prediction Techniques for Human Error Probabilities.....	31
II.1 Point Numbers Used in Figure II.5.....	66

LIST OF FIGURES

FIGURE	PAGE
II.1 A Generic Accident Sequence.....	39
II.2 Fault Tree for a Generic Accident Sequence in an Event Tree.....	40
II.3 A Diagram Illustrating the Time Sequence for the Occurrence of an Accident Sequence.....	41
II.4 Failure Block Diagram: Shutdown Heat Removal System.....	63
II.5 Accident Sequence Undependability for Cases I and II.....	65

CHAPTER 1

INTRODUCTION

Nuclear reactor safety concerns the public, the utilities that operate the nuclear power reactors, and the government. Increased public concern creates a need for advanced methods of risk assessment to provide proper information to the decision makers of our society. This dissertation extends the methodologies and computer programs available for the estimation of the potential for nuclear accidents. It also expands the techniques of reliability analysis as applied to large, complex systems such as those in the nuclear and chemical industries.

In particular, the complexity and the size of the protection system of nuclear power reactors require more advanced methods of system reliability analysis. The protection system includes the containment isolation system (CI), the emergency core cooling system (ECCS), the containment-pressure reduction system, the emergency or auxiliary power system, the air filtration system, and the reactor shutdown system. The protection system mitigates the consequences resulting from the occurrence of accident initiating events, such as a loss of coolant accident (LOCA), in nuclear power reactors. In this context, the systems mentioned form a group of standby systems which act when the accident initiating event occurs.

Upon the occurrence of the accident initiating event, each of the standby systems either works or fails (success or failure). Any combination of failures and successes of the standby systems is

called an accident sequence. The expected number of times that an accident sequence occurs over a period of time represents an important safety parameter. This parameter, called the Expected Number of Failures (ENF) for the accident sequence, has direct application in probabilistic risk assessment. The ENF is also an important parameter in reliability analysis, where it provides an important tool in optimization studies.

A standby system's failure may occur in two ways. A standby system may fail to start its intended function, or it may start to function properly but fail to perform adequately during the required period of operation. The term "failure to run" labels this second case. Analysis of these systems' failures may require different reliability failure models (fault trees, reliability block diagrams, and so forth).

I.1 PURPOSE AND SCOPE

This dissertation develops a methodology and a computer program to calculate the expected number of occurrences for each accident sequence in an event tree, where fault trees are available for each branching point in the event tree. The methodology evaluates the time-dependent behavior of a generic accident sequence, allowing a detailed modeling of periodic testing and repair.

The time-dependent analysis of the systems in the accident sequence includes not only the possibility of a system's failure to start at a point in time but also the chance of a system's failure to perform its intended function, following a successful start. Thus,

the analysis accounts for failures that occur before the demand, the failures that occur on demand, and the failures that occur during the mission. With respect to the failures that occur during the mission, the methodology developed in this dissertation is unique in the sense that it allows the system's components to be repairable during the mission time. The following assumptions are used in the methodology:

1. The fault trees representing the system's failures at each branching point in the event tree are
27
coherent.
2. The different basic events in the fault trees are statistically independent in failure and repair.
3. The expected number of accident sequence occurrences during the mission is used to provide a conservative upper bound to the mission unreliability (the probability that the system formed by all the systems in the accident sequence starts and fails to perform adequately during the mission).
4. The repairable systems in the accident sequence or combinations of such systems are assumed to be nonrepairable during the mission (a conservative assumption).

In the analysis of a single system, assumption 4 needs not be made. In some applications, the systems in the accident sequence share no basic events and are independent of each other. In these cases, each system may be treated as an independent event, and the

combination of such independent events becomes a single system for which assumption 4 is unnecessary.

This is the case, for example, presented by Elerath, Vaurio,²³ and Wood. They modeled the common support systems (power supplies) as independent systems in parallel with the front line systems (the cooling systems). In this way, each of the front line and support systems becomes an independent basic event. Chapter II presents the analysis of this same problem using the computer program developed in the study presented here.

Chapter II dicusses assumptions 3 and 4 in more detail. The remainder of this section briefly discusses assumptions 1 and 2 and phased-mission analysis (a related topic).

The fault trees representing the system's failures at each branching point in the event tree are assumed to be coherent as²⁷ defined by Esary and Prochan. As a consequence of this assumption, the following topics are not directly addressed in this work:

1. Secondary Failures. These are causes of component malfunction for which the component itself is not held accountable; however, the component needs to be repaired before the malfunction is corrected (see reference 72 for a methodology that considers secondary failures).
2. "DELAY" Gates. These represent situations in which the top event occurs if the basic events in at least one MCS exist for a sufficient time period (a definition of an MCS appears on page 9). For

example, a "vessel rupture" results if the malfunction causing a high-pressure condition persist long enough that the pressure can build up to the rupture point.

3. Mutually Exclusive "OR" Gates. These represent situations in which the existence of one of the inputs to the "OR" gate guarantees the nonexistence of another input.
4. Basic events in the fault trees which, when they exist, decrease the existence probability of the top event. This is to say that the top event must be a nondecreasing function of the existence probabilities of the basic events.

In addition to the assumption of coherence, the different basic events in the fault trees are assumed to be statistically independent in both failure and repair. The study of dependencies among components' failures has received increased attention in PRA,^{14,15,21,30} where it has become a complex part of the analysis. In some cases, as in flood analysis, special event trees/fault trees are required to study dependencies because accident-sequence issues are different for these scenarios than for accidents initiated from other sources (see, for example, the comments by Budnitz on flood analysis).¹¹ Parametric methods such as the Beta-factor³⁰ and the BFR models⁶ account for other types of dependencies, those not explicitly considered in the event trees or fault trees.³⁰

A third method to study dependencies consists of using computer programs such as COMCAN II⁷² and SETS,¹⁰² which identify the root causes of dependencies, called the root cause events (e.g., high temperature and high vibration conditions). In practice, a combination of the methods above provides an adequate inventory of techniques for the Dependent Failure Analysis (DFA). This dissertation does not address, but is complemented by, dependent failure analysis.

In some applications, the system configuration may change at some times. A good example is the Emergency Core Cooling System (ECCS) changing from the High Pressure Coolant Injection (HPCI) to the Low Pressure Coolant Injection (LPCI). At such moments, the accident sequence's and the system's failure probability may change without a component failure or repair. This situation, called "Phased-Mission Analysis," requires special mathematical^{13,39,62} treatment and is not addressed in this dissertation.

I.2 STRUCTURE OF THE DISSERTATION

The remainder of this chapter discusses the following topics: 1) important definitions, 2) existing methodologies and computer programs related to the subject of this research, 3) reliability and system reliability analyses, and 4) comments on data.

Chapter II describes the methodology developed in this study. It starts with the derivation of an integral equation for the accident sequence's ENF. The ENF is a function of the initiating event's rate of failure and the accident sequence's

undependability. Then Chapter II defines the system's and accident sequence's time-dependent undependabilities. Sections II.3 and II.4 show how to calculate the accident sequence's undependability as a function of the basic event's unavailabilities. The equations for the basic event's unavailabilities are derived in Section II.5. Chapter II then presents a brief description of the computer program used to implement the methodology developed here. The last section shows an example problem extracted from the available literature.

Chapter III summarizes the report and concludes the research. Recommendations for further studies are also presented. Appendix A contains the information necessary to run the ASA code. Appendix B shows an example of an input to the code, and, in conjunction with Appendix A, should provide enough detail to allow the use of the program. Appendix C shows the program output to the example in Appendix B. The listing of the ASA computer program appears in Appendix D.

I.3 IMPORTANT DEFINITIONS

Event tree and fault tree analyses are major tools in system reliability analysis. The event tree identifies the possible outcomes resulting from accident initiating events. The accident initiating event may be a system failure (such as a ruptured pipe or a thermal transient) or an external event (such as loss of off-site power or an earthquake). The event tree begins with the initiating event. Next, all the systems that affect the subsequent course of

events are identified, defined, and ordered in a convenient form. Each system may either work or fail following the occurrence of the initiating event. Under this binary assumption, each system generates two branches in the event tree. References 59 and 99 provide detailed information about event trees.

Fault trees provide the means to compute the probabilities of failure and successes at each branching point in the event tree. A fault tree is a logical representation of an undesirable event or malfunction of interest, called the "top event," in terms of the basic failures that lead to the top event. The basic failures are called the "basic events." The top event may represent a general statement such as "Release of radioactivity from a nuclear power plant." It can also represent a specific system failure, such as "Failure to insert control rods" or "Motor does not operate."

Given a particular system failure in the event tree, fault trees identify the various combinations of basic failures that lead to the given system failure. The probabilistic information available for the basic events in the fault trees is then combined to provide probabilistic information for the top event. Fault trees are often very large, and computer programs are usually required to perform the desired calculations. Examples of such computer programs are SUPERPOCUS, KITT, FRANTIC, and FRANTIC II-MIT (see references 37, 90, 94, and 20, respectively).

A general time-dependent and quantitative reliability analysis must include not only the possibility of a system's failure to start at a point in time but also the chance of a system's failure

to run following a successful start. The analysis should then account for failures that occur before the demand (predemand), failures that occur on demand (demand-related), and the failures that occur during the mission (postdemand). Table I.1 lists the factors which affect these failures.

In this study, a component is said to have failed to "start" if the failure results from a predemand or from a demand-related factor. If a component's failure results from a postdemand factor, the component is said to have failed to "run."

Some basic events in the fault trees represent component failures that can result from predemand or demand-related as well as postdemand factors (e.g., a diesel generator can fail to start or fail to run). These basic events are here defined as "Type I" basic events. Some basic events represent components' failures to start only. The basic events which represent failures to start only (predemand and demand-related failures) are here defined as "Type II" basic events.

In this dissertation, the approach selected to relate the systems and accident sequences to the basic events in the fault tree makes use of the Minimal Cut Sets (MCSs) and the Minimal Path Sets (MPSs). An MCS is a collection of basic events, such that the simultaneous existence of all these events guarantees the existence of the top event, and removal of any basic event from this set no longer guarantees the existence of the top event. An MPS is the smallest collection of basic events, such that if all the basic

Table I.1 Factors Affecting the Basic Event and the Accident Sequence Unavailabilities.

Factor Affecting the Unavailability	Example
Random failures and repair prior to the demand or during the mission (predemand and postdemand factors).	A pump that fails on standby due to corrosion problems or a pump that fails to run due to normal wear of a moving part.
Unavailability due to testing, repair, and maintenance (pre-demand factor).	A pump which is unavailable because of the inability to recover from a test, repair, or maintenance work.
Human errors in testing, maintenance, and repair (usually a predemand factor).	A check valve that is installed backwards.
Unavailability due to unrevealed design, manufacturing, installation, and commissioning errors (predemand, demand-related and postdemand effects).	The use of inadequate components, poor welding, component damaged during installation, and so forth.
Unavailability due to extreme environmental conditions such as high temperature, humidity, contamination, vibration, etc. (predemand, demand-related and postdemand effects).	A pump- or valve- seal that fails due to contamination damage.

Table I.1 (continued)

Factor Affecting the Unavailability	Example
Failures due to events such as fire, flooding, earthquakes, etc. (usually a post- demand or demand- related factor).	A building collapsing during an earthquake, resulting in several component failures.
Human errors during abnormal conditions (demand-related or a postdemand factor).	Failure to follow the emergency procedures or failure due to misinterpretation of the information available.
Defective procedures (predemand, demand- related or post- demand factor).	A defective operation procedure that results in reactor shutdown.
Changes in the system (postdemand factor)	A system change during a phased-mission.

events simultaneously do not exist then the top event is guaranteed
39
not to exist.

An MCS fails to start if all of its basic events fail to start. Any other MCS failure is a failure to run. An accident sequence (or a system) fails to start if at least one of its MCSs fails to start. Any other accident sequence (system) failure is a failure to run. An MCS containing only Type II basic events cannot fail to run; it either fails to start or does not fail. Within this framework of definitions, the same fault tree represents the system's failure to start and the system's failure to run.

I.4 EXISTING METHODOLOGIES AND COMPUTER PROGRAMS FOR QUANTITATIVE RELIABILITY ANALYSIS

Several methodologies and computer programs are currently available for the quantitative reliability analysis of complex systems. Basically, they synthesize probabilistic information for a system from the probabilistic information available for the system's components or parts. Some of the computer programs for quantitative system reliability analysis are briefly described in Table I.2.

Some of the codes in Table I.2 (particularly the FRANTIC family and FRANCALC) evaluate the time-dependent and average unavailability for any general system model. They analyze components with a constant probability of failure, nonrepairable components, monitored components, and periodically tested components. FRANTIC II and FRANTIC II-MIT allow even more detailed treatment of the basic
20,96
events. The unique feature of these computer programs is the

Table I.2 Some Computer Programs for Quantitative System Reliability Analysis.

Computer Program	Comments
^a FAUNET	Written for minicomputer; uses a top-down pruning and bottom-up modularization Boolean substitution algorithm; also calculates top event existence probability.
^b GO	Uses a Boolean manipulation algorithm; also calculates point estimates of top event characteristics.
^c KITT 1&2	Calculate time-dependent availability, reliability, and expected number of failures from component failure rates and repair times; also calculate component importance. For some controversy on the computation of the time-dependent reliability, see references 18, 63, 89, and 91 in the list of references.
^d SUPERPOCUS	Calculates the same time-dependent characteristics as KITT, using bounding approximation methods.
^e WAM-BAM	Calculates Top event existence probabilities using Boolean manipulation.
^f FRANTIC	Calculates the effect on the average unavailability and time-dependent instantaneous unavailability due to periodic system testing; testing characteristics include the test interval, test duration time, repair time, and human-caused failure potential associated with the testing. This program requires an analytical expression of the system unavailability as a function of the component unavailabilities as an input.

Table I.2 (continued)

Computer Program	Comments
^g PROBCALC	Uses a direct evaluation method that does not rely on MCSs and Boolean reduction but employs a numeric technique for calculating the probabilities of series and parallel paths in either success or failure state diagrams or from fault trees.
^h FRANCALC	Combines the features of FRANTIC and PROBCALC with additional improvements such as a criteria for ordering and terminating conditional probability calculations in order to reduce computing time within a special level of accuracy. It also accepts m-out-of-n:G subsystems. Mutually exclusive and multiple failure modes can also be defined for components.
ⁱ FRANTIC II and FRANTIC II-MIT	The original FRANTIC code assumes constant failure rates, and its extension (the FRANTIC II code) models burn-in and wear-out periods. Dykes has further improved the code with several modifications and additions including interfacing the code with a cut set generator. The resulting computer program is called FRANTIC II-MIT.

^a
Platz, O. and Olsen, J.V., "FAUNET: A Program Package for Evaluation of Fault Trees and Networks," Report RISO-348, Danish Atomic Energy Commission, September 1976.

^b
Gately, W.Y. and Williams, R.L., "GO methodology- System Reliability Assessment and Computer Code Manual," Electric Power Research Institute, EPRI NP-766, May 1978.

Table I.2 (continued)

^c
Vesely, W.E. and Narum, R.E., "PREP and KITT: Computer Codes for the Automatic Evaluation of a Fault Tree," USAEC Rep. IN 1349, Idaho Nuclear Corporation, August 1970.

^d
Fussell, J.B., et al., "SUPERPOCUS- A Computer Program for Calculating System Probabilistic Reliability and Safety Characteristics," NERS-77-01, Knoxville: Nuclear Engineering Department, May 1977.

^e
"WAMCUT-II, A Fault Tree Evaluation Program," Electric Power Research Institute, EPRI NP-2421, June 1982.

Leverenz, F.L. and Kirch, H., "User's Guide for the WAM-BAM Computer Code," Electric Power Research Institute, EPRI-217-2-5, January 1976.

^f
Vesely, W.E. and Goldberg, F.F., "FRANTIC- A Computer Code for Time Dependent Unavailability Analysis," NUREG-0193, United States Nuclear Regulatory Commission, March 1977.

^g
Elerath, J.G. and Ingram, G.E., "PROBCALC User's Manual: A Computer Program for Probability Calculation," GEFR-00408, General Electric Company, Sunnyvale, California, 1980.

^h
Elerath, J.G., Vaurio, J.K., and Wood, A.P., "A Method for Reliability Analysis of Complex Reactor Systems," The ANS/ENS International Meeting on Fast Safety Technology, Lyon, France, July 1982.

ⁱ
Dykes, A.A., "Application of Time Dependent Unavailability Analysis to Standby Safety Systems," Ph.D. Dissertation, Department of Nuclear Engineering, MIT, June 1982.

Vesely, W.E., Goldberg, F.F., Powers, J.T., et al., "FRANTIC II- A Computer Code for Time Dependent Unavailability Analysis," NUREG/CR-1924, April 1981.

detailed, time-dependent modeling of periodic testing and repair. This modeling accounts for the effects of the test downtime, test overrides, detection inefficiencies, test-caused failures, and so forth.

FRANTIC requires a user-defined analytical expression relating the system failure probability to the component failure probabilities. The latest version, FRANTIC II-MIT, which includes an MCS generator, uses MCSs to perform this task. FRANCALC works in a different way, making no use of MCSs nor of Boolean reduction. The approach in FRANCALC consists of computing the system failure probability by evaluating series and parallel arrangements of components. For complex logics, when components appear in more than one path of a block diagram, the code applies the theorem of total probability²³ to the system. To illustrate this approach, suppose that an event E appears in more than one path of a failure block diagram (or, equivalently, in more than one MCS). The system failure probability, $P(\bar{S})$, is then given by

$$P(\bar{S}) = P(\bar{S}|E) P(E) + P(\bar{S}|\bar{E}) P(\bar{E}), \quad (1.1)$$

which can be applied to any number of such events. In the preceding equation, $P(\bar{E})$ and $P(E)$ are the probabilities of occurrence and nonoccurrence of the event E, respectively.

A quantitative system reliability analysis must include the possibility of a system's failure to start and the chance of a system's failure to run following a successful start. The

methodology developed and implemented by Elerath, Vaurio, and Wood in FRANCALC models the two components of the system's failure probability when the basic events are assumed to be nonrepairable during the mission. The basic events, however, may be repaired at any other time. FRANTIC, FRANTIC II, and FRANTIC II-MIT perform the same analysis under the same assumption.

23

Elerath, Vaurio, and Wood have analyzed the total probability of a system failure by combining the probability that the component starts and fails to run and the probability that the component fails to start. The total component failure probabilities are then input to the fault tree model (or any other reliability model) to compute the probability that the system will fail. Since the components are assumed to be independent in failure, and there is no repair, the probability of a system's failure depends only on the state of the components at the end of the mission. For example, if all the components are working at the end of the mission, the system's failure has not occurred.

This is not the case when component repair is allowed during the mission. Knowing that all the components are working at the end of the mission does not guarantee that some of them were not failed during the mission, causing the top event to exist. The approach by Elerath, Vaurio, and Wood, here defined as the "existing approach," does not apply to the case where the components are repairable during the mission. The existing approach can only be used to provide an upper bound in this case (this is accomplished by assuming that the repairable basic events are nonrepairable).

The approach proposed in the work presented here calculates the probability of system failure by combining the probability that the system starts and fails to run and the probability that the system fails to start. This allows a more realistic solution to the problem. This approach, here defined as the "proposed approach," combines the probabilities of failure to start and failure to run at the system level while the existing approach combines them at the basic event (or component) level.

I.4.1 Comparison of Existing and Proposed Methodologies:

A Simple Example

The following simple example shows a major difference between the existing and the proposed approaches. In this example, a system is composed of two components. The components fail independently and are nonrepairable during the mission. The failure block diagram for this system is as following:



When a demand occurs, the system may fail to start. If the system starts, two possibilities remain: the system may perform its required function or the system may fail to run. The notation used in this example is consistent with the notation used in Chapter II and is given below. The component's unreliability is its conditional failure probability, given a successful start:

i	represents components A and B.
$\bar{a}_i$	the unavailability of component i .
$\bar{r}_i$	the unreliability of component i .
$a_i = 1 - \bar{a}_i$	the availability of component i .
$r_i = 1 - \bar{r}_i$	the reliability of component i .
$P = \bar{a}_i + a_i \bar{r}_i$	the probability that component i fails.

For simplicity, $\bar{a}_A = \bar{a}_B = \bar{a}$ and $\bar{r}_A = \bar{r}_B = \bar{r}$, where $\bar{a}$ and $\bar{r}$ are constants with respect to time. According to the description in reference 23 (pages 2-4), the existing approach calculates the system's undependability as follows:

$$P(\text{system fails}) = P(AB) = P(A) P(B) = P^2,$$

where $P = \bar{a} + (1 - \bar{a})\bar{r}$. Thus,

$$P(\text{system fails}) = (\bar{a} + (1 - \bar{a})\bar{r})^2$$

Following the approach proposed in this dissertation,

$$\begin{aligned}
 P(\text{system fails}) &= P\left(\begin{array}{c} \text{system} \\ \text{fails} \\ \text{to start} \end{array} \text{ or } \begin{array}{c} \text{system} \\ \text{fails} \\ \text{to run} \end{array}\right) \\
 &= P\left(\begin{array}{c} \text{system} \\ \text{fails} \\ \text{to start} \end{array}\right) + P\left(\begin{array}{c} \text{system} \\ \text{starts} \end{array} \text{ and } \begin{array}{c} \text{system} \\ \text{fails} \\ \text{to run} \end{array}\right) \quad (1.2)
 \end{aligned}$$

The last step above is based on the expression $P(EUF) = P(E) + P(\bar{E}F)$. Each term of the equation above is now evaluated separately. By direct inspection of the failure block diagram,

$$P \left(\begin{array}{c} \text{system} \\ \text{fails} \\ \text{to start} \end{array} \right) = \bar{a} \bar{a} = \bar{a}^2.$$

The last term in Equation 1.2 requires a special treatment. The probability of a system failure to run depends on the condition of the system's components at the time of the demand. Therefore, it is convenient to consider all the possible combinations of component failures and successes at the time when the demand on the system occurs. The number of combinations is given by 2^n , where n is the number of components ($n=2$ for the system under consideration). Let S_i ($\bar{S}_i$) represent the event "component i (not) available when the demand occurs." Then, the set of all possible combinations of component failures and successes represents the set of possible states for the system. When the demand occurs, the system must be in one of the following states:

S_A	S_B	1
S_A	$\bar{S}_B$	2
$\bar{S}_A$	S_B	3
$\bar{S}_A$	$\bar{S}_B$	4

The system's states 1, 2, and 3 represent states for which the system starts to operate. State 4 represents the failure to start. In order for the system to fail to run, it must first be in one of the states 1, 2, or 3. Therefore, the computation of the second term in Equation 1.2 begins by calculating the probability of the system being in one of the states 1, 2, and 3. If the system is indeed in one of these three states, it can perform properly until the end of the mission, or it can fail to run. Thus, the second step in the computation of the second term in Equation 1.2 is to calculate the probability that the system fails to run given that it is in one of the states 1, 2, and 3.

The components' failures are statistically independent. Therefore, the probability of the system being in one of the states 1, 2, and 3 equals the product of the probabilities of the components being in the failed or working states:

System's State i	Probability of the System Being in State i
1	$(1-\bar{a})^2$
2	$(1-\bar{a}) \bar{a}$
3	$\bar{a} (1-\bar{a})$

If the system is in state 1, the probability of a failure to run is $\bar{r}^2$. If the system is in states 2 or 3, this probability is $\bar{r}$. Thus,

$$P \left(\begin{array}{c} \text{system} \\ \text{fails} \\ \text{to run} \end{array} \text{ and } \begin{array}{c} \text{system} \\ \text{starts} \end{array} \right) = (1-\bar{a})^2 \bar{r} + 2 \bar{a} (1-\bar{a}) \bar{r},$$

which, when added to the probability that the system starts, gives the following result:

$$\begin{aligned} P \left(\begin{array}{c} \text{system} \\ \text{fails} \end{array} \right) &= \bar{a}^2 + (1-\bar{a})^2 \bar{r} + 2 \bar{a} (1-\bar{a}) \bar{r} \\ &= \left(\bar{a} + (1-\bar{a}) \bar{r} \right)^2. \end{aligned}$$

This is the same result obtained by using the existing approach.

I.5 RELIABILITY ANALYSIS

The discipline reliability analysis models and analyzes random failure processes. System reliability analysis, a subset of reliability analysis, obtains probabilistic information about a system from probabilistic information available for the system's parts or components. System reliability analysis attempts to reduce the expected number of system failures, the expected time the system failures exist, or a combination of these.

I.5.1 Historical Remarks

The concern for reliability has existed for thousands of years. According to Goldberg, "in the structural world reliability meant structures that would not collapse." Reliable structures have been designed and built for thousands of years. The pyramids in

Egypt, the cathedrals in Europe, and other buildings of the past represent the highly reliable structures built in our early days.

Several reliable devices were built before the advent of reliability formalisms or reliability analysis. The undersea telephone cables built by Bell Telephone Laboratories provide a good example. As Goldberg⁴¹ mentions, the cables are still operating today. This high reliability, however, resulted from about twenty years of tests and experience in working with those cables.

The advent of high-technology systems in the 1940s, however, brought about the need for reliability formalisms and reliability analysis. It would take too much time and an unacceptable number of accidents if the complex systems of today were built without reliability analysis techniques. The early 1940s marked the beginning of the formal application of mathematical and statistical theories in reliability analysis.

I.5.2 Fault Tree Analysis

During the early years of reliability analysis, the systems studied were not as large and complex as they are today. Also, the techniques for system reliability analysis were just beginning to be developed. Therefore, the emphasis of reliability analysis was directed towards components and simple systems.

Fault tree analysis (FTA) originated in the early 1960s and soon became one of the principal methods of system reliability analysis. A fault tree is a logical representation of an undesirable

event or malfunction of interest, called the "top event," in terms of basic failures, called the "basic events."

89

In 1970, Vesely⁸⁹ presented the Kinetic Tree Theory (KTT), a major contribution in the field of system reliability analysis. The KTT forms a basis for quantitative fault tree analysis. Later works^{93,94,96} -including those by Vesely and Goldberg,^{31,35,39} Fussell,⁶² Montague,²⁰ and Dykes -- have expanded the theory and practical applications of fault trees. The following paragraphs illustrate the development of fault trees.

Fault trees originated in 1961 as a technique to perform safety evaluation of the Minuteman Launch Control System. The concept was created by the Bell Telephone Laboratories.³³

At the Safety Symposium sponsored by the University of Washington and the Boeing Company in 1965, the papers presented showed the advantages of fault tree analysis. According to Fussell, this symposium "marked the beginning of a widespread interest" in the use of fault tree analysis as a reliability tool in the nuclear industry.³³

89,90

In 1970, Vesely^{89,90} published the Kinetic Tree Theory (KTT), which forms a basis for quantitative fault tree analysis (milestone suggested by Apostolakis, Garriba, and Volta).²

31,33

In 1972, Fussell and Vesely^{31,33} published a methodology that allows the identification of minimal cut sets of the fault trees. This milestone concerns the logical analysis of fault trees and provides qualitative and quantitative improvements in fault tree analysis (milestone suggested by Apostolakis, Garriba, and Volta).²

The publication of the Reactor Safety Study, in 1975, contributed to the development and increased applications of fault trees. It consisted of a major study to assess the risk involved in nuclear power reactors. The study summarized and expanded the fault tree methodology. The study also developed fault trees for all the safety-related systems in a nuclear power plant .

A recent milestone (1980s) has been the implementing of national reliability and risk evaluation programs such as the Interim Reliability Evaluation Program (IREP) and the Risk Methods Integration and Evaluation Program (RMIEP). Within these and other programs, techniques have been developed to further extend the theory and the application of fault trees.

I.5.3 Comments on Data

Quantitative reliability analysis depends on the quality of the reliability data available. Fussell and Arendt³⁸ have summarized the problems with reliability data for nuclear power plant applications as follows:

Reliability data are unlike other data such as nuclear cross sections. The basis of cross-section data is a large finite number of nuclei, all with identical properties. The basis of reliability data is stochastic, involving ever-changing components and environmental conditions. In addition, reliability data have the property of describing a statistical distribution rather than a fixed but unknown value. In other words, even under perfect measurement conditions, reliability data for a single event cannot be determined by a single test but rather must be determined from years of observation of equipment in various environments during which time the equipment designs may change. In addition, it is frequently easy to determine how

many components of a certain type failed in a certain way during a known time period. Unfortunately, it is often not known how many identical components did not fail during this time interval; i.e., the population of components in use is not known. Collecting and evaluating reliability data is very frustrating.

On the other hand, a set of precise data, although desirable, may not be required in many practical applications. Major engineering insights are still available even in the case of uncertain numerical results. The Probabilistic Reactor Accident Analysis for External Initiators (earthquakes, floods, and so forth), for example, provides insights which are "by-and-large qualitative in nature, even though the results are quantitative" (Budnitz).¹¹ The results of the IREP can aid in simulator design, and emergency-response personnel and operating training. Also, improvements in emergency or maintenance procedures often result from studies such as IREP. In addition, quantitative measures of importance to safety for the reliability of components allows cost-benefit analyses on reliability improvements for components. These, and other applications, do not depend on the exact accident sequence probability of occurrence.

Several sources of reliability data are currently available for application to nuclear power plants. These sources emerge from several years of operating experience in nuclear power plants, coal and oil-fired power plants, and other industries. Table I.3 shows some of the well-known and commonly used data sources for nuclear components. The IEEE Std. 500-1984 is a compilation of most of the nuclear reliability data publicly available for nuclear power plants in the United States. It is the most comprehensive set of nuclear

Table I.3 Some Sources of Nuclear Component Reliability Data.

Data Sources	Remarks ^a
^b LERs Fault/Failure rates and LERs Common Cause Fault/ Failure rates	Resulted from several studies performed at EG&G, Idaho, based on thousands of LERs.
^c IEEE Std. 500-1977	Data based on the Delphi method, with participation of more than 200 experts in the nuclear field.
^d IEEE Std. 500-1984	Compilation of several data banks (see text).
Modified WASH-1400	Data assembled by NRC personnel to be used in specific PRAs.
^e NPRDS	Data bank sponsored by the utilities and operated by INPO.
^f IPRDS	Data bank compiled from selected nuclear power plants.
^g Other NRC-sponsored studies or EPRI-sponsored studies	

^a
This table uses the following acronyms:

LER	Licensee Event Report
IEEE	Institute of Electrical and Electronic Engineers

Table I.3 (continued)

NRC	Nuclear Regulatory Commission
PRA	Probabilistic Risk Assessment
NPRDS	Nuclear Plant Reliability Data System
INPO	Institute for Nuclear Power Operations
IPRDS	In-Plant Reliability Data System
EPRI	Electric Power Research Institute

b

Atwood, C.L. and Steverson, J.A., "Common Cause Fault Rates for Diesel Generators: Estimates Based on Licensee Event Reports at U.S. Commercial Nuclear Power Plants, 1976-1978," NUREG/CR-2099, EGG-EA-5359, Revision 1, 1982.

Atwood, C.L., "Common Cause Fault Rates for Pumps," NUREG/CR-2098, EGG-EA-5289, EG&G Idaho, Inc., February 1983.

Atwood, C.L. and Steverson, J.A., "Common Cause Fault Rates for Valves," NUREG/CR-2770, EGG-EA-5485, EG&G Idaho, Inc., February 1983.

Atwood, C.L. and Meachum, T.R., "Common Cause Fault Rates for Instrumentation and Control Assemblies," NUREG/CR-3289, EGG-EA-2258, Idaho National Engineering Laboratory, EG&G Idaho, Inc., May 1983.

Hubble, W.H. and Miller, C.F., "Data Summaries of Licensee Event Reports of Control Rods and Drive Mechanisms at U.S. Commercial Nuclear Power Plants," NUREG/CR-1331, EGG-EA-5079, EG&G Idaho, Inc., February 1980.

Miller, C.F. et al., "Data Summaries of Licensee Event Reports of Selected Instrumentation and Control Components at U.S. Commercial Nuclear Power Plants," NUREG/CR-1363, EGG-EA-5816, Revision 1, October 1982.

Miller, C.F. et al., "Data Summaries of Licensee Event Reports of Valves at U.S. Commercial Nuclear Power Plants from January 1, 1976 to December 31, 1980," EGG-EA-5816, April 1982.

Sams, D.W. and Trojovsky, M., "Data Summaries of Licensee Event Reports of Primary Containment Penetrations at U.S. Commercial Nuclear Power Plants," NUREG/CR-1730, EGG-EA-5188, EG&G Idaho, Inc., September 1980.

Sullivan, W.H. and Poloski, J.P., "Data Summaries of Licensee Event Reports of Pumps at U.S. Commercial Nuclear Power Plants," NUREG/CR-1205, EGG-EA-5044, EG&G Idaho, Inc., January 1980.

Table I.3 (continued)

Trojovsky, M., "Data Summaries of Licensee Event Reports of Pumps at U.S. Commercial Nuclear Power Plants," NUREG/CR-1205, Revision 1, EGG-EA-5524, January 1982.

c

"IEEE Guide to the Collection and Presentation of Electrical, Electronic, and Sensing Component Reliability Data for Nuclear-Power Generating Stations," IEEE Std 500-1977, Institute of Electrical and Electronics Engineers, Inc., Wiley-Interscience, June 1977.

d

"IEEE Guide to the Collection and Presentation of Electrical, Electronic, Sensing Component, and Mechanical Equipment Reliability Data for Nuclear-Power Generating Stations," IEEE Std 500-1984, Institute of Electrical and Electronics Engineers, Inc., Wiley-Interscience, 1984.

e

"Nuclear Plant Reliability Data System (NPRDS) 1980 Annual Reports of Cumulative System and Component Reliability," NUREG/CR-2232.

f

"In-Plant Reliability Data System (IPRDS) Interim Draft Report on the Reliability Characteristics of Selected Pumps in Four Nuclear Plants," NUREG/CR-2886, May 1982.

g

Baranowsky, P.W., Kolaczowski, A.M., and Fedele, M.A., "A Probabilistic Safety Analysis of DC Power Supply Requirements for Nuclear Power Plants," NUREG-0666, April 1981.

Crooks, J.L. and Vissing, G.S., "Diesel-Generator Operating Experience at U.S. Nuclear Power Plants," USAEC, OOE-ES-002, June 1974.

"Loss of OffSite Power at Nuclear Power Plants: Data and Analysis," Electric Power Research Institute, EPRI NP-2301, March 1982.

Leverenz, F.L., Jr., Koren, J.M., Erdmann, R.C., and Lellouche, G.S., "Electric Power Research Institute, ATWS: A Reappraisal, Part II Frequency of Anticipated Transients," EPRI NP-801, June 1978.

reliability data available in the world. Table I.4 lists and briefly summarizes some of the sources for estimating human error probabilities. The THERP method, developed by Swain, ⁸⁵ is the most widely used method in the nuclear power industry.

Table I.4 Data Sources and Prediction Techniques for Human Error Probabilities.

Technique/Data Bank	Remarks
a American Institute for Research's Data Store (AIR's data store)	Contains information about various commonly found controls and displays for each item within the data store. The information was derived out of a review of over 2,000 research reports.
a Technique for Establishing Personnel Performance Standards (TEPPS)	Similar to THERP but assumes optimal conditions (no performance shape factors). Uses Pair-Comparison Ranking Technique to generate data from expert opinion.
b Technique for Human Error Reliability Prediction (THERP)	Same philosophy of the AIR data store but uses performance shape factors and recovery factors to allow a more realistic analysis.
a,c Siegel-Wolf Models 1-2 man model 4-20 crew size model 20-100 large group model	These are simulation techniques. They use probability distributions as input.
d Systems Analysis of Integrated Networks of Tasks (SAINT)	This is a simulation language which allows great flexibility to model the man-machine system.

Table I.4 (continued)

Technique/Data Bank	Remarks
a,e Maintenance Personnel Performance Simulation (MAPPS)	This is a simulation technique developed for maintenance applications. It allows dynamic representation of human behavior and behavioral influences on a computer.
a Siegel, A.I., Bartter, W.D., Wolf, J.J., Knee, H.E., and Haas, P.M., "Front-End Analysis for the Nuclear Power Plant Maintenance Personnel Reliability Model," NUREG/CR-2669, ORNL/TM-8300, August 1983.	
b Swain, A.D., "Handbook of Human Reliability Analysis with Emphasis on Nuclear Power Plant Applications," NUREG/CR-1278, H.E. Guttman (Ed.), Sandia National Laboratories, Albuquerque, NM, 1980.	
c Siegel, A.I. and Wolf, J.J., "Man-Machine Simulation Models," John Wiley & Sons, Inc., New York, 1969.	
d Seifert, D.J. and Chubb, G.P., "SAINT: A Combined Simulation Language for Modelling Large Complex Systems," AMRL-TR-78-48, Aerospace Medical Research Laboratory, Wright-Patterson Air Force Base, Ohio, October 1978.	
Wortman, D.B., Duket, S.D., Seifert, D.J., Hann, R.L., and Chubb, G.P., "The SAINT User's Manual," AMRL-TR-77-62, Aerospace Medical Research Laboratory, Wright-Patterson Air Force Base, Ohio, June 1978.	
e Knee, H.E., Krois, P.A., Haas, P.M., Siegel, A.I., and Ryan, T.G., "Maintenance Personnel Performance Simulation (MAPPS)- A Model for Predicting Maintenance Performance Reliability in Nuclear Power Plants," 11th Water Reactor Safety Information Meeting, National Bureau of Standards, Washington, D.C., October 24-28, 1983.	

CHAPTER II

A METHODOLOGY FOR THE TIME-DEPENDENT ANALYSIS OF ACCIDENT SEQUENCES

This chapter presents a methodology for the time-dependent analysis of accident sequences. It derives equations to calculate the accident sequence's expected number of occurrences in a specified time interval. This chapter also includes a brief description of the ASA computer program. This program allows the implementation of the methodology developed here. In addition, this chapter contains an example problem to illustrate the application of the methodology and the computer program.

II.1 THE ACCIDENT SEQUENCE'S EXPECTED NUMBER OF FAILURES

This section presents the derivation of an expression for the Expected Number of Failures (ENF) for a generic accident sequence. It gives the ENF as a function of the rate of failure of the initiating event and the accident sequence's time-dependent undependability.

The rate of failure of the initiating event is defined as the expected number of occurrences of the initiating event per unit time. The term "undependability" represents the total probability of occurrence of an accident sequence following the occurrence of the initiating event. Section II.2 presents a detailed definition and discussion of the undependability.

The ENF for each accident sequence is here defined as the average number of occurrences of that sequence due to occurrences of the initiating event in the specified period of time (0,t). The ENF has direct application in Probabilistic Risk Assessment (PRA). In PRA, the ENF for an accident sequence may multiply a power of the expected damage, i.e., the magnitude of a consequence resulting from the occurrence of the accident sequence. This product provides a probabilistic measure of risk.

The ENF also provides a useful tool in optimization studies. An optimization study consists of changing the system structure, the maintenance procedures, or a system component in order to minimize a system parameter such as the ENF, cost, and others parameters. The ENF is a more complete optimization parameter than the unavailability or the undependability. As shown later in this section, the ENF includes the effects of the undependability and the rate of failure of the initiating event. If the rate of failure of the initiating event is a constant, then the optimization of the ENF and the optimization of the undependability lead to identical numerical results.

The time-dependent rate of failure of the initiating event, $\text{rof}_{\text{IE}}(t')$, is defined as the expected number of occurrences of the initiating event per unit time at time t' . In this way,

$$\text{rof}_{\text{IE}}(t') dt' = \begin{array}{l} \text{Expected number of} \\ \text{occurrences of the} \\ \text{initiating event} \\ \text{in the time} \\ \text{interval } dt' \\ \text{around } t'. \end{array}$$

Not all the occurrences of the initiating event result in the occurrence of the top event (a specific accident sequence). As already mentioned, the undependability, represented by $\bar{d}_{AS}(t', t'+T)$, is the probability that the accident sequence does occur following the existence of the initiating event. Thus, the ENF of the accident sequence in the time interval from 0 to t due to occurrences of the initiating event in the time interval dt' around t' is given by the following expression:

$$\begin{aligned} & \left[\text{rof}_{IE}(t') dt' \right] \times \bar{d}_{AS}(t', t'+T) = \text{Contribution to the ENF of the} \\ & \hspace{15em} \text{top event in the time interval} \\ & \hspace{15em} \text{from 0 to t due to occurrences} \\ & \hspace{15em} \text{of the initiating event in the} \\ & \hspace{15em} \text{time interval } dt' \text{ around } t'. \end{aligned}$$

Integration over t' from 0 to t gives the ENF of the top event during the time interval from 0 to t:

$$\text{ENF}_{TE}(0, t) = \int_0^t \text{rof}_{IE}(t') \bar{d}_{AS}(t', t'+T) dt' \quad (2.1)$$

The accident sequence's undependability, $\bar{d}_{AS}(t', t'+T)$, consists of the following two parts:

$$\bar{d}_{AS}(t', t'+T) = \bar{a}_{AS}(t') + \int_{t'}^{t'+T} f_{AS}(t''-t'; t') dt'', \quad (2.2)$$

where $\bar{a}_{AS}(t')$ represents the accident sequence's unavailability at t' , and $f_{AS}(t''-t';t') dt''$ represents the probability that the accident sequence starts at t' and occurs for the first time in dt'' around t'' . The last term on the right-hand side of the equation above includes the accident sequence unreliability.

In practical applications, $rof_{IE}(t')$ is usually directly estimated from past experience and from analytical models. The accident sequence's undependability depends on the probabilistic parameters of the components and their functional relationship. In this dissertation, fault trees model the accident sequences and provide the basic theory to evaluate these quantities. Section II.3 describes the derivation of expressions to evaluate the accident sequence undependability.

II.1.1 An Alternative Equation for the Expected Number of Failures

The $ENF_{TE}(0,t)$ can also be defined as a function of the rate of failure of the top event as follows:

$$ENF_{TE}(0,t) = \int_0^t rof_{TE}(t') dt', \quad (2.3)$$

where $rof_{TE}(t')$ is the rate of failure of the top event at time t' , defined as the expected number of occurrences of the top event in the time interval dt' around t' per unit time. In general,

$$rof_{TE}(t') dt' \neq rof_{IE}(t') \bar{d}_{AS}(t',t'+T) dt'.$$

An expression for $\text{rof}_{\text{TE}}(t')$ is derived in the following way. Failures of the top event at t' may result from the occurrence of the initiating event at t' . In this case, the contribution to $\text{rof}_{\text{TE}}(t')$ is $\text{rof}_{\text{IE}}(t') \bar{a}_{\text{AS}}(t')$. Failures of the top event at t' may also result from the occurrence of the initiating event prior to t' . The following sequence must happen in this case:

1. The initiating event occurs at t'' , $t' - T \leq t'' \leq t'$, with rate of failure $\text{rof}_{\text{IE}}(t'')$.
2. The accident sequence starts at t'' and fails to run at t' , with probability $f_{\text{AS}}(t' - t''; t'') dt''$.

Thus,

$$\text{rof}_{\text{TE}}(t') dt' = \left[\text{rof}_{\text{IE}}(t') \bar{a}_{\text{AS}}(t') + \int_{t' - T}^{t'} \text{rof}_{\text{IE}}(t'') dt'' f_{\text{AS}}(t' - t''; t'') \right] dt' \quad (2.4)$$

Although Equations 2.3 and 2.4 provide the same final result as Equation 2.1, the former are more expensive to evaluate in a computer. Therefore, 2.1 has been selected for this dissertation.

II.2 THE ACCIDENT SEQUENCE'S TIME-DEPENDENT UNDEPENDABILITY

An accident sequence consists of a combination of successes and failures of the systems included in the event tree. The probability of a system success, $P(S)$, approaches 1 due to the high reliability of the systems involved. Furthermore, the assumption of

the unit value for $P(S)$ always overpredicts the expected number of failures of the accident sequence. Therefore, setting $P(S)=1$ results in a realistic and conservative assumption. If this is done, the problem becomes the analysis of a sequence of system failures. These system failures are defined here as $\bar{S}_1, \bar{S}_2, \bar{S}_3, \dots, \bar{S}_n$. In general, $\bar{S}_i$ represents the i th system failure ($i=1,2,3,\dots,n$). Figure II.1 further exemplifies the notation just defined.

The accident sequence analysis starts by conceptually drawing a fault tree for the accident sequence under consideration. The following top event heads the fault tree: "The accident sequence under study occurs." This fault tree appears in Figure II.2. The top event occurs if the initiating event occurs and the system failures $\bar{S}_1, \bar{S}_2, \bar{S}_3, \dots, \bar{S}_n$ exist simultaneously in the time interval $(t', t'+T)$. The time interval $(t', t'+T)$ (the mission time) starts when the initiating event occurs at time t' and extends from t' to $t'+T$, with duration T . T represents the average time that the systems in the accident sequence must operate following the occurrence of the initiating event. The period of time of interest represents the time interval for which the ENF for the accident sequence must be computed. The period of time of interest arbitrarily starts at 0 and ends at time t . Figure II.3 illustrates the time sequence for the occurrence of an accident sequence. The top event occurs at t'' , $t' \leq t'' \leq t'+T$.

Occurrence of the initiating event does not necessarily result in the occurrence of the top event. For example, if any one of the n system failures $\bar{S}_1, \bar{S}_2, \bar{S}_3, \dots, \bar{S}_n$ does not occur in $(t', t'+T)$,

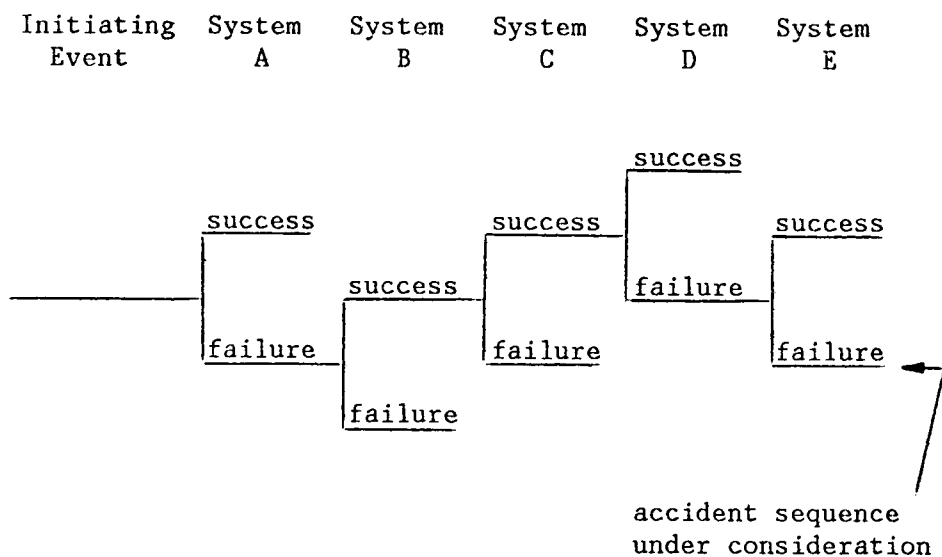


Figure II.1 A Generic Accident Sequence. For this sequence to occur, system A must fail ($\bar{S}_1$), systems B and C must operate, system D must fail ($\bar{S}_2$), and system E must fail ($\bar{S}_3$).

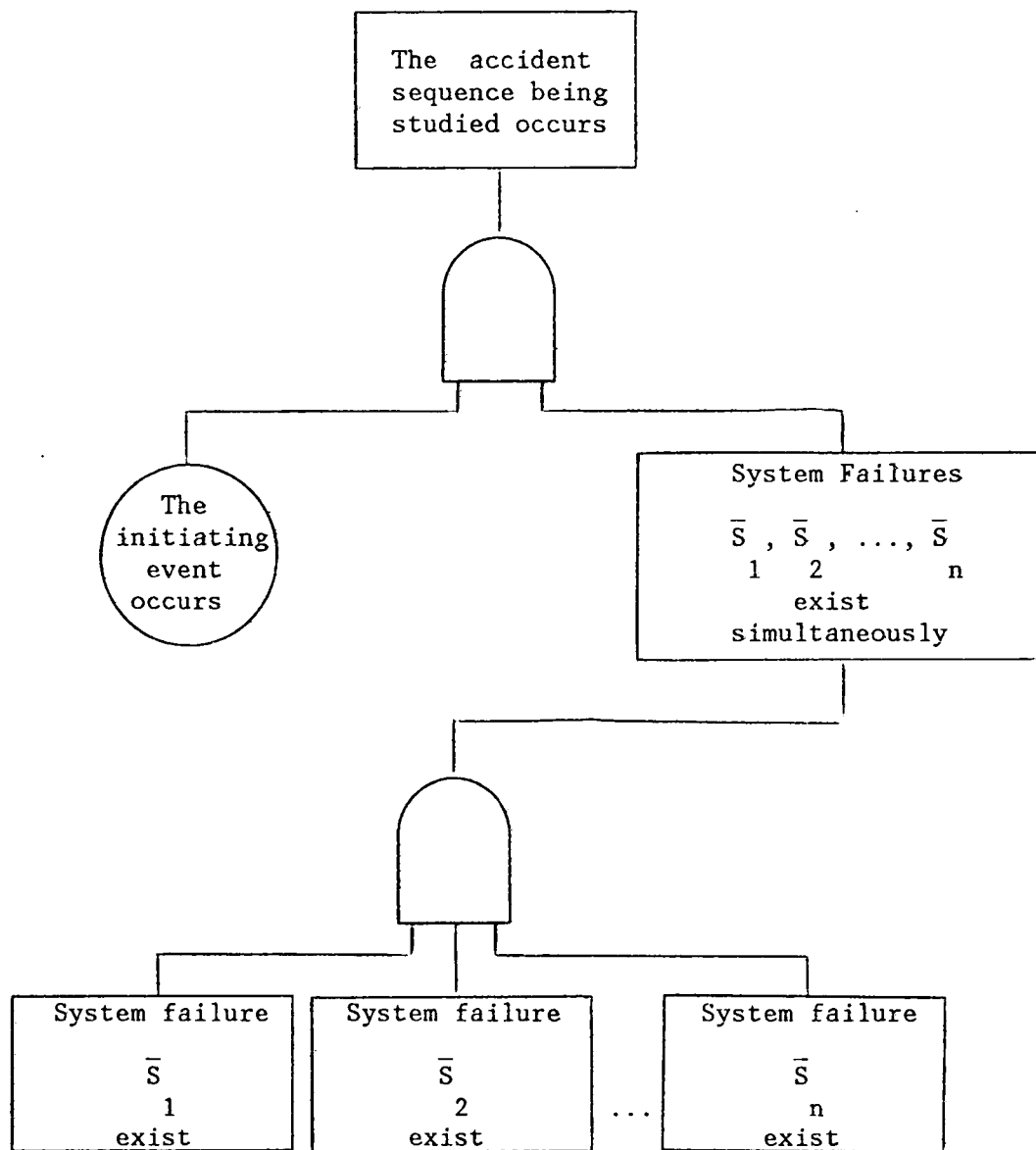


Figure II.2 Fault Tree for a Generic Accident Sequence in an Event Tree.

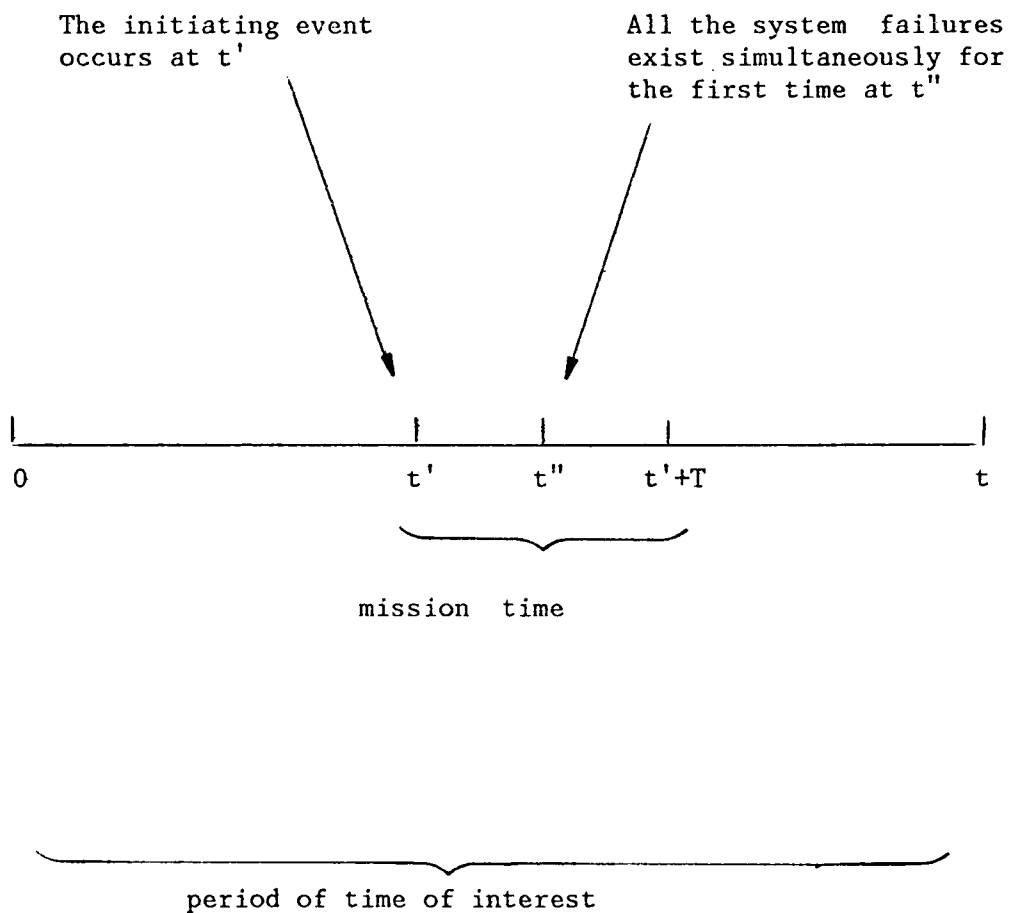


Figure II.3 A Diagram Illustrating the Time Sequence for the Occurrence of an Accident Sequence. The initiating event occurs at t' . The top event occurs at t'' .

the top event does not occur. Also, they may all occur but not simultaneously. The top event does not occur in this case either. In these cases, the accident sequence under consideration does not happen. Therefore, there is a probability that the accident sequence will occur following the occurrence of the initiating event.

The probability mentioned above clearly equals the probability that $\bar{S}_1, \bar{S}_2, \bar{S}_3, \dots, \bar{S}_n$ exist simultaneously any time between t' and $t'+T$. It represents the probability that the situation described in Figure II.3 happens. It is defined as the time-dependent undependability of the accident sequence, and it is represented by $\bar{d}_{AS}(t', t'+T)$. The undependability depends on the probabilistic parameters of the systems involved and on the nature of the problem as well. The variable $d_{AS}(t', t'+T) = 1 - \bar{d}_{AS}(t', t'+T)$ represents the probability that the accident sequence does not occur following the existence of the initiating event. The term "dependability" labels this probability.

A definition of undependability, as presented above, includes all the system failures in the accident sequence. A similar definition applies for each system involved. The system time-dependent undependability, represented by $\bar{d}_{Si}(t', t'+T)$ for system i , is here defined as the probability that the system will fail in the time interval $(t', t'+T)$ following the occurrence of the initiating event at t' . T represents the average time that system i must operate following the occurrence of the initiating event.

The undependabilities defined above depend on the nature of the systems and on the particular problem. In general, they have two

components. One, here defined as the time-dependent unavailability, represents the probability of the accident sequence's (system's) failure to start. A second component represents the probability of the accident sequence's (system's) failure to run given that it has started properly. In this work, the term "unreliability" labels this component of the accident sequence (system) undependability. Fault trees, or any other reliability failure model, for the two components of the undependability may differ from each other.

A complex relationship exists between the system's undependability and the accident sequence's undependability. For example, if at least one of the systems is dependable, the accident sequence is dependable. But the accident sequence may still be dependable even if all the systems involved are undependable. This situation arises when all the system failures exist in $(t', t'+T)$ but not simultaneously.

II.3 AN EXPRESSION FOR THE ACCIDENT SEQUENCE'S UNDEPENDABILITY

Section II.1 showed how to obtain $ENF(0, t)$ as a function of the accident sequence undependability. This section presents the derivation of an expression to compute the accident sequence undependability as a function of the undependabilities of the system failures in the accident sequence.

As mentioned in Section II.2, a complex relationship exists between the system undependability and the accident sequence undependability. Suppose, as an example, that an accident sequence includes a Core Cooling System (CCS) failure and a Containment

Pressure Reduction System (CPRS) failure. Suppose also that a CCS failure results in core meltdown and a high pressure condition. In this example, if the CPRS fails before the CCS failure, it could be repaired and returned to work without the occurrence of the accident sequence (release of radioactive material in the environment). If the CCS failure occurs first, however, a high-pressure condition will exist. In this second case, if the CPRS fails, the accident sequence occurs (assuming a containment failure under high-pressure conditions). In the first case, an equation for the accident sequence undependability would assume that the CPRS is a repairable system. In the second case, the CPRS must be considered a nonrepairable system. The probability of the occurrence of the accident sequence must then be conditioned on the time sequence of the system's failures, which considerably increases the computational effort needed to solve the problem.

The fault trees representing the repairable system's failures may be combined through an AND gate to form a larger fault tree (the smaller trees are said to be "ANDed" together). If the larger fault tree is assumed to be nonrepairable (a conservative assumption), the complexity described in the last paragraph will no longer exist. Alternatively, the assumption of nonrepairability may be made on each of the repairable system's failures or on combinations of such system's failures. In these cases, the results are more conservative than in the case previously described. The advantage of making these assumptions on each system or groups of systems is that the number of MCSs does not grow to unmanageable sizes.

This dissertation assumes that one of the alternatives explained in the last paragraph is taken. The accident sequence then becomes a combination of nonrepairable system's failures. These system's failures are represented by $\bar{S}_1, \bar{S}_2, \dots, \bar{S}_n$. The accident sequence undependability becomes

$$\begin{aligned} \bar{d}_{AS}(t', t'+T) &= P(\bar{S}_1 \bar{S}_2 \dots \bar{S}_n) \\ &= P(\bar{S}_1) \cdot P(\bar{S}_2 | \bar{S}_1) \dots P(\bar{S}_n | \bar{S}_1 \bar{S}_2 \dots \bar{S}_{n-1}). \quad (2.5) \end{aligned}$$

Dependencies among the system's failures result from the system's fault trees sharing common basic events. Two approaches are proposed here to account for these dependencies in the computation of the conditional probabilities in Equation 2.5.

First, Equation 2.5 may be conditioned on the occurrence and nonoccurrence of each of the shared basic events. This approach is essentially the approach used in the computer program FRANCALC,²³ as explained in Chapter I (see Equation 1.1 on page 17). This first approach is accurate but greatly increases the computational effort to solve the problem (if there are k common basic events, the computational effort may be increased by as much as 2^k times). Therefore, this approach should be applied only to those common basic events that have a significant effect on the system's failure probabilities (e.g., common basic events which appear in MCSs with only one basic event). For the other common basic events, a second approach is proposed as explained in the remainder of this section.

For the second approach, define $\bar{S}_i^*$ as the event system's failure i occurs in $(t', t'+T)$ given the existence of all the basic events in the fault trees for $\bar{S}_1, \bar{S}_2, \dots, \bar{S}_{i-1}$ that also appear in the fault tree for $\bar{S}_i$. The following relations result from this definition:

$$P(\bar{S}_i^*) \geq P(\bar{S}_i | \bar{S}_1 \bar{S}_2 \dots \bar{S}_{i-1}) \geq P(\bar{S}_i). \quad (2.6)$$

Therefore, upper and lower bounds for the accident sequence undependability are given by the following equations:

$$\prod_{i=1}^n P(\bar{S}_i^*) \geq \bar{d}_{AS}(t', t'+T) \geq \prod_{i=1}^n P(\bar{S}_i). \quad (2.7)$$

The ASA computer program uses the upper bound in Equation 2.7 to provide an estimate of the accident sequence's undependability. If the fault trees representing the system's failures have no common basic events, then $P(\bar{S}_i^*) = P(\bar{S}_i)$ for all i , and Equation 2.7 becomes an equality on both sides.

In computing the upper bound in Equation 2.7, the order in which the system failures are considered in the analysis becomes relevant. Although any order will give conservative estimates, the order which produces the smallest value is the most desirable one. A few simple examples were investigated in this study to determine the proper system ordering to produce the smallest upper bound in

Equation 2.7. These examples indicated that the proper ordering depends on the basic event Fussell-Vesely importance. This measure of importance is defined as the probability that the basic event exists given that the top event exists. The examples were restricted to simple systems with nonrepairable basic events. Further research is necessary to provide a general approach to the proper system ordering.

Equation 2.7 provides an upper bound to the accident sequence undependability as a function of $P(\bar{S}_i^*)$, which is given by

$$P(\bar{S}_i^*) = \bar{a}_{Si}^*(t') + \int_{t'}^{t'+T} f_{Si}^*(t''-t';t') dt'', \quad (2.8)$$

where the definitions of $\bar{a}_{Si}^*(t')$ and $f_{Si}^*(t''-t';t')$ are the same as those used in Equation 2.2 but applied for system i . In addition, the superscript "*" indicates the condition defined for the event $\bar{S}_i^*$. The next section shows how to obtain $P(\bar{S}_i^*)$ as a function of the basic event unavailabilities.

II.4 AN EXPRESSION FOR THE SYSTEM UNDEPENDABILITY

The last section derived an equation relating the accident sequence undependability to the system undependabilities. This section derives an equation for the system undependabilities as a function of the basic event unavailabilities. Section II.5 shows the computation of the basic event unavailabilities from the basic data, which are assumed available.

The superscript "*" implies that a basic event in system i is unavailable if it also appears in any one of the previous systems $(1, 2, \dots, i-1)$. This section assumes that this condition has already been satisfied before the analysis actually begins. In the ASA computer program, this is achieved by using a subroutine called PREPAR, which simply deletes all such basic events from the MCSs previously to any computation.

The Kinetic Tree Theory (KTT) provides an exact analytical solution to $\bar{a}_{Si}^*(t')$. Consider an accident sequence with 'm' MCSs. Equation 40 in reference 89 gives the following expression for $\bar{a}_{Si}^*(t')$:

$$\bar{a}_{Si}^*(t') = \sum_{r=1}^m (-1)^{r+1} \sum_{\substack{i_1 < i_2 < \dots < i_r \\ 1 \leq i_1 < i_2 < \dots < i_r}} \prod_{j=+1, \dots, r} \bar{a}_j(t'), \quad (2.9)$$

where:

$\bar{a}_j(t')$ is the basic event j unavailability.

$\prod_{j=+1, \dots, r}$ is the product of unique basic event quantities where the basic event appears in at least one of the MCSs $1, \dots, r$.⁸⁹

$\sum_{i_1 < i_2 < \dots < i_r}$ is taken over all of the $\binom{m}{r}$ possible subsets of the set $(1, 2, \dots, m)$. This definition appears in reference 73.

For $r=1$, $i=i$, and the summation over all the $\binom{m}{r}$ possible subsets of the set $(1,2,\dots,m)$ becomes the summation of all the MCSs' unavailabilities. The MCSs' unavailabilities are given by the simple product of the unavailabilities of the basic events in each MCS.

When $r=2$, the probabilities of two MCSs being unavailable at t' are added together. Since $r+1=3$ (odd), this term is subtracted from the first term. When $r=3$, the summation is over the MCSs taken three at a time, and so forth.

The second term on the right-hand side of Equation 2.8 involves the integral of the probability density function of the time to first system failure. An exact solution to this integral "is incalculable analytically except in exceedingly simple cases" (Murchland).⁶³ This integral, however, is bounded by the expected number of system failures in $(t', t'+T)$, given no system failure to start at t' .⁶³ As expressed by Clarotti,¹⁸ insofar as reliable systems are considered, no important numerical difference exists between the upper bound and the exact solution. Thus, this dissertation adopts the upper bound mentioned above as the approximation to the integral in Equation 2.8.

The remainder of this section presents the development of an equation for the computation mentioned above. The basis of this approach has been developed by Vesely.⁸⁹

A system failure occurs in dt if it does not exist at t and if " r " of the system's MCSs occur in dt , $1 \leq r \leq m$. The probability that a basic event fails in an infinitesimal interval dt is

proportional to dt'' . Thus, the probability that two or more basic events fail simultaneously in dt'' is zero. Therefore, r MCSs may occur in dt'' if and only if there exists at least one basic event that appears in all the r MCSs. Suppose that there are " l " such basic events. If $l=0$, the MCSs cannot all fail simultaneously in dt'' . If $l>0$, the MCSs can fail simultaneously in dt'' only under the following conditions:

1. One of the l common basic events must be available at t'' and must fail in dt'' . This will occur with a probability of $(1-\bar{a}_i(t'')) h_i(t'') dt''$,

where

$i = 1, 2, \dots, l$ represents one of the l common, basic events,

$1-\bar{a}_i(t'')$ is the probability that the i basic event is available at t'' , and

$h_i(t'')$ is the conditional probability of the basic event i failure in dt'' , given working at t'' (the basic event failure or hazard rate).

2. All the remainder basic events in the r MCSs must be unavailable at t'' , with probability given by

$\prod_{\substack{j=+1, \dots, r \\ j \neq i}} \bar{a}_j(t'')$ the definition of this symbol appears in Equation 2.9.

3. The system failure does not exist at time t'' , given the conditions in (1) and (2) above. Let P_i represent the probability of such condition.

From the above, the following expression results:

$$\begin{aligned}
 & \text{system failure} \\
 & \text{occurs in } dt'' \\
 & p(\text{ due to the occurrence }) \\
 & \text{ of one specific} \\
 & \text{ combinations of } r \text{ MCSs} \\
 & = \sum_{i=1}^1 P_i (1 - \bar{a}_i(t'')) h_i(t'') dt'' \prod_{\substack{j=+1, \dots, r \\ j \neq i}} \bar{a}_j(t'') , \quad (2.10)
 \end{aligned}$$

The summation over i accounts for all the common basic events in the r MCSs. A system failure does not exist at time t'' if and only if at least one of its MPSs is up at t'' . A MPS is up at t'' if all of its basic events do not exist at t'' . Therefore, P_i is the probability that at least one MPS is up at t'' given the conditions (1) and (2). To account for the conditions (1) and (2) in the computation of P_i , the following facts are considered:

4. Any MPS must contain at least one basic event from each MCS. Thus, any MPS must contain at least one basic event in the set of basic events which appear at least once in the r MCSs. If the MPS contains more than one such basic event, then it must be down at t'' and does not contribute to P_i . This results from the conditions (1) and (2).

5. If an MPS contains only one basic event in the set of basic events which appear at least once in the r MCSs, two possibilities remain: the basic event exists at t'' , or the basic event does not exist at t'' . In the first case, the MPS again cannot contribute to P_i . Therefore, only the MPSs which contain the basic event 'i' in (1) may contribute to P_i . In addition, the MPS containing 'i' should not contain any of the other basic events which appear in the set of the r MCSs. Thus,

$$P_i = \sum_{s=1}^{g_i} (-1)^{s+1} \sum_{\substack{j_1 < \dots < j_s \\ j \neq i}} \prod_{j=1}^s \overline{a_j}(t'') \quad (2.11)$$

where,

$\overline{a_j}(t'')$ is the basic event j unavailability where basic event j appears in at least one of the MPSs $j_1, \dots, j_s$.

g_i is the number of MPSs which contain the basic event i (as defined in item (1) above) and do not contain any other basic event in the set of basic events which appear at least once in the r MCSs.

$\sum_{\substack{j < j_1 < \dots < j_s \\ 1 \quad 2 \quad s}}$
 is taken over all the $\binom{g}{s}$ possible subsets of the set $(1, \dots, g)$. The definition of this symbol appears in reference 73.

Therefore, except for the basic event unavailabilities, Equation 2.10 has been completely defined. It applies to the computation of the probability that the system failure will occur in dt'' due to the occurrence of one specific combination of r MCSs. There are $\binom{m}{r}$ combinations of m MCSs taken r at a time. Then,

$$p(\text{system failure occurs in } dt'' \text{ due to the occurrence of } r \text{ MCSs in } dt'') = \sum_{\substack{i < i_1 < \dots < i_r \\ 1 \quad 2 \quad r}} (\text{Equation 2.10}).$$

Finally, adding the contributions from all possible r 's,

$$f_{Si}(t'' - t'; t') dt'' =$$

$$\sum_{r=1}^m (-1)^{r+1} \sum_{\substack{i < \dots < i_r \\ 1 \quad r}} (\text{Equation 2.10}). \quad (2.12)$$

Thus, given the basic event unavailabilities at t' and t'' , the ENF for the accident sequence can be calculated using Equations 2.8, 2.9, and 2.12. The next section shows how to evaluate the basic event unavailabilities.

II.5 THE BASIC EVENT UNAVAILABILITIES

The methodology developed in this dissertation allows the analysis of the accident sequences as a function of the basic event unavailabilities as shown in the preceding sections. This section presents the basic event unavailability equations implemented in the ASA computer program. For the basic event probabilities of failure to start, the equations used here are the ones used in the FRANTIC and the FRANCALC codes. The program includes four types of basic events:

1. Constant Unavailability (CU) basic events,

$$\bar{a}_{CU}(t') = \text{constant}, \quad 0 \leq t' \leq t, \quad (2.13)$$

which is called the "per demand unavailability" or the "cyclic unavailability."

2. Nonrepairable (NR) basic events,

$$\bar{a}_{NR}(t') = h t', \quad (2.14)$$

where h is the failure rate (a constant). The nonrepairable basic events can also have a cyclic unavailability contribution.

3. Constantly Monitored (CM) basic events,

$$\bar{a}_{CM}(t') = h T_R, \quad (2.15)$$

where h is the failure rate (a constant) and T_R represents the average detection plus repair time. The ASA program also allows the constantly monitored basic events to have a cyclic unavailability contribution.

4. Periodically Tested (PT) basic events.

This type of basic event has its unavailability given by three equations, one for each time period as follows:

4.1 Basic event undergoing test,

$$\bar{a}_{PT}(t') = p_f + (1-p_f) q_o + (1-p_f)(1-q_o) Q_o \quad (2.16)$$

4.2 Basic event undergoing repair,

$$\bar{a}_{PT}(t') = p_f + (1-p_f) Q_f + (1-p_f)(1-Q_f) \frac{1}{2} h T_R \quad (2.17)$$

4.3 Basic event on standby,

$$\bar{a}_{PT}(t') = h (t_{pt} - \text{Tau}) \quad (2.18)$$

where

t_{pt} = the time from the preceding test,
 T_1 = first test interval,
 T_2 = test interval,
 Tau = test period (duration),
 T_R = repair period,

$$\begin{aligned}
 p &= \text{probability of a test caused failure,} \\
 f & \\
 q &= \text{probability of not overriding a test} \\
 o & \\
 &\text{if a demand occurs, and} \\
 Q &= h (T - \tau). \\
 &\quad 2
 \end{aligned}$$

During the first test interval T , Equation 2.18 is modified to $\bar{a}(t') = h_1 t'$, and Q is given by $h_1 T$. To account for periodic test inefficiencies, h in the above equations is substituted by $h(1-p)$, and hpt (the undetected contribution) is added to those equations. The periodically tested basic events may also have a cyclic unavailability contribution.

Following the occurrence of the accident sequence at t' , all of the basic events have a probability of being failed or a probability of failing on demand (cyclic unavailability) as given in the equations above. In order to solve the equations in Section II.4, however, the basic event unavailabilities at time t'' , $t' \leq t'' \leq t' + T$, are also required. For Type I basic events,

$$\bar{a}(t'') = a(t') = \text{constant.} \quad (2.19)$$

For Type II basic events, the ASA computer program has two possibilities currently implemented. The basic event may be nonrepairable, with constant failure rate h , or the basic event may be repairable, with constant failure and repair rates given by h and μ , respectively. The repair rate μ is defined as the conditional probability of the basic event being repaired in dt'' per unit time, given that it was failed at t'' .

For the repairable case, an expression for the basic event unavailability results from a probabilistic balance. The basic event is failed at $(t'' + \Delta t'')$ if it was failed at t'' and was not repaired in $\Delta t''$ at t'' , or if it was not failed at t'' and failed in $\Delta t''$. Mathematically speaking, with $P(t'')$ representing the unavailability at t'' ,

$$P(t'' + \Delta t'') = P(t'') (1 - \mu \Delta t'') + (1 - P(t'')) h \Delta t'' .$$

Rearranging this equation,

$$\frac{P(t'' + \Delta t'') - P(t'')}{\Delta t''} = - (h + \mu) P(t'') + h ,$$

and taking the limit as $\Delta t''$ goes to zero,

$$\frac{dP(t'')}{dt''} = h - (h + \mu) P(t'') ,$$

which has the following solution:

$$P(t'') = \bar{a}_{CM}(t'') = \frac{h}{h + \mu} + \left(\bar{a}(t') - \frac{h}{h + \mu} \right) \exp(-(h + \mu)(t'' - t')) . \quad (2.20)$$

12

By applying the renewal theory, Caldarola¹² has developed the equation above for two limiting cases, $\bar{a}(t')=0$ and $\bar{a}(t')=1$. For these limiting cases, the equation above agrees with the previous result.

For the nonrepairable case, the basic event unavailability is obtained from equation 2.20 by simply setting $\mu=0$:^{18,63}

$$\bar{a}_{NR}(t'') = 1 - (1 - \bar{a}(t')) \exp(-h(t'' - t')), \quad (2.21)$$

which applies for constant h . For time-dependent failure rates, the definition of h should be changed to the conditional probability of failure in dt'' per unit time, given no failures in the interval $(t', t'' - t')$ (rather than given working at t''). This theoretically important modification was pointed out by Murchland⁶³ and further clarified by Clarotti.¹⁸

II.6 THE ASA COMPUTER PROGRAM

The ASA computer program allows the practical application of the methodology developed in this dissertation. The code contains the main program, ten subroutines, and five function subroutines. It is written in FORTRAN and contains approximately 3,300 source statements, about 40% of which are comment lines providing adequate internal documentation of the algorithms used. The next paragraphs describe each of the following routines:

Main Program
START

PREPAR
TIMES
UNDEPE
BASIC1
BASIC2
CUTS
PATHS
RECKON
ROFIE
Functions: FNRA, FNRE, FCMA, FCME and FPTA.

Subroutine START reads and analyzes all the input data, printing part of the input data for checking purposes. Several checks are performed, and messages are given in case of errors.

Subroutine PREPAR has two functions. First, if specified by the user, it will eliminate from a fault tree all the basic events in this fault tree which also appear in any of the preceding fault trees in the accident sequence. In doing so, the program evaluates the upper bound given by Equation 2.7 (page 46). It then identifies the MCSs which represent a failure-to-start only as well as the number of such MCSs.

The main program controls the evaluation of Equation 2.1 (page 35). It calls subroutines START and PREPAR and then computes the integration intervals to numerically integrate Equation 2.8 (page 47). Subroutine TIMES is called several times by the main program to determine the times at which the integrand in Equation 2.1 experiences a discontinuity. The numerical integration of Equation 2.1 can be performed using Simpson's rule, the trapezoidal rule, or the rectangular rule, depending on the user specifications. The computation of the integrand in Equation 2.1 is accomplished by calling ROFIE, BASIC1 and UNDEPE, as described later in this section.

Subroutine TIMES, when called for the first time, will identify all the times at which the unavailability of any of the basic events in the accident sequence experiences a discontinuity. It then stores all such times points in a vector for later use. In subsequent calls, this subroutine will provide such information to the main program.

Subroutine UNDEPE controls the computation of the time-dependent undependability (Equation 2.8--page 47) for each system in the accident sequence. This is accomplished by calling CUTS and RECKON and by performing a numerical integration on the results of RECKON using Simpson's rule. CUTS calculates the probability of an accident sequence's failure to start on demand (Equation 2.9--page 48). RECKON computes the probability of an accident sequence failure-to-run at a time during the mission, given a demand and a successful start (Equation 2.12--page 53). PATHS calculates Equation 2.11 (page 52).

Subroutine BASIC1 controls the computation of the basic event unavailabilities at the time of the demand. For each basic event, it selects the proper equation from those in Section II.5. Subroutine BASIC2 controls the computation of the basic event unavailabilities during the mission, conditioned on the basic event unavailabilities at the time of the demand (computed by BASIC1). For each Type I basic event, BASIC2 selects one of the two currently available equations applicable to nonrepairable or to constantly monitored basic events (Equations 2.21 and 2.20 -- pages 58 and 57).

The subroutine ROFIE calculates the rate of failure, or the frequency of occurrence, of the initiating event as a function of time. It performs a linear interpolation between the data points provided by the user. ROFIE is not called if the initiating event has a constant rate of failure.

Several functions are available for the computation of the basic event unavailabilities. They are used in subroutines BASIC1 and BASIC2. The listing of the ASA code in Appendix D includes a detailed description of each function. These functions apply to the following Equations in Section II.5:

FNRA	Equation 2.14 (page 54)
FNRE	Equation 2.21 (page 58)
FCMA	Equation 2.15 (page 54)
FCME	Equation 2.20 (page 57)
FPTA	Equation 2.16, 2.17, and 2.18 (page 55).

Checking the ASA computer program included three steps: (1) reviews of the code, (2) runs of simple problems which could also be solved by hand calculations, and (3) runs of example problems available in the literature. Several problems were selected from the literature, including one example by Fussell; ³⁵ four examples by Elerath, Vaurio, and Wood; ²³ and sixteen examples by Vesely and ⁹⁴ Goldberg. The examples problems selected from the available literature represent limiting cases for the capability of the ASA computer program. Therefore, these examples problems were used to

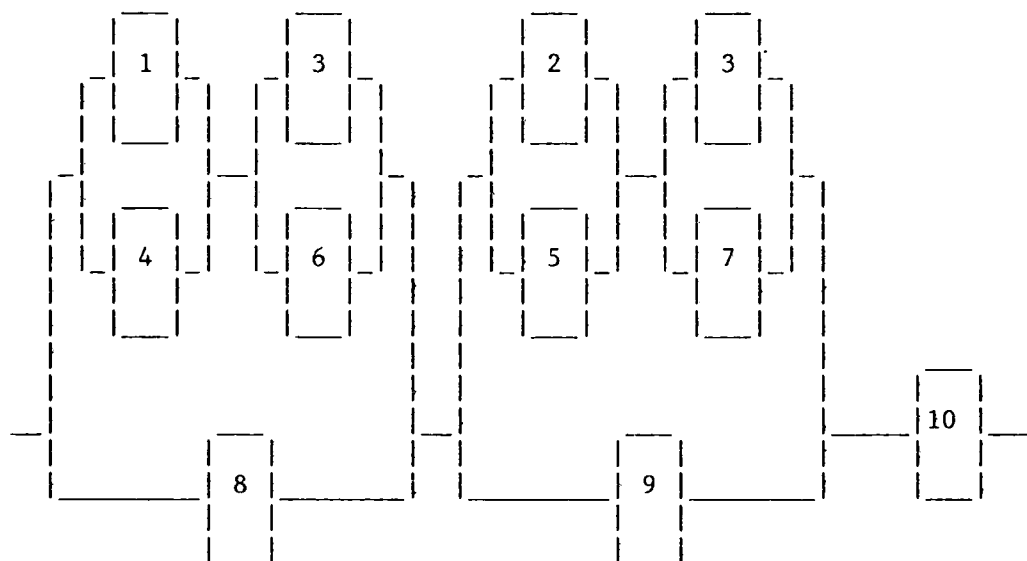
check different portions of the ASA code. For example, the agreement of the results given by ASA and the results obtained by Vesely and Goldberg provides a check of the main program; subroutines START, TIMES, UNDEPE, BASIC1, and CUTS; and some of the function subroutines. The agreement with the results presented by Fussell, on the other hand, provides checking of subroutines RECKON and BASIC2, and the function subroutine FCME. The examples by Elerath, Vaurio, and Wood required the use of most of the ASA computer program, providing a more general test of the ASA code and methodology.

Those portions of the code necessary to reproduce the examples from the literature have been comprehensively checked by the three methods mentioned above. The portions of the computer program which were not used for the examples above (less than 20% of the code) have been reviewed only. The listing of the ASA computer program in Appendix D includes comment cards which give more detailed information about the code.

II.7 APPLICATION OF THE ASA COMPUTER PROGRAM

This section presents the application of the ASA computer program to the Shutdown Heat Removal System (SHRS) analyzed by Elerath, Vaurio, and Wood.²³ Only the initiating event "One-month shutdown for refueling" is illustrated here. Figure II.4 shows the failure block diagram applicable for this accident initiator.

It is clear that the DRACS is the only independent path to successfully remove the decay heat. The other paths have at least one basic event which also appears in a different path. Thus, the



- | | |
|----|---|
| 1 | Diesel Generator 1 |
| 2 | Diesel Generator 2 |
| 3 | Offsite Power |
| 4 | Intermediate Reactor Auxiliary Cooling System 1 |
| 5 | Intermediate Reactor Auxiliary Cooling System 2 |
| 6 | Steam Loop 1 |
| 7 | Steam Loop 2 |
| 8 | Sodium System in Loop 1 |
| 9 | Sodium System in Loop 2 |
| 10 | Direct Reactor Auxiliary Cooling System (DRACS) |

Figure II.4 Failure Block Diagram: Shutdown Heat Removal System.

accident sequence may be analyzed by assuming two major systems, the DRACS (with only one basic event) and the system formed by deleting basic event 10 from the diagram presented in Figure II.4.

The Sodium Loops (basic events 8 and 9) and the Offsite Power (basic event 3) are also reactor shutdown initiators and, therefore, must be available at the time of the shutdown for refueling. The input data for each basic event is shown in Appendix B for the case of staggered testing. The input to the ASA computer program appears in Appendix B, and the output appears in Appendix C.

Two cases are considered in this section. In Case 1, the basic events are assumed to be nonrepairable during the mission, which corresponds to the approach currently available in the literature. Appendixes B and C refer to this case. In Case 2, all the basic events are assumed to be constantly monitored during the mission, except for the DRACS, which is a nonrepairable system. In this second case, the same repair data given for the predemand period have been used for the postdemand period. Figure II.5 shows the time-dependent undependabilities for the two cases at the time points shown in Table II.1.

The undependabilities show large discrepancies. This discrepancies result because the probability of an accident sequence failure to run is greatly overpredicted when using the existing approach. The ASA program gives the following values for the ENF in these two cases:

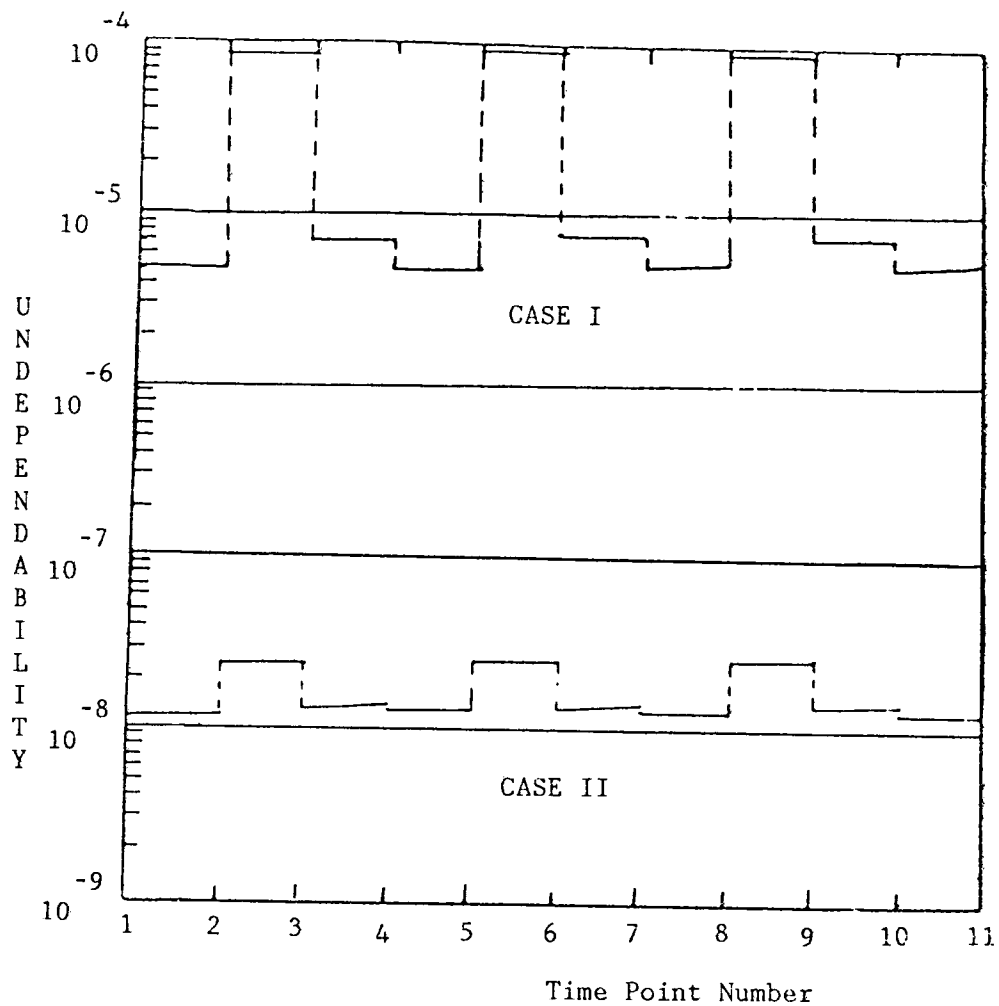


Figure II.5 Accident Sequence Undependability for Cases I and II.

Table II.1 Point Numbers Used in Figure II.5

Point Numbers	Time (hours)
1	7356
2	7665
3	7673
4	7721
5	8030
6	8038
7	8086
8	8395
9	8403
10	8451
11	8760

	CASE 1	CASE 2
Expected		
Number of	-8	-11
Accident	4.17×10	7.67×10
Sequence		
Occurrences		
in One Year		

This example illustrates the necessity of the methodology developed in this dissertation. This example agrees with the comments by Fussell,³⁵ which state that a large overprediction results when there is a large degree of redundancy and when the basic event average repair times are small with respect to the corresponding mean times to failure.

CHAPTER III

SUMMARY, CONCLUSIONS, AND RECOMMENDATIONS

This report presents the development of a methodology to calculate the Expected Number of Failures (ENF) for each accident sequence in an event tree, where fault trees are available for each branching point in the event tree. The methodology evaluates the average and the time-dependent behavior of a generic accident sequence, allowing a detailed modeling of periodic testing and repair. The analysis includes the probability of system failure to start and the probability of system failure to run following a successful start. The method developed here applies to repairable and to nonrepairable components in the accident sequence. In particular, it allows the study of systems with components that may be repaired during the mission. The following assumptions have been adopted in this work:

1. The fault trees representing the system's failures at each branching point in the event tree are
27
coherent.
2. The basic events in the fault trees are statistically independent in failure and repair.
3. The expected number of accident sequence occurrences during the mission is used to provide a conservative upper bound to the mission unreliability (the probability that the system formed by all the systems

in the accident sequence starts and fails to perform adequately during the mission).

4. The repairable systems in the accident sequence or combinations of such systems are assumed to be nonrepairable during the mission (a conservative assumption).

A computer program called ASA (an acronym for Accident Sequence Analysis) allows the practical implementation of the theory developed. It consists of a main program, ten subroutines, and five functions. Checking the ASA computer program included reviews of the code, runs of simple problems which could also be solved by hand calculations, and runs of examples problems available in the literature.

A potential problem has been identified during the course of this study. It refers to the computation of the probability of occurrence of the intersections of two or more MCSs. Two alternative approaches have been identified to solve this potential problem. One possibility consists of using disjoint product methods such as the Sigma Pi method.¹⁹ This approach is general and exactly calculates the probability of occurrence of a system failure during the mission time, under the assumptions listed above. The second alternative consists of evaluating only the intersections of MCSs containing high-unavailability basic events with the remaining MCSs.

The work presented here is a required extension of the presently available methodology and allows a more realistic PRA of

nuclear power plants. It also expands the techniques of reliability analysis as applied to large, complex systems such as those in the nuclear and chemical industries. The following improvements are suggested for further work in this area:

1. The application of the methodology developed here to a nuclear power reactor. This application may reveal problem areas and provide guidelines for future studies.
2. The interfacing of the time-dependent methodology developed here with the existing phased-mission³⁹ methodology.
3. The generalization of the equations used to calculate^{20,87} the basic event unavailabilities.
4. The investigation of the proper system ordering in the accident sequence that will produce the smallest upper bound to the accident sequence's ENF.
5. The investigation of the possibility of using the methodology developed here to analyze systems for which the fault trees for failure to start and failure to run have different structures.

LIST OF REFERENCES

LIST OF REFERENCES

1. Apostolakis, G., "Probability and Risk Assessment: The Subjectivistic Viewpoint and Some Suggestions," Nuclear Safety 19, pp. 305, 1978.
2. Apostolakis, G., Garribba, S. and Volta, G., eds., "Synthesis and Analysis Methods for Safety and Reliability Studies," Plenum Press, New York, 1980.
3. Atwood, C.L. and Steverson, J.A., "Common Cause Fault Rates for Diesel Generators: Estimates Based on Licensee Event Reports at U.S. Commercial Nuclear Power Plants, 1976-1978," NUREG/CR-2099, EGG-EA-5359, Revision 1, 1982.
4. Atwood, C.L., "Common Cause Fault Rates for Pumps," NUREG/CR-2098, EGG-EA-5289, EG&G Idaho, Inc., February 1983.
5. Atwood, C.L. and Steverson, J.A., "Common Cause Fault Rates for Valves," NUREG/CR-2770, EGG-EA-5485, EG&G Idaho, Inc., February 1983.
6. Atwood, C.L. and Meachum, T.R., "Common Cause Fault Rates for Instrumentation and Control Assemblies," NUREG/CR-3289, EGG-EA-2258, Idaho National Engineering Laboratory, EG&G Idaho, Inc., May 1983.
7. Baranowsky, P.W., Kolaczowski, A.M., and Fedele, M.A., "A Probabilistic Safety Analysis of DC Power Supply Requirements for Nuclear Power Plants," NUREG-0666, April 1981.
8. Barlow, R.E., Fussell, J.B. and Singpurwalla, N.D., "Reliability and Fault Tree Analysis," SIAM, Philadelphia, 1975.
9. Barlow, R.E. and Proschan, F., "Statistical Theory of Reliability and Life Testing," Holt, Rinehart and Winston, New York, 1975.
10. Barlow, R.E. and Proschan, F., "Theory of Maintained Systems: Distribution of Time to First System Failure," Mathematics of Operations Research, Vol. 1, pp. 32-42, February 1976.
11. Budnitz, R.J., "Methodology for Probabilistic Reactor Accident Analysis for External Initiators- Earthquakes, Fire, Floods, Winds," Future Resources Associates, Inc., Berkeley, California, Submitted to "Risk Analysis."
12. Caldarola, L., "A Method for the Calculation of the Cumulative Failure Probability Distribution of Complex Repairable Systems," Nuclear Engineering and Design, Vol. 36, pp. 109-122, 1976.

13. Campbell, D.J., "A Procedure for Determining the Importance of Basic Events to Systems Undergoing Phased Missions," Master's Thesis, NERS78-07, Department of Nuclear Engineering, University of Tennessee, December 1978.
14. Campbell, D.J. and Ellison, B.C., "Dependent Failure Analysis Procedures Guide," JBFA-105-83, JBF Associates, Inc., Knoxville, TN, June 1983.
15. Campbell, D.J. et al., "Common Cause Failure Analysis of Selected Accident Sequences at Arkansas Nuclear One- Unit 1," JBFA-104-83, JBF Associates, Inc., Knoxville, TN, September 1983.
16. Crooks, J.L. and Vissing, G.S., "Diesel-Generator Operating Experience at U.S. Nuclear Power Plants," USAEC, OOE-ES-002, June 1974.
17. Chow, David K., "Reliability of Some Redundant Systems with repair," IEEE Trans. Rel., Vol. R-22, No.4, pp.223-228, October 1973.
18. Clarotti, C.A., "Limitations of Minimal Cut-Set Approach in Evaluating Reliability of Systems with Repairable Components," IEEE Transactions on Reliability, Vol. R-30, No.4, October 1981.
19. Corynen, G.C., "Evaluating the Response of Complex Systems to Environmental Threats: The Sigma Pi Method," UCRL-53399, May 1983.
20. Dykes, A.A., "Application of Time Dependent Unavailability Analysis to Standby Safety Systems," Ph.D. Dissertation, Department of Nuclear Engineering, MIT, June 1982.
21. Edwards, G.T. and Watson, I.A., "A Study of Common-Mode Failures," Safety and Reliability Directorate, SRD R 146, U.K. Atomic Energy Authority, Wigshaw Lane, Culcheth Warrington, WA3 4NE, July 1979.
22. Elerath, J.G. and Ingram, G.E., "PROBCALC User's Manual: A Computer Program for Probability Calculation," GEFR-00408, General Electric Company, Sunnyvale, California, 1980.
23. Elerath, J.G., Vaurio, J.K., and Wood, A.P., "A Method for Reliability Analysis of Complex Reactor Systems," The ANS/ENS International Meeting on Fast Safety Technology, Lyon, France, July 1982.
24. "Loss of OffSite Power at Nuclear Power Plants: Data and Analysis," Electric Power Research Institute, EPRI NP-2301, March 1982.
25. "WAMCUT-II, A Fault Tree Evaluation Program," Electric Power Research Institute, EPRI NP-2421, June 1982.

26. "Recirculating Pump Seal Investigation," Electric Power Research Institute, EPRI NP-351, Vol. 1, December 1977.
27. Esary, J.D. and Proschan, F., "Coherent Structures of Nonidentical Components," Technometrics, Vol. 5, pp. 191-209, 1963.
28. Esary, J.D. and Marshall, A.W., "System Structure and the Existence of a System Life," Technometrics, 6, pp. 459-462, 1964.
29. Esary, J.D. and Proschan, F., "A Reliability Bound for Systems of Maintained Interdependent Components," J. American Statistical Association, vol 65, pp. 329-338, March 1970.
30. Fleming, K.N., Mosleh, A. and Kelly, Jr., A.P., "On the Analysis of Dependent Failures in Risk Assessment and Reliability Evaluation," Nuclear Safety, Vol. 24, No. 5, September-October 1983.
31. Fussell, J.B. and Vesely, W.E., "A New Methodology for Obtaining Cut Sets for Fault-Trees," Trans. American Nuclear Society, 15, 1972.
32. Fussell, J.B., "Synthetic Tree Model- A Formal Methodology for Fault Tree Construction," ANCR-1098, March 1973.
33. Fussell, J.B., "Fault Tree Analysis -- Concepts and Techniques," presented at the NATO Advanced Study Institute on Generic Techniques of System Reliability Assessment, Liverpool, England, July 1973.
34. Fussell, J.B., Henry, E.B. and Marshall, N.H., "MOCUS- A Computer Program to Obtain Minimal Cut Sets from Fault Trees," USAEC Rep. ANCR-1156, Aerojet Nuclear Company, August 1974.
35. Fussell, J.B., "How to Hand-Calculate System Reliability and Safety Characteristics," IEEE Transactions on Reliability, Vol. R-24, NO. 3, pp. 169-174, August 1975.
36. Fussell, J.B., "Fault Tree Analysis - Concepts and Techniques," in Generic Techniques in Systems Reliability Assessment (E.J. Henley and J.N. Lynn, eds.), pp. 133-162. Noordhoff, Leyden, 1976.
37. Fussell, J.B., et al., "SUPERPOCUS- A Computer Program for Calculating System Probabilistic Reliability and Safety Characteristics," NERS-77-01, Knoxville: Nuclear Engineering Department, May 1977.
38. Fussell, J.B. and Arendt, J.S., "System Reliability Engineering Methodology: A Discussion of the State of the Art," Nuclear Safety 20, pp. 541, 1979.

39. Fussell, J.B., et. al., "Phased-Mission System Reliability Analysis. Volume 1: Methodology," prepared by the University of Tennessee for the Electric Power Research Institute, EPRI NP-1945, Project 1233-2, July 1981.
40. Gately, W.Y. and Williams, R.L., "GO methodology- System Reliability Assessment and Computer Code Manual," Electric Power Research Institute, EPRI NP-766, May 1978.
41. Goldberg, H., "Extending the Limits of Reliability Theory," John Wiley & Sons, 1981.
42. Green, A.E. and Bourne, A.J., "Reliability Technology," New York: John Wiley and Sons, 1972.
43. Hatch, S.W., Cybulskis, P., and Wooton, R.O., "Reactor Safety Study Methodology Applications Program: Grand Gulf #1 BWR Power Plant," NUREG/CR-1659, SAND80-1897, Sandia National Laboratories, October 1981.
44. Henley, Ernest J. and Kumamoto, H., "Reliability Engineering and Risk Assessment," Englewood Cliffs, N.J.: Prentice-Hall, 1981.
45. Hubble, W.H. and Miller, C.F., "Data Summaries of Licensee Event Reports of Control Rods and Drive Mechanisms at U.S. Commercial Nuclear Power Plants," NUREG/CR-1331, EGG-EA-5079, EG&G Idaho, Inc., February 1980.
46. Spectrum, "A Special Issue: RELIABILITY," The Institute of Electrical and Electronics Engineers, Inc., Vol. 18, No. 10, October 1981.
47. "IEEE Guide to the Collection and Presentation of Electrical, Electronic, and Sensing Component Reliability Data for Nuclear-Power Generating Stations," IEEE Std 500-1977, Institute of Electrical and Electronics Engineers, Inc., Wiley-Interscience, June 1977.
48. "IEEE Guide to the Collection and Presentation of Electrical, Electronic, Sensing Component, and Mechanical Equipment Reliability Data for Nuclear-Power Generating Stations," IEEE Std 500-1984, Institute of Electrical and Electronics Engineers, Inc., Wiley-Interscience, 1984.
49. "In-Plant Reliability Data System (IPRDS) Interim Draft Report on the Reliability Characteristics of Selected Pumps in Four Nuclear Plants," NUREG/CR-2886, May 1982.
50. Kapur, K.C. and Lamberson, L.R., "Reliability in Engineering Design," John Wiley & Sons, Inc., 1977.

51. Knee, H.E., Krois, P.A., Haas, P.M., Siegel, A.I., and Ryan, T.G., "Maintenance Personnel Performance Simulation (MAPPS)- A Model for Predicting Maintenance Performance Reliability in Nuclear Power Plants," 11th Water Reactor Safety Information Meeting, National Bureau of Standards, Washington, D.C., October 24-28, 1983.
52. Kolb, G.J., Hatch, S.W., Cybulskis, P., and Wooton, R.O., "Reactor Safety Study Methodology Applications Program: Oconee #3 Laboratories, May 1981.
53. Kolb, G.J. et al., "Interim Reliability Evaluation Program: Analysis of the Arkansas Nuclear One- Unit 1 Nuclear Power Plant," NUREG/CR-1987, Sandia Laboratories, Albuquerque, New Mexico, June 1982.
54. Kreyszig, Erwin, "Advanced Engineering Mathematics," John Wiley & Sons, Fourth Edition, 1979.
55. Leverenz, F.L. and Kirch, H., "User's Guide for the WAM-BAM Computer Code," Electric Power Research Institute, EPRI-217-2-5, January 1976.
56. Leverenz, F.L., Jr., Koren, J.M., Erdmann, R.C., and Lellouche, G.S., "Electric Power Research Institute, ATWS: A Reappraisal, Part II Frequency of Anticipated Transients," EPRI NP-801, June 1978.
57. Levine, S. and Vesely, W.E., "Important Event-Tree and Fault-Tree Considerations in the Reactor Safety Study," IEEE Trans. Reliability, R-25, 132, 1976.
58. Lie, C.H., Hwang, C.L. and Tillman, F.A., "Availability of Maintained Systems: A State-of-the-Art Survey," AIIE Transactions, American Institute of Industrial Engineers, Inc., Volume 9, Number 3, September 1977.
59. McCormick, N.J., "Reliability and Risk Analysis Methods and Nuclear Power Applications," Academic Press, New York, 1981.
60. Miller, C.F. et al., "Data Summaries of Licensee Event Reports of Selected Instrumentation and Control Components at U.S. Commercial Nuclear Power Plants," NUREG/CR-1363, EGG-EA-5816, Revision 1, October 1982.
61. Miller, C.F. et al., "Data Summaries of Licensee Event Reports of Valves at U.S. Commercial Nuclear Power Plants from January 1, 1976 to December 31, 1980," EGG-EA-5816, April 1982.
62. Montague, D., "A Procedure for Determining the Expected Number of Failure of a Phased Mission," Master's Thesis, NERS-79-03, Department of Nuclear Engineering, The University of Tennessee, Knoxville, Tennessee, July 1979.

63. Murchland, J.D., "Comment on 'A Time Methodology for Fault Tree Evaluation'," Nuclear Engineering and Design, vol 22, pp 167-169, 1972.
64. Nielsen, D.S., "The Cause/Consequence Diagram Method as a Basis for Quantitative Accident Analysis," Danish Atomic Energy Commission, RISØ-M-1374, May 1971.
65. Nielsen, D.S. and Runge, B., "Unreliability of a Standby System with Repair and Imperfect Switching," IEEE Transactions on Reliability, Vol. R-23, No.1, April 1974.
66. "Nonelectric Parts Reliability Data," NPRD-2, Reliability Analysis Center, Rome Air Development Center, Griffiss Air Force Base, NY, Summer 1981.
67. "Nuclear Plant Reliability Data System (NPRDS) 1980 Annual Reports of Cumulative System and Component Reliability," NUREG/CR-2232.
68. Okrent, D., "Risk-Benefit Evaluation for Large Technological Systems," Nuclear Safety, Vol. 20, No. 2, March-April 1979.
69. Pacitti, T. and Atkinson, C.P., "Programação e Métodos Computacionais," (in Portuguese) Vols. 1 and 2, Livros Técnicos e Científicos Editora S.A., Brazil, 1977.
70. Peebles, Peyton Z., "Probability, Random Variables, and Random Signal Principles," McGraw-Hill, Inc., 1980.
71. Platz, O. and Olsen, J.V., "FAUNET: A Program Package for Evaluation of Fault Trees and Networks," Report RISØ-348, Danish Atomic Energy Commission, September 1976.
72. "PRA Procedures Guide," NRC Report NUREG/CR-2300, prepared under auspices of the American Nuclear Society and the Institute of Electrical and Electronics Engineers, April 1983.
73. Ross, Sheldon M., "A First Course in Probability," Macmillan Publishing Co., Inc., 1976.
74. Rowe, W.D., "An Anatomy of Risk," John Wiley & Sons, Inc., New York, 1977.
75. Rust, J.H. and Weaver, L.E., "Nuclear Power Safety," Georgia Institute of Technology Series in Nuclear Engineering, Pergamon Press Inc., pp. 303-349, 1976.
76. Sams, D.W. and Trojovsky, M., "Data Summaries of Licensee Event Reports of Primary Containment Penetrations at U.S. Commercial Nuclear Power Plants," NUREG/CR-1730, EGG-EA-5188, EG&G Idaho, Inc., September 1980.

77. Seifert, D.J. and Chubb, G.P., "SAINT: A Combined Simulation Language for Modelling Large Complex Systems," AMRL-TR-78-48, Aerospace Medical Research Laboratory, Wright-Patterson Air Force Base, Ohio, October 1978.

78. Shooman, M.L., "Probabilistic Reliability: An Engineering Approach," McGraw-Hill Book Co., 1968.

79. Siegel, A.I. and Wolf, J.J., "Man-Machine Simulation Models," John Wiley & Sons, Inc., New York, 1969.

80. Siegel, A.I., Bartter, W.D., Wolf, J.J., Knee, H.E., and Haas, P.M., "Front-End Analysis for the Nuclear Power Plant Maintenance Personnel Reliability Model," NUREG/CR-2669, ORNL/TM-8300, August 1983.

81. Singh, C., "Reliability Calculations of Large Systems," Proceedings 1975 Annual Reliability and Maintainability Symposium.

82. Singh, C., "A Cut Set Method for Reliability Evaluation of Systems Having s-Dependent Components," IEEE Transactions on Reliability, Vol. R-29, No. 5, December 1980.

83. Smith, R.L., Westland, R.A., and Blanchard, R.E., "Technique for Establishing Personnel Performance Standards (TEPPS), Technical Manual," Report PTB-70-5, Vols. 1 and 2, Personnel Research Division, Bureau of Naval Personnel, Washington, D.C., December 1969.

84. Sullivan, W.H. and Poloski, J.P., "Data Summaries of Licensee Event Reports of Pumps at U.S. Commercial Nuclear Power Plants," NUREG/CR-1205, EGG-EA-5044, EG&G Idaho, Inc., January 1980.

85. Swain, A.D., "Handbook of Human Reliability Analysis with Emphasis on Nuclear Power Plant Applications," NUREG/CR-1278, H.E. Guttman (Ed.), Sandia National Laboratories, Albuquerque, NM, 1980.

86. Trojovský, M., "Data Summaries of Licensee Event Reports of Pumps at U.S. Commercial Nuclear Power Plants," NUREG/CR-1205, Revision 1, EGG-EA-5524, January 1982.

87. Vaurio, J.K., "Unavailability of Components with Inspection and Repair," Nuclear Engineering and Design, Vol. 54, pp. 309-324, 1979.

88. Vaurio, J.K., "Practical Availability Analysis of Standby Systems," Proceedings Annual Reliability and Maintainability Symposium, pp. 125-131, 1982.

89. Vesely, W.E., "A Time-Dependent Methodology for Fault Tree Evaluation," Nuclear Engineering and Design 13(1970)337-360. North-Holland Publishing Company, 1970.

90. Vesely, W.E. and Narum, R.E., "PREP and KITT: Computer Codes for the Automatic Evaluation of a Fault Tree," USAEC Rep. IN 1349, Idaho Nuclear Corporation, August 1970.

91. Vesely, W.E., "Reply to J.D. Murchland's 'Comment on 'A Time Dependent Methodology for Fault Tree Evaluation' ' , " Nuclear Engineering and Design, vol. 22, pp 170-172, 1972.

92. Venton, A.O.F., Davidson, A.T.G. and Fraser, G.G., "The Effects of Limited Spares and Scheduled Downtime Upon the Dependability of a Simple System," IEEE Transactions on Reliability, Vol. R-25, No. 5, December 1976.

93. Vesely, W.E. and Goldberg, F.F., "Time Dependent Unavailability Analysis of Nuclear Safety Systems," IEEE Transactions on Reliability, Vol. R-26, NO. 4, October 1977.

94. Vesely, W.E. and Goldberg, F.F., "FRANTIC- A Computer Code for Time Dependent Unavailability Analysis," NUREG-0193, United States Nuclear Regulatory Commission, March 1977.

95. Vesely, W.E., Goldberg, F.F., Roberts, N.H. and Haasl, D.F., "Fault Tree Handbook," United States Nuclear Regulatory Commission Rep. NUREG-0492, 1981.

96. Vesely, W.E., Goldberg, F.F., Powers, J.T., et al., "FRANTIC II-A Computer Code for Time Dependent Unavailability Analysis," NUREG/CR-1924, April 1981.

97. Vljacic, Paul, "Building a Network of Safety," Nuclear News, March 1984.

98. Wagner, David P., "A Procedure for Qualitative Common Cause Failure Analysis of Complex Systems," Master Thesis, Department of Nuclear Engineering, The University of Tennessee, Knoxville, Tennessee, 1977.

99. "Reactor Safety Study, An Assessment of Accident Risks in U.S. Commercial Nuclear Power Plants," United States Nuclear Regulatory Commission, NUREG-75/014, 1975.

100. Winkler, R.L., "An Introduction to Bayesian Inference and Decision," Holt, Rinehart and Winston, Inc., 1972.

101. Wortman, D.B., Duket, S.D., Seifert, D.J., Hann, R.L., and Chubb, G.P., "The SAINT User's Manual," AMRL-TR-77-62, Aerospace Medical Research Laboratory, Wright-Patterson Air Force Base, Ohio, June 1978.

102. Worrell, R.B. and Stack, D.W., "A SETS User's Manual for the Fault Tree Analyst," SAND77-2051, Sandia National Laboratories, November 1978.

APPENDIXES

APPENDIX A

INPUT TO THE ASA COMPUTER
PROGRAM

INPUT DESCRIPTION FOR THE ASA COMPUTER PROGRAM

The ASA computer program, written in FORTRAN IV, determines the expected number of failures (or occurrences) for an accident sequence in an event tree. It allows the implementation of the methodology developed in Chapter II. This Appendix describes the input to the ASA computer program.

The user must supply failure, repair, and maintenance data for each basic event. The MCSs and the MPSs (optional) must be given for each system. Information concerning the initiating event must also be provided. In addition, the program requires parameters such as the time period of interest, the maximum integration interval, the mission duration, and so forth. The program does not provide non-zero default values.

The input data to ASA consist of seven sets of data cards called "data groups." The first card in each data group is a keyword identification card. The last card in each data group usually contains the number "-1" to indicate the end of the data group. The program requires all the data groups to run. In addition, the data groups must appear in the same order in which they are presented in this Appendix. Error messages will indicate a missing or displaced data group. The next sections describe each data group. The following definitions are used in the next sections:

The System Identification
Number (SIN).

This is a unique number
(from one to the number of
systems in the accident
sequence) assigned to each

system. The same SIN must be used for all the input data concerning the same system. The program will consider the system with SIN equal to one first, and SIN equal to two second, and so on. This order is important when subroutine PREPAR is used to delete some of the basic events which are common to two or more systems.

The Basic Event Identification Number (BEIN).

This is a unique number (from one to the number of basic events in the accident sequence) assigned to each basic event. The same BEIN must be used for all the input data concerning the same basic event.

Data Groups

A.1 "TITLE" Data Group

This data group specifies the title for each run. It contains the following three cards:

1. First card:

Contents..... The keyword "TIT."

Format..... 1X,A3.

2. Second card:

Contents..... Identification title.

Format Any alphanumeric information describing the title for the to 80 characters.

3. Third card:

Contents..... The number "-1."

Format..... I2.

A.2 "SYSTEM" Data Group

This data group indicates to the program how the systems relate to the basic events by providing the MCSs and, if desired, the MPSs.

1. First card:

Contents..... The keyword "SYS."

Format..... 1X,A3.

2. Second card:

Contents..... The number of systems in the accident sequence.

Format..... I2.

3. The following cards must be provided for each system:

(3.1) Contents..... The SIN and the number of MCSs in the system.

Format..... I2,I3.

(3.2) The following card must be provided for each MCS in this system:

Contents..... The BEIN for each basic event in the MCS.

Format..... 10I5.

(3.3) After completing (3.2) for all MCSs, repeat (3) for the next system.

4. After providing the cards described in (3) for all the systems in the accident sequence, the following card should appear:

Contents..... The number "-1."

Format..... I2.

5. This card indicates whether or not the MPSs are provided with the input data. If the input data contain the MPSs, the program may use (depending on the specifications in A.7) this information to compute the probabilities of the systems being up at the required times. If the MPSs are not provided, the program automatically assumes that this probability is 1.

If a number other than 1 is provided, the program assumes that the input data do not contain the MPSs. In this case, item (6) below does not apply, and the next data group should be provided. If the number 1 is inputted, proceed as indicated in (6). The format for this card is I2.

6. The following cards must be provided for each system:

6.1 Contents..... The SIN and the number of MPSs in the system.

Format..... I2,I3.

6.2 The following cards must be provided for each MPS in the system:

6.2.1 Contents..... The BEIN of the first 10 basic events.

Format..... 10I5.

6.2.2 Contents..... The BEIN of the next 10 basic events in the MPS.

Format..... 10I5.

6.2.3 Item (6.2.2) should be repeated until all the basic events in the MPS have been provided. Then, the following card should appear:

Contents..... The number "-2."

Format..... I2.

6.3 Contents..... The number "-1."

Format..... I2.

A.3 "BASIC EVENT" Data Group

This data group provides information concerning all the basic events in the accident sequence. Any basic event referred to in the MCSs should be properly defined here. The variables and parameters considered in this data group are the following:

NBE	The total number of basic events in the accident sequence.
Basic Event Type	=1 a basic event which represents a component which may fail to start or run. =2 a basic event which represents a component's failure to start only.

Basic Event Pre-	=1 constant unavailability.
demand class	=2 nonrepairable.
	=3 constantly monitored.
	=4 periodically tested.
Basic Event Post-	=2 nonrepairable.
demand class	=3 constantly monitored.

1. First card:

Contents.....	The keyword "BAS."
Format.....	1X,A3.

2. Second card:

Contents.....	NBE.
Format.....	I5.

3. The following cards should be provided for each basic event in the accident sequence:

3.1	Contents.....	BEIN.
	Format.....	I5.

3.2	Contents.....	The basic event type, the hazard rate, the periodic test interval, the first test interval, the test period (duration), and the repair period (duration).
	Format.....	I5,5E10.5.

3.3	Contents.....	The basic event predemand class, the test override unavailability, the probability of a test-caused failure, the detection inefficiency, the undetected hazard rate, and the unavailability per demand.
-----	---------------	---

Format..... I5,5E10.5.

3.4 If the basic event type is not 1, skip this item. Otherwise, the following card should appear:

Contents..... The basic event postdemand
class, the postdemand hazard
rate, and the postdemand
repair time.

Format..... I5,2E10.5.

4. Contents..... The number "-1."

Format..... I2.

A.4 "TIME" Data Group

This data group consists of five cards. The "period of time of interest" is the period of time for which the ENF is to be computed. The "maximum time interval" (to apply the rectangular and the trapezoidal rules) refers to the numerical integration of Equation 2.1 in Chapter II. The "mission duration" is the average time that a system has to run following the occurrence of the initiating event. The "maximum integration interval" applies to the numerical integration of Equation 2.8 in Chapter II.

1. First card:

Contents..... The keyword "TIM."

Format..... 1X,A3.

2. Second card:

Contents..... The period of time of interest,
the maximum time interval to
apply the rectangular rule, and
the maximum time interval to
apply the trapezoidal rule.

Format..... 3F8.2.

3. Third card:

Contents..... The mission duration for
systems 1, 2, and 3.

Format..... 3F8.2.

4. Fourth card:

Contents..... The maximum integration
interval for systems 1, 2,
and 3.

Format..... F8.2.

5. Fifth card:

Contents..... The number "-1."

Format..... I2.

A.5 "PRINT" Data Group

Optional output information is not currently available. This data group will be further developed in the future. The following two cards must appear in the input data:

1. Contents..... The keyword "PRI."

Format..... 1X,A3.

2. Contents..... The number "-1."
- Format..... I2.

A.6 "INITIATING EVENT" Data Group

This data group allows the user to specify the information concerning the initiating event. Two alternatives are currently available. The initiating event may have a constant failure (or occurrence) rate or a time-dependent failure rate. In the second case, the failure rate is specified by providing its values at user-defined times. A linear interpolation is automatically performed to compute the failure rate at times for which the failure rate was not specified. The following cards are requested in this data group:

1. Contents..... The keyword "INI."
- Format..... 1X,A3.

2. Contents..... The number "1," if (constant failure rate) or the number "2" (if time-dependent failure rate).
- Format..... I2.

3. If constant failure rate:

- Contents..... The failure rate in 1/hr.
- Format..... E10.5.

If the rate of failure is time-dependent, the user may specify the failure rate at up to 100 time points. Thus, the

cards that follow may be repeated up to 100 times. The time points must be in an increasing order, starting at time zero. The last time point must be at the time corresponding to the end of the period of interest (specified in A.4, item 2).

Contents..... Time and the initiating event
rate of failure at this time.

Format..... F10.2,E10.5.

4. Contents..... The number "-1."

Format..... I2.

A.7 "RUN" Data Group

This data group allows the user to control the execution of the ASA computer program. It currently consists of four cards as follows:

1. Contents..... The keyword "RUN."

Format..... 1X,A3.

2. Contents..... The following answers should be
given (a 1 means YES):

Compute the intersections of
the MCSs when evaluating the
probabilities of a system
failure to start?

Compute the probability that
the system is "up" when
evaluating the probability of a
system failure to run?

Compute the intersection of the
MCSs when evaluating the
probability of a system failure
to run?

Compute the upper bound in
Equation 2.7 (Chapter II,
page 48)?

Compute the probability that
the system fails to start?

Format..... 10I5.

3. Contents..... Maximum overprediction allowed.
For values below or equal to
this bound, the program will
not compute the intersection of
MCSs taken three at a time.

Format..... F6.5.

4. Contents..... The number "-1."

Format..... I2.

APPENDIX B

EXAMPLE OF AN INPUT TO THE ASA
COMPUTER PROGRAM

SYSTEM DATA GROUP

02001
10

01004

-2
-1

-2
-1
BASIC EVENT DATA GROUP

94

```

4.50000E+00.01000E+00.00000E+00.00000E+00.10000E-02 ; PT
2.10000E-05 ; NR
3 ;OFFSITE POWER
1.10000E-03 .48000E+02 ;TYPE 1
1 .00000E+00 ; CU
2.10000E-03 ; NR
4 ;IRACS 1
1.10000E-06.73000E+03.36500E+03.80000E+01.48000E+02 ;TYPE 1
4.50000E+00.01000E+00.05000E+00.00000E+00.00000E+00 ; PT
2.10000E-06 ; NR
5 ;IRACS 2
1.10000E-06.73000E+03.00000E+00.80000E+01.48000E+02 ;TYPE 1
4.50000E+00.01000E+00.05000E+00.00000E+00.00000E+00 ; PT
2.10000E-06 ; NR
6 ;LOOP 1- STEAM
1.10000E-03 .12000E+03 ;TYPE 1
3 ; CM
2.10000E-03 ; NR
7 ;LOOP 2- STEAM
1.10000E-03 .12000E+03 ;TYPE 1
3 ; CM
2.10000E-03 ; NR
8 ;LOOP 1- SODIUM
1.10000E-04 .24000E+03 ;TYPE 1
1 .00000E+00 ; CU
2.10000E-04 ; NR
9 ;LOOP 2- SODIUM
1.10000E-04 .24000E+03 ;TYPE 1
1 .00000E+00 ; CU
2.10000E-04 ; NR
10 ;DRACS
1.10000E-06 ;TYPE 1
2 ; NR
2.10000E-06 ; NR
-1
TIME DATA GROUP
08760.0000000.0108760.00
00730.0000730.00
00700.0000700.00
-1
PRINT DATA GROUP
01
-1
INITIATING EVENT DATA GROUP
01
.11416E-03
-1
RUN DATA GROUP
1 2 1 2 1
.01000
-1

```


APPENDIX C

EXAMPLE OF AN OUTPUT OF THE ASA COMPUTER PROGRAM

TIME (HOURS)	ACCIDENT SEQUENCE UNDEPENDABILITY (U)	RATE OF FAILURE OF THE INITIATING EVENT (ROF) IN (1/HR)	U X ROF
0.000	.7186E-07	.1142E-03	.8204E-11
8.000	.7269E-07	.1142E-03	.8298E-11
8.000	.6011E-08	.1142E-03	.6862E-12
56.000	.6414E-08	.1142E-03	.7322E-12
56.000	.4496E-08	.1142E-03	.5132E-12
365.000	.6355E-08	.1142E-03	.7255E-12
365.000	.1103E-06	.1142E-03	.1260E-10
373.000	.1112E-06	.1142E-03	.1269E-10
373.000	.9157E-08	.1142E-03	.1045E-11
421.000	.9573E-08	.1142E-03	.1093E-11
421.000	.6639E-08	.1142E-03	.7579E-12
730.000	.8546E-08	.1142E-03	.9756E-12
730.000	.1472E-06	.1142E-03	.1680E-10
738.000	.1480E-06	.1142E-03	.1690E-10
738.000	.1226E-07	.1142E-03	.1400E-11
786.000	.1268E-07	.1142E-03	.1448E-11
786.000	.8745E-08	.1142E-03	.9983E-12
1095.000	.1068E-07	.1142E-03	.1220E-11

1095.000	.1840E-06	.1142E-03	.2100E-10
1103.000	.1849E-06	.1142E-03	.2110E-10
1103.000	.1531E-07	.1142E-03	.1748E-11
1151.000	.1574E-07	.1142E-03	.1797E-11
1151.000	.1085E-07	.1142E-03	.1239E-11
1460.000	.1282E-07	.1142E-03	.1464E-11
1460.000	.2208E-06	.1142E-03	.2520E-10
1468.000	.2217E-06	.1142E-03	.2531E-10
1468.000	.1836E-07	.1142E-03	.2096E-11
1516.000	.1879E-07	.1142E-03	.2145E-11
1516.000	.1296E-07	.1142E-03	.1479E-11
1825.000	.1496E-07	.1142E-03	.1708E-11
1825.000	.2576E-06	.1142E-03	.2941E-10
1833.000	.2585E-06	.1142E-03	.2951E-10
1833.000	.2141E-07	.1142E-03	.2444E-11
1881.000	.2185E-07	.1142E-03	.2494E-11
1881.000	.1507E-07	.1142E-03	.1720E-11
2190.000	.1710E-07	.1142E-03	.1952E-11
2190.000	.2944E-06	.1142E-03	.3361E-10
2198.000	.2954E-06	.1142E-03	.3372E-10
2198.000	.2446E-07	.1142E-03	.2792E-11
2246.000	.2490E-07	.1142E-03	.2843E-11
2246.000	.1717E-07	.1142E-03	.1960E-11
2555.000	.1924E-07	.1142E-03	.2196E-11
2555.000	.3313E-06	.1142E-03	.3782E-10

2563.000	.3322E-06	.1142E-03	.3793E-10
2563.000	.2751E-07	.1142E-03	.3141E-11
2611.000	.2796E-07	.1142E-03	.3192E-11
2611.000	.1928E-07	.1142E-03	.2201E-11
2920.000	.2137E-07	.1142E-03	.2440E-11
2920.000	.3681E-06	.1142E-03	.4202E-10
2928.000	.3691E-06	.1142E-03	.4214E-10
2928.000	.3056E-07	.1142E-03	.3489E-11
2976.000	.3102E-07	.1142E-03	.3541E-11
2976.000	.2139E-07	.1142E-03	.2442E-11
3285.000	.2351E-07	.1142E-03	.2684E-11
3285.000	.4050E-06	.1142E-03	.4623E-10
3293.000	.4060E-06	.1142E-03	.4635E-10
3293.000	.3362E-07	.1142E-03	.3838E-11
3341.000	.3408E-07	.1142E-03	.3890E-11
3341.000	.2350E-07	.1142E-03	.2682E-11
3650.000	.2565E-07	.1142E-03	.2929E-11
3650.000	.4418E-06	.1142E-03	.5044E-10
3658.000	.4429E-06	.1142E-03	.5056E-10
3658.000	.3667E-07	.1142E-03	.4186E-11
3706.000	.3714E-07	.1142E-03	.4239E-11
3706.000	.2560E-07	.1142E-03	.2923E-11
4015.000	.2779E-07	.1142E-03	.3173E-11
4015.000	.4787E-06	.1142E-03	.5465E-10
4023.000	.4798E-06	.1142E-03	.5477E-10

4023.000	.3972E-07	.1142E-03	.4535E-11
4071.000	.4020E-07	.1142E-03	.4589E-11
4071.000	.2771E-07	.1142E-03	.3164E-11
4380.000	.2993E-07	.1142E-03	.3417E-11
4380.000	.5156E-06	.1142E-03	.5886E-10
4388.000	.5166E-06	.1142E-03	.5898E-10
4388.000	.4278E-07	.1142E-03	.4883E-11
4436.000	.4325E-07	.1142E-03	.4938E-11
4436.000	.2982E-07	.1142E-03	.3405E-11
4745.000	.3207E-07	.1142E-03	.3662E-11
4745.000	.5525E-06	.1142E-03	.6307E-10
4753.000	.5536E-06	.1142E-03	.6319E-10
4753.000	.4583E-07	.1142E-03	.5232E-11
4801.000	.4632E-07	.1142E-03	.5287E-11
4801.000	.3193E-07	.1142E-03	.3645E-11
5110.000	.3422E-07	.1142E-03	.3906E-11
5110.000	.5894E-06	.1142E-03	.6728E-10
5118.000	.5905E-06	.1142E-03	.6741E-10
5118.000	.4889E-07	.1142E-03	.5581E-11
5166.000	.4938E-07	.1142E-03	.5637E-11
5166.000	.3404E-07	.1142E-03	.3886E-11
5475.000	.3636E-07	.1142E-03	.4151E-11
5475.000	.6263E-06	.1142E-03	.7149E-10
5483.000	.6274E-06	.1142E-03	.7162E-10
5483.000	.5194E-07	.1142E-03	.5930E-11

5531.000	.5244E-07	.1142E-03	.5986E-11
5531.000	.3615E-07	.1142E-03	.4127E-11
5840.000	.3850E-07	.1142E-03	.4395E-11
5840.000	.6632E-06	.1142E-03	.7571E-10
5848.000	.6643E-06	.1142E-03	.7584E-10
5848.000	.5500E-07	.1142E-03	.6279E-11
5896.000	.5550E-07	.1142E-03	.6336E-11
5896.000	.3826E-07	.1142E-03	.4368E-11
6205.000	.4064E-07	.1142E-03	.4640E-11
6205.000	.7001E-06	.1142E-03	.7992E-10
6213.000	.7013E-06	.1142E-03	.8005E-10
6213.000	.5806E-07	.1142E-03	.6628E-11
6261.000	.5856E-07	.1142E-03	.6685E-11
6261.000	.4037E-07	.1142E-03	.4609E-11
6570.000	.4278E-07	.1142E-03	.4884E-11
6570.000	.7370E-06	.1142E-03	.8414E-10
6578.000	.7382E-06	.1142E-03	.8427E-10
6578.000	.6111E-07	.1142E-03	.6977E-11
6626.000	.6162E-07	.1142E-03	.7035E-11
6626.000	.4249E-07	.1142E-03	.4850E-11
6935.000	.4493E-07	.1142E-03	.5129E-11
6935.000	.7739E-06	.1142E-03	.8835E-10
6943.000	.7751E-06	.1142E-03	.8849E-10
6943.000	.6417E-07	.1142E-03	.7326E-11
6991.000	.6469E-07	.1142E-03	.7385E-11

6991.000	.4460E-07	.1142E-03	.5091E-11
7300.000	.4707E-07	.1142E-03	.5373E-11
7300.000	.8109E-06	.1142E-03	.9257E-10
7308.000	.8121E-06	.1142E-03	.9271E-10
7308.000	.6723E-07	.1142E-03	.7675E-11
7356.000	.6775E-07	.1142E-03	.7735E-11
7356.000	.4671E-07	.1142E-03	.5332E-11
7665.000	.4921E-07	.1142E-03	.5618E-11
7665.000	.8478E-06	.1142E-03	.9679E-10
7673.000	.8491E-06	.1142E-03	.9693E-10
7673.000	.7029E-07	.1142E-03	.8024E-11
7721.000	.7082E-07	.1142E-03	.8084E-11
7721.000	.4882E-07	.1142E-03	.5573E-11
8030.000	.5136E-07	.1142E-03	.5863E-11
8030.000	.8848E-06	.1142E-03	.1010E-09
8038.000	.8861E-06	.1142E-03	.1012E-09
8038.000	.7335E-07	.1142E-03	.8373E-11
8086.000	.7388E-07	.1142E-03	.8434E-11
8086.000	.5093E-07	.1142E-03	.5815E-11
8395.000	.5350E-07	.1142E-03	.6108E-11
8395.000	.9218E-06	.1142E-03	.1052E-09
8403.000	.9230E-06	.1142E-03	.1054E-09
8403.000	.7641E-07	.1142E-03	.8723E-11
8451.000	.7695E-07	.1142E-03	.8784E-11
8451.000	.5305E-07	.1142E-03	.6056E-11
8760.000	.5564E-07	.1142E-03	.6352E-11

THE SYSTEM EXPECTED NUMBER OF FAILURES IS .416748E-07

APPENDIX D

THE LISTING OF THE ASA COMPUTER
PROGRAM

```

C ASASASASASASASASASAS ASASASASASASASASASAS ASASASASASASASASASAS
C SASASASASASASASASASAS SASASASASASASASASASAS SASASASASASASASASASAS
C ASASASASASASASASASASAS ASASASASASASASASASASAS ASASASASASASASASASASAS
C SASASASASASASASASASAS SASASASASASASASASASASAS ASASASASASASASASASASAS
C ASASASASASASASASASASAS ASASASASASASASASASASAS ASASASASASASASASASASAS
C SASASASASASASASASASASAS ASASASASASASASASASASAS ASASASASASASASASASASAS
C ASASASASASASASASASASAS ASASA ASASASASASASASASASASASAS
C SASASASASASASASASASASAS SASAS SASASASASASASASASASASAS
C ASASA SASAS ASASA ASASA SASAS SASAS
C SASAS SASAS ASASA SASAS SASAS SASAS
C ASASA SASAS ASASA SASAS SASAS SASAS
C SASAS ASASA SASAS SASAS SASAS SASAS
C ASASA SASAS ASASASASASASASASASAS ASASA SASAS
C SASAS ASASA SASASASASASASASASASAS SASAS ASASA
C ASASASASASASASASASASAS SASASASASASASASASASASAS SASASASASASASASASASASAS
C ASASASASASASASASASASAS ASASASASASASASASASASAS ASASASASASASASASASASAS
C SASASASASASASASASASASAS SASASASASASASASASASASAS SASASASASASASASASASASAS
C ASASASASASASASASASASAS SASAS ASASASASASASASASASASAS
C SASASASASASASASASASASAS ASASA ASASA SASASASASASASASASASAS
C ASASA SASAS SASAS ASASA SASAS ASASA SASAS
C SASAS ASASA ASASA ASASA SASAS ASASA SASAS
C ASASA SASAS ASASA ASASA SASAS ASASA SASAS
C SASAS ASASA ASASA ASASA SASAS ASASA SASAS
C ASASA SASAS ASASASASASASASASASAS ASASA SASAS
C SASAS ASASA SASASASASASASASASASAS SASAS ASASA
C ASASA SASAS ASASASASASASASASASASAS ASASA SASAS
C ASASA SASAS ASASASASASASASASASASAS ASASA SASAS
C SASAS ASASA SASAS ASASASASASASASASASASAS SASAS ASASA
C *****
C *
C * TITLE: ASA (AN ACRONYM FOR ACCIDENT SEQUENCE ANALYSIS)*
C *
C * PURPOSE: THIS PROGRAM COMPUTES THE EXPECTED NUMBER OF *
C * OCCURRENCES (OR FAILURES) OF AN ACCIDENT *
C * SEQUENCE IN AN EVENT TREE, WHERE FAULT TREES *
C * ARE AVAILABLE FOR EACH BRANCHING POINT IN THE *
C * EVENT TREE. *
C *
C * PROGRAMMER: THE ASA COMPUTER PROGRAM WAS WRITTEN BY *
C * HENRIQUE M. PAULA AS A PART OF THE *
C * REQUIREMENTS FOR OBTAINING THE PH. D. DEGREE *
C * IN NUCLEAR ENGINEERING AT THE UNIVERSITY OF *
C * TENNESSEE IN KNOXVILLE, TENNESSEE. *
C *****

```

```

COMMON  INFORM( 3, 20, 5), JNFORM(3, 20, 20), RBE( 300,12), NDP
COMMON  IBE( 300,3), MCSTYP(3, 20), NUMMCS(3), NUMMPS ( 3)
COMMON  NUMRUN(3), IHELP(1000), TRUN(3), BASE( 300 )
COMMON  MPSVCT(10, 20), ROFVCT(100,2), TFINAL
COMMON  TPRIME, DPRIME, FIRST, FINAL, NS
COMMON  DELTA1, DELTA2, BOUND , IDELTA
COMMON  DELTAP, TDIFF, DELTA, NIM, IND01
COMMON  NBE, IND02, IND03, IND04 , IND05
COMMON  IND10, IND09, IND08, IND07, IND06
COMMON  JDELTA(3),          DLTPR (3)
COMMON ROF
DIMENSION FSIMP(200),STORE4(2000,4)

C
C  READ THE INPUT DATA
C
C  CALL START
C
C      BEGIN THE EXECUTION OF THE ASA COMPUTER PROGRAM
C
C      CALL PREPAR
C
C          COMPUTE THE NUMBER OF POINTS (IDELTA) FOR THE
C          NUMERICAL INTEGRATION OF THE DENSITY FUNCTION
C          FOR THE TIME TO FIRST FAILURE.
C
C          DO 90000 I=1,NS
C              I1=INT(TRUN(I)/DLTPR(I))+1
C              IF((FLOAT(I1)/2.).NE.FLOAT(INT(FLOAT(I1)
C                  /2.)))
C                  GO TO 2000
C              JDELTA(I)=I1+1
C              GO TO 2010
C              CONTINUE
C              JDELTA(I)=I1
C              CONTINUE
C              IF(JDELTA(I).GE.3)      GO TO 2011
C              JDELTA(I)=3
C              CONTINUE
C              IF(JDELTA(I).GT.101)    GO TO 20030
C
C          COMPUTE THE ACTUAL INTEGRATION INTERVAL
C
C          DLTPR(I)=TRUN(I)/(JDELTA(I)-1)
C
C          90000      CONTINUE
C
C      START THE COMPUTATION OF THE EXPECTED NUMBER OF FAILURES
C
C      ENF=0.
C      IN=1
C      ISTORE=1
C      701  CONTINUE

```

```

C
C      SUBROUTINE TIMES
C
C      CALL TIMES (IN)
C      IN=IN+1
C      EPS=.001
C      IF(NIM.EQ.1) GO TO 11
C      IF(NIM.EQ.2) GO TO 12
C*****
C      NUMERICAL INTEGRATION -- SIMPSON'S RULE
C*****
C      IF(NDP.GT.201)
C      HELP=DELTA/FLOAT(NDP-1)
C      GO TO 14000
C
C      COMPUTE THE FIRST DATA POINT FOR THE NUMERICAL INTEGRATION.
C
C      TPRIME=FIRST+EPS
C      IF(TPRIME.EQ.FIRST) GO TO 20000
C      UNDEP=1.
C
C      COMPUTE THE UNAVAILABILITIES OF THE BASIC EVENTS
C      ( THE VECTOR BASE( 300) ).
C
C      CALL BASIC1
C      DO 10000 J=1,NS
C      IDELTA=JDELTA(J)
C      DELTAP=DLTPR(J)
C      JJ=J
C      IF(TRUN(JJ).NE.0)
C      GO TO 15000
C      IND05=2
C      GO TO 15010
15000 CONTINUE
C      IND05=1
15010 CONTINUE
C      CALL UNDEPE (JJ,UNDE)
C      UNDEP=UNDEP*UNDE
10000 CONTINUE
C
C      COMPUTE THE RATE OF FAILURE OF THE INITIATING EVENT:
C
C      IF(IND06.EQ.1)
C      CALL ROFIE(ROF)
C      GO TO 11010
11010 CONTINUE
C      FSIMP(1)=UNDEP*ROF
C      STORE4(ISTORE,1) = FIRST
C      STORE4(ISTORE,2) = UNDEP
C      STORE4(ISTORE,3) = ROF
C      STORE4(ISTORE,4) = FSIMP(1)
C      ISTORE=ISTORE+1

```

```

C
C      COMPUTE THE REMAINING DATA POINTS FOR THE NUMERICAL INTEGRATION.
C
      DO 10010 I=2,NDP-1
      UNDEP=1.
      TPRIME=HELP*(I-1)+TFINAL
C
C      COMPUTE THE UNAVAILABILITIES OF THE BASIC EVENTS
C      ( THE VECTOR BASE(300) ).
C
      CALL BASIC1
      DO 10015 J=1,NS
      IDELTA=JDELTA(J)
      DELTAP=DLTPR(J)
      JJ=J
      IF(TRUN(JJ).NE.0) GO TO 15040
      IND05=2
      GO TO 15050
15040 CONTINUE
      IND05=1
15050 CONTINUE
      CALL UNDEPE (JJ,UNDE)
      UNDEP=UNDEP*UNDE
10015 CONTINUE
C
C      COMPUTE THE RATE OF FAILURE OF THE INITIATING EVENT:
C
      IF(IND06.EQ.1) GO TO 11030
      CALL ROFIE(ROF)
11030 CONTINUE
      FSIMP(1)=ROF*UNDEP
      STORE4(ISTORE,1) = TPRIME
      STORE4(ISTORE,2) = UNDEP
      STORE4(ISTORE,3) = ROF
      STORE4(ISTORE,4) = FSIMP(1)
      ISTORE=ISTORE+1
10010 CONTINUE
C
C      COMPUTE THE LAST DATA POINT FOR THE NUMERICAL INTEGRATION.
C
      TPRIME=FINAL-EPS
      UNDEP=1.
C
C      COMPUTE THE UNAVAILABILITIES OF THE BASIC EVENTS
C      ( THE VECTOR BASE( 300) ).
C
      CALL BASIC1
      DO 10020 J=1,NS
      IDELTA=JDELTA(J)
      DELTAP=DLTPR(J)
      JJ=J

```

```

        IF(TRUN(JJ).NE.0)                                GO TO 15020
            IND05=2
            GO TO 15030
15020  CONTINUE
            IND05=1
15030  CONTINUE
        CALL UNDEPE(JJ,UNDE)
        UNDEP=UNDEP*UNDE
10020  CONTINUE
C
C          COMPUTE THE RATE OF FAILURE OF THE INITIATING EVENT:
C
        IF(IND06.EQ.1)                                GO TO 11020
            CALL ROFIE(ROF)
11020  CONTINUE
        FSIMP(NDP)= UNDEP*ROF
        STORE4(ISTORE,1) = FINAL
        STORE4(ISTORE,2) = UNDEP
        STORE4(ISTORE,3) = ROF
        STORE4(ISTORE,4) = FSIMP(NDP)
        ISTORE=ISTORE+1
C
C          PERFORM THE INTEGRATION USING SIMPSON'S RULE.
C
        FEVEN=0.0
        FODD=0.0
        DO 10030 I=2,NDP-1,2
10030  FEVEN=FEVEN+FSIMP(I)
        DO 10040 I=3,NDP-2,2
10040  FODD=FODD+FSIMP(I)
        ENF=ENF+(HELP/3.)*(FSIMP(1)+4.*FEVEN+2.*FODD+FSIMP(NDP))
        IF(FINAL.NE.TFINAL) GO TO 701
        GO TO 20010
C*****
C
C          NUMERICAL INTEGRATION  --  RECTANGULAR RULE
C
C*****
11  CONTINUE
    TPRIME=(FINAL+FIRST)/2.
C
C          COMPUTE THE UNAVAILABILITIES OF THE BASIC EVENTS
C          ( THE VECTOR BASE( 300) ).
C
        CALL BASIC1
        UNDEP=1.
        DO 20 I=1,NS
        IDELTA=JDELTA(I)
        DELTAP=DLTPR(I)
        II=I
        IF(TRUN(II).NE.0)                                GO TO 15060

```

```

                IND05=2
                GO TO 15070
15060 CONTINUE
                IND05=1
15070 CONTINUE
                CALL UNDEPE (11,UNDE)
                UNDEP=UNDEP*UNDE
20 CONTINUE
C
C                COMPUTE THE RATE OF FAILURE OF THE INITIATING EVENT:
C
                IF(IND06.EQ.1)                                GO TO 11040
                CALL ROFIE(ROF)
11040 CONTINUE
                F=ROF*UNDEP
                STORE4(ISTORE,1) = TPRIME
                STORE4(ISTORE,2) = UNDEP
                STORE4(ISTORE,3) = ROF
                STORE4(ISTORE,4) = F
                ISTORE=ISTORE+1
                ENF=ENF+F*(FINAL-FIRST)
                IF(FINAL.NE.TFINAL) GO TO 701
                GO TO 20010
C*****
C                                                                *
C                NUMERICAL INTEGRATION  --  TRAPEZOIDAL RULE                                *
C                                                                *
C*****
12 CONTINUE
                TPRIME=FIRST+EPS
                IF(TPRIME.EQ.FIRST)                                GO TO 20000
13 CONTINUE
C
C                COMPUTE THE UNAVAILABILITIES OF THE BASIC EVENTS
C                ( THE VECTOR BASE( 300) ).
C
                CALL BASIC1
                UNDEP=1.
                DO 21 I=1,NS
                IDELTA=JDELTA(I)
                DELTAP=DLTPR(I)
                II=I
                IF(TRUN(II).NE.0.)                                GO TO 15080
                IND05=2
                GO TO 15090
15080 CONTINUE
                IND05=1
15090 CONTINUE
                CALL UNDEPE (11,UNDE)
                UNDEP=UNDEP*UNDE
21 CONTINUE

```

```

C
C          COMPUTE THE RATE OF FAILURE OF THE INITIATING EVENT:
C
      IF(IND06.EQ.1)                      GO TO 11050
      CALL ROFIE(ROF)
11050  CONTINUE
      F=ROF*UNDEP
      IF(TPRIME.EQ.(FIRST+EPS))            GO TO 11051
      STORE4(ISTORE,1) = FINAL
      GO TO 11052
11051  CONTINUE
      STORE4(ISTORE,1) = FIRST
11052  CONTINUE
      STORE4(ISTORE,2) = UNDEP
      STORE4(ISTORE,3) = ROF
      STORE4(ISTORE,4) = F
      ISTORE=ISTORE+1
      IF(TPRIME.NE.FIRST+EPS) GO TO 19
      TPRIME=FINAL-EPS
      FA=F
      GO TO 13
19     CONTINUE
      ENF=ENF+((FA+F)/2.)*(FINAL-FIRST)
      IF(FINAL.NE.TFINAL) GO TO 701
20010  CONTINUE
      WRITE(21,1020)
      WRITE(21,1031)
      WRITE(21,1060)
      WRITE(21,1070)
      WRITE(21,1060)
      WRITE(21,1080)
      WRITE(21,1060)
      WRITE(21,1090)
      WRITE(21,1060)
      WRITE(21,1100)
      WRITE(21,1060)
      WRITE(21,1031)
      WRITE(21,1060)
      WRITE(21,1060)
      DO 888 IFIZ=1,ISTORE-1
        WRITE(21,1110) (STORE4(IFIZ,LFIZ),LFIZ=1,4)
        WRITE(21,1060)
888    CONTINUE
      WRITE(21,1031)
      WRITE(21,1020)
      WRITE(21,1030)
      WRITE(21,1040) ENF
      WRITE(5,1040) ENF
      WRITE(21,1030)
      STOP
20030  CONTINUE

```



```

        WRITE(21,1030)
        WRITE(21,1020)
        WRITE(21,1050) JDELTA(1),1
        WRITE(21,1010)
        STOP
20000          CONTINUE
                WRITE(21,1000) EPS
                WRITE(21,1010)
                STOP
14000  CONTINUE
        WRITE(21,1031)
        WRITE(21,1120) NDP
        WRITE(21,1010)
        WRITE(21,1031)
        STOP
C *****
C
C          FORMATS
C
C *****
1000  FORMAT('1 THE TIME INTERVAL EPS=',E15.5,' IS TOO SMALL.')
1010  FORMAT('0 THE PROGRAM WILL NOT BE EXECUTED')
1020  FORMAT('1')
1030  FORMAT('0-----')
      1-----')
1031  FORMAT('-----')
      1-----')
1040  FORMAT('0THE SYSTEM EXPECTED NUMBER OF FAILURES IS ',E11.6)
1050  FORMAT('0THE NUMBER OF DATA POINTS (' ,12,' ) REQUIRED TO NUMERICA
      1LLY COMPUTE THE PROBABILITY OF ',//,' FAILURE TO RUN FOR SYSTEM (' ,
      212,' ) HAS EXCEEDED THE LIMIT (101).')
1060  FORMAT(' ',10X,' ',19X,' ',18X,' ',20X,' ')
1070  FORMAT(' ',3X,' TIME',3X,' ',1X,' ACCIDENT SEQUENCE',1X,' ',1X
      1,' RATE OF FAILURE',2X,' ',7X,' U',12X,' ')
1080  FORMAT(' ',2X,' (HOURS)',1X,' ',2X,' UNDEPENDABILITY',2X,' ',4
      1X,' OF THE',8X,' ',7X,' X',12X,' ')
1090  FORMAT(' ',10X,' ',7X,' (U)',9X,' ',1X,' INITIATING EVENT',1X,
      1,' ',6X,' ROF',11X,' ')
1100  FORMAT(' ',10X,' ',19X,' ',1X,' (ROF) IN (1/HR)',2X,' ',20X,'
      1')
1110  FORMAT(' ',1X,F8.3,1X,' ',4X,E9.4,6X,' ',4X,E9.4,5X,' ',6X,E
      19.4,5X,' ')
1120  FORMAT('0THE NUMBER OF DATA POINTS (' ,13,' ) REQUIRED TO NUMERICA
      1LLY COMPUTE THE "ENF" HAS EXCEEDED THE LIMIT (201).')
      END

```



```

C*****
C
C          THE SYSTEM DATA GROUP
C
C*****
C          ILET(2)=1
C
C          INITIALIZATION
C
C          DO 20010 I1=1,3
C            DO 20020 I2=1,20
C              DO 20030 I3=1,20
C                IF(I3.GT.5) GO TO 20040
C                INFORM(I1,I2,I3)=0
20040              CONTINUE
C                JNFORM(I1,I2,I3)=0
20030              CONTINUE
20020            CONTINUE
20010          CONTINUE
C          LOAD THE VECTOR INFORM(3,20,5).
C
C          READ(20,20500) NS
C          WRITE(21,10510)
C          WRITE(21,10520)
C          WRITE(21,20510) NS
C          WRITE(21,10520)
C          DO 20050 I=1,NS
C
C            READ THE SYSTEM IDENTIFICATION (I1) AND THE
C            NUMBER OF MCS'S IN EACH SYSTEM (I1).
C
C            READ(20,20520) I1,NUMMCS(I)
C            IF(I1.NE.1) GO TO 20060
C
C            READ THE BASIC EVENTS IN EACH MCS OF THE SYSTEM
C            'I1'.
C
C            DO 20070 I2=1,NUMMCS(I)
C              READ(20,20540) (INFORM(I1,I2,J),J=1,5)
20070            CONTINUE
20050          CONTINUE
C          READ THE NEXT CARD AFTER THE DATA FOR INFORM(3,20,5).
C
C          READ(20,20500) ITEST
C          IF(ITEST.NE.-1) GO TO 20080
C
C          LOAD THE VECTOR JNFORM(3,20,20).
C          (IF APPLICABLE)
C

```



```

20150                                CONTINUE
                                WRITE(21,10510)
                                WRITE(21,20530)
                                WRITE(21,20551)
                                WRITE(21,10570)
                                STOP

20091                CONTINUE
C
C      ECHO-PRINTING THE VECTORS INFORM(3,20,5) AND JNFORM(3,20,20).
C
      DO 20160 LL=1,NS
        WRITE(21,10510)
        WRITE(21,10520)
        WRITE(21,20560) LL
        WRITE(21,10520)
        WRITE(21,20570)
        WRITE(21,10550)
        DO 20170 KK=1,NUMMCS(LL)
          WRITE(21,20580) KK,(INFORM(LL,KK,M),M=1,5)
20170      CONTINUE
          IF(IND01.NE.1)                                GO TO 20160
          WRITE(21,10510)
          DO 20180 KK=1,NUMMPS(LL)
            WRITE(21,20590) KK
            JAUX=1
            DO 20190 JJ=1,2
              WRITE(21,10550)
              IF(JNFORM(LL,KK,JAUX).EQ.0) GO TO 20200
              WRITE(21,20540)(JNFORM(LL,KK,L),L=JAUX,
                1              JAUX+9)
              JAUX=JAUX+10
20190      CONTINUE
20200      CONTINUE
20180      CONTINUE
20160  CONTINUE
      GO TO 10
30000  CONTINUE
      IF(KEY.NE.'BAS') GO TO 40000
      IF(ILET(2).EQ.0) GO TO 111
C*****
C
C      THE BASIC EVENT DATA GROUP
C
C*****
      ILET(3)=1
      READ(20,30510) NBE
C
C      THE BASIC EVENTS IN INFORM(1SYS,1MCS,1BAS) AND
C      JNFORM(1SYS,1MPS,1BAS) SHOULD HAVE IDENTIFICATION
C      NUMBERS BETWEEN 1 AND "NBE".
C

```

```

C
C
C      CHECK INFORM( ISYS, IMCS, IBAS):
C
C      DO 36000                                LL1=1, NS
C      DO 36010                                LL2=1, NUMMCS(LL1)
C      DO 36020                                LL3=1, 5
C      IF( INFORM(LL1, LL2, LL3).EQ.0)          GO TO 36010
C      IF(( INFORM(LL1, LL2, LL3).LT.1).OR.
C      ( INFORM(LL1, LL2, LL3).GT.NBE))        GO TO 36030
C      1
C      CONTINUE
36020
36010 CONTINUE
36000 CONTINUE
C
C      CHECK JNFORM( ISYS, IMPS, IBAS):
C
C      DO 36100                                LL1=1, NS
C      DO 36110                                LL2=1, NUMMPS(LL1)
C      DO 36120                                LL3=1, 20
C      IF( JNFORM(LL1, LL2, LL3).EQ.0)          GO TO 36110
C      IF(( JNFORM(LL1, LL2, LL3).LT.1).OR.
C      ( JNFORM(LL1, LL2, LL3).GT.NBE))        GO TO 36130
C      1
C      CONTINUE
36120
36110 CONTINUE
36100 CONTINUE
C
C      INITIALIZATION.
C
C      DO 30010                                I1=1, NBE
C      DO 30020                                I2=1, 12
C      IF( I2.GT.3) GO TO 30030
C      IBE( I1, I2)= 0
C      30030 CONTINUE
C      RBE( I1, I2)= 0
C      30020 CONTINUE
C      30010 CONTINUE
C
C      LOAD THE VECTORS IBE(NBE,3) AND RBE(NBE,12).
C
C      DO 30040 JJ1=1,300
C      READ(20,30510) IDUMMY
C      IF( IDUMMY.LT.0) GO TO 30041
C      IF( IDUMMY.NE. JJ1 ) GO TO 30050
C      READ(20,30520) IBE( JJ1, 1), (RBE( JJ1, L), L=1, 5)
C      READ(20,30520) IBE( JJ1, 2), (RBE( JJ1, L), L=6, 10)
C      IF( IBE( JJ1, 1).EQ.2) GO TO 39040
C      READ(20,30520) IBE( JJ1, 3), (RBE( JJ1, L), L=11, 12)
C      CONTINUE
C      39040 CONTINUE
C      30040 READ(20,30510) IDUMMY
C      IF( IDUMMY.NE.-1) GO TO 30070
C      30041 CONTINUE
C      GO TO 30080

```



```

C
C
C
30110      THE PRE-DEMAND DATA:
          CONTINUE
          WRITE(21,30600) IBE( IBAS,1)
          IF( IBE( IBAS,2).EQ.1)      GO TO 30120
          IF( IBE( IBAS,2).EQ.2)      GO TO 30130
          IF( IBE( IBAS,2).EQ.3)      GO TO 30140
          IF( IBE( IBAS,2).EQ.4)      GO TO 30150
          WRITE(21,30530)
          WRITE(21,30610) IBE( IBAS,2)
          WRITE(21,10570)
          STOP
30120      CONTINUE
          WRITE(21,30620)
          WRITE(21,30660) RBE( IBAS,10)
          GO TO 30200
30130      CONTINUE
          WRITE(21,30630)
          WRITE(21,30670) RBE( IBAS,1)
          WRITE(21,30671) RBE( IBAS,10)
          GO TO 30200
30140      CONTINUE
          WRITE(21,30640)
          WRITE(21,30680) RBE( IBAS,1),RBE( IBAS,5)
          WRITE(21,30671) RBE( IBAS,10)
          GO TO 30200
30150      CONTINUE
          WRITE(21,30650)
          WRITE(21,30690) RBE( IBAS,1),RBE( IBAS,2)
          WRITE(21,30700) RBE( IBAS,3),RBE( IBAS,4)
          WRITE(21,30710) RBE( IBAS,5),RBE( IBAS,6)
          WRITE(21,30720) RBE( IBAS,7),RBE( IBAS,8)
          WRITE(21,30730) RBE( IBAS,9),RBE( IBAS,10)

C
C
C
30200      THE POST-DEMAND DATA:
          CONTINUE
          IF( IBE( IBAS,1).EQ.2)      GO TO 30100
          IF( IBE( IBAS,3).EQ.2)      GO TO 30220
          IF( IBE( IBAS,3).EQ.3)      GO TO 30230
          WRITE(21,30740) IBAS, IBE( IBAS,3)
          WRITE(21,10570)
          STOP
30220      CONTINUE
          WRITE(21,30760)
          WRITE(21,30790) RBE( IBAS,11)
          GO TO 30100
30230      CONTINUE
          WRITE(21,30770)
          WRITE(21,30800) RBE( IBAS,11),RBE( IBAS,12)
          GO TO 30100

```



```

30100  CONTINUE
      GO TO 10
40000  CONTINUE
      IF(KEY.NE.'TIM')          GO TO 50000
      IF(ILET(3).EQ.0)          GO TO 112
C*****
C
C              THE TIME DATA GROUP
C
C*****
      ILET(4)=1
      READ(20,40510) TFINAL,DELTA1,DELTA2
      READ(20,40510) (TRUN(LL1),LL1=1,NS)
      READ(20,40510) (DLTPR(LL2),LL2=1,NS)
      READ(20,10505) IDUMMY
      IF(IDUMMY.NE.-1)          GO TO 40040
C
C      CHECK FOR INVALID ENTRIES:
C
      DO 40010 I4=1,NS
        IF(TRUN(I4).LT.0)      GO TO 40020
        IF(DLTPR(I4).LE.0.)    GO TO 40030
40010  CONTINUE
      GO TO 10
40020  CONTINUE
      WRITE(21,40520)
      WRITE(21,40530) I4
      WRITE(21,10570)
      STOP
40030  CONTINUE
      WRITE(21,40520)
      WRITE(21,40540) I4
      WRITE(21,10570)
      STOP
40040  CONTINUE
      WRITE(21,40550)
      WRITE(21,10570)
      STOP
50000  CONTINUE
      IF(KEY.NE.'PRI')          GO TO 60000
      IF(ILET(4).EQ.0)          GO TO 113
C*****
C
C              THE PRINT DATA GROUP
C
C*****
      ILET(5)=1
      READ(20,10505) IND10
      READ(20,10505) IDUMMY
      IF(IDUMMY.NE.-1)
        GO TO 50020
      IF(IND10.EQ.1)
        GO TO 50010
      WRITE(21,50510)

```

```

        GO TO 10
50010  CONTINUE
        WRITE(21,50520)
        GO TO 10
50020  CONTINUE
        WRITE(21,50530)
        WRITE(21,10570)
        STOP
60000  CONTINUE
        IF(KEY.NE.'INI')          GO TO 70000
        IF(ILET(5).EQ.0)          GO TO 114
C*****
C
C          THE INITIATING EVENT DATA GROUP
C
C*****
        ILET(6)=1
        READ(20,10505) IND06
        IF(IND06.NE.1) GO TO 60100
        READ(20,60502) ROF
        WRITE(21,60620) ROF
        READ(20,10505) IDUMMY
        IF(IDUMMY.NE.-1)          GO TO 60200
        GO TO 10
60200  CONTINUE
        WRITE(21,60610)
        WRITE(21,10570)
        STOP
60100  CONTINUE
        READ(20,60501) ROFVCT(1,1),ROFVCT(1,2)
C
C          THE FIRST TIME DATA POINT MUST BE ZERO:
C
        IF(ROFVCT(1,1).NE.0.)    GO TO 60010
        DO 60020 I=2,100
            READ(20,60501) ROFVCT(I,1),ROFVCT(I,2)
            IF(ROFVCT(I,1).EQ.-1.) GO TO 60021
            KOUNT=I-1
60020  CONTINUE
        READ(20,60500) DUMMY
        IF(DUMMY.NE.-1.)          GO TO 60030
        KOUNT=100
60021  CONTINUE
C
C          THE LAST TIME DATA POINT MUST BE AT TFINAL:
C
        IF(ROFVCT(KOUNT,1).EQ.TFINAL) GO TO 10
C
C          ERROR MESSAGES:
C

```

```

        WRITE(21,60510)
        WRITE(21,60540) ROFVCT(KOUNT,1)
        WRITE(21,60530)
        STOP
60010  CONTINUE
        WRITE(21,60510)
        WRITE(21,60520) ROFVCT(1,1)
        WRITE(21,60530)
        STOP
60030  CONTINUE
        WRITE(21,60510)
        WRITE(21,60560)
        WRITE(21,60570)
        WRITE(21,60530)
        STOP
70000  CONTINUE
        IF(KEY.NE.'RUN')
                                GO TO 70010
        IF(ILET(6).NE.1)
                                GO TO 116
C*****
C
C          THE "RUN" DATA GROUP.
C
C*****
        READ(20,70520) IND02,IND03,IND04,IND09,IND08
        READ(20,70540) BOUND
        READ(20,10505) IDUMMY
        IF(IDUMMY.EQ.-1)
                                GO TO 70020
        WRITE(21,10510)
        WRITE(21,70530) IDUMMY
        WRITE(21,10570)
        STOP
C*****
C
C          ERROR MESSAGES INDICATING A MISSING OR DISPLACED
C
C          DATA GROUP.
C
C*****
00110  CONTINUE
C
C          THE "TITLE DATA GROUP" IS EITHER MISSING OR DISPLACED.
C
        WRITE(21,10510)
        WRITE(21,10580)
        WRITE(21,10570)
        STOP
00111  CONTINUE
C
C          THE "SYSTEM DATA GROUP" IS EITHER MISSING OR DISPLACED.
C
        WRITE(21,10510)
        WRITE(21,20600)

```

```

        WRITE(21,10570)
        STOP
00112  CONTINUE
C
C      THE "BASIC EVENT DATA GROUP" IS EITHER MISSING OR DISPLACED.
C
        WRITE(21,10510)
        WRITE(21,30500)
        WRITE(21,10570)
        STOP
00113  CONTINUE
C
C      THE "TIME DATA GROUP" IS EITHER MISSING OR DISPLACED.
C
        WRITE(21,10510)
        WRITE(21,40500)
        WRITE(21,10570)
        STOP
00114  CONTINUE
C
C      THE "PRINT DATA GROUP" IS EITHER MISSING OR DISPLACED.
C
        WRITE(21,10510)
        WRITE(21,50500)
        WRITE(21,10570)
        STOP
00115  CONTINUE
C
C      THE "INITIATOR DATA GROUP" IS EITHER MISSING OR DISPLACED.
C
        WRITE(21,10510)
        WRITE(21,60500)
        WRITE(21,10570)
        STOP
00116  CONTINUE
C
C      THE "RUN DATA GROUP" IS EITHER MISSING OR DISPLACED.
C
        WRITE(21,10510)
        WRITE(21,70500)
        WRITE(21,10570)
        STOP
70010  CONTINUE
        WRITE(21,10510)
        WRITE(21,70510) KEY
        WRITE(21,10570)
        STOP
70020  CONTINUE
        RETURN

```

```

C*****
C
C          FORMATS
C
C*****
01000  FORMAT(1X,A3)
C
C          10000 LEVEL
C
10500  FORMAT(20A4)
10505  FORMAT(3I2)
10510  FORMAT('1')
10520  FORMAT('0-----' )
10530  FORMAT('0 THE ACCIDENT SEQUENCE IDENTIFICATION TITLE:')
10540  FORMAT('0',20A4)
10550  FORMAT('0')
10560  FORMAT('1 THE LAST CARD IN THE "TITLE DATA GROUP" MUST CONTAIN T
1HE NUMBER -1')
10570  FORMAT('0 THE PROGRAM WILL NOT BE EXECUTED')
10580  FORMAT('0THE "TITLE DATA GROUP" IS EITHER MISSING OR DISPLACED')
C
C          20000 LEVEL
C
20500  FORMAT(I2)
20510  FORMAT('0THE NUMBER OF SYSTEMS IN THE ACCIDENT SEQUENCE: ',I2)
20520  FORMAT(I2,I3)
20530  FORMAT('0AN ERROR HAS BEEN DETECTED IN THE "SYSTEM DATA GROUP".
1 ')
20531  FORMAT('0THE PROGRAM IS READING ',I2,' AS THE IDENTIFICATION NUM
1BER FOR SYSTEM ',I2,' (MCS).')
20532  FORMAT('0THE PROGRAM IS READING ',I2,' AS THE IDENTIFICATION
1NUMBER FOR SYSTEM ',I2,' (MPS).')
20540  FORMAT(10I5)
20550  FORMAT('0AFTER THE DATA FOR "INFORM(1,J,K)", THE PROGRAM SHOU
1LD READ A -1.')
20551  FORMAT('0AFTER THE DATA FOR "JNFORM(3,20,20)", THE PROGRAM
1SHOULD READ A "-1".')
20560  FORMAT('0SYSTEM NUMBER ',I3)
20570  FORMAT('0MCS ',20X,' BASIC EVENTS')
20580  FORMAT(2X,I2,20X,10I5)
20590  FORMAT('1 MINIMAL PATH SET ',I3,' CONTAINS THE FOLLOWING BASIC
1EVENTS:')
20600  FORMAT('0THE "SYSTEM DATA GROUP" IS EITHER MISSING OR DISPLA
1CED.')
C
C          30000 LEVEL
C
30500  FORMAT('0THE "BASIC EVENT DATA GROUP" IS EITHER MISSING OR DISPL
1ACED.')
30510  FORMAT(I5)
30520  FORMAT(I5,5E10.5)

```

```

30530  FORMAT('OAN ERROR HAS BEEN DETECTED IN THE "BASIC EVENT DATA GRO
1UP".')
30540  FORMAT('OBASIC EVENT ',14,' IS EITHER INVALID OR OUT OF ORDER.')
```

30560 FORMAT('O1000 BASIC EVENTS HAVE BEEN PROVIDED. THE NEXT DATA
1CARD MUST CONTAIN THE NUMBER -1.')

```

30570  FORMAT(' BASIC EVENT # ',14)
30580  FORMAT('O-----')
```

30590 FORMAT('OTHE TYPE OF THE BASIC EVENT ',14,' SHOULD BE EITHER 1
1OR 2.')

```

30600  FORMAT('OTYPE OF BASIC EVENT:',12)
30610  FORMAT('OTHE PRE-DEMAND CLASS OF THIS BASIC EVENT SHOULD BE EITH
1ER 1, 2, 3, OR 4, NOT ',12,'.')
```

30620 FORMAT('OBASIC EVENT PRE-DEMAND CLASS: 1 (CONSTANT UNAVAILABI
1TY).')

30630 FORMAT('OBASIC EVENT PRE-DEMAND CLASS: 2 (NONREPAIRABLE).')

30640 FORMAT('OBASIC EVENT PRE-DEMAND CLASS: 3 (CONSTANTLY MONITORED)
1.')

30650 FORMAT('OBASIC EVENT PRE-DEMAND CLASS: 4 (PERIODICALLY TESTED).
1.')

30660 FORMAT('OPRE-DEMAND UNAVAILABILITY = ',E12.5)

30670 FORMAT('OPRE-DEMAND HAZARD RATE = ',E12.5,' 1/HR.')

30671 FORMAT('OUNAVAILABILITY PER DEMAND = ',E12.5)

30680 FORMAT('OPRE-DEMAND HAZARD RATE = ',E12.5,' 1/HR',10X,'PRE-DEMAND
1 REPAIR TIME = ',F8.2,' HRS.')

30690 FORMAT('OPRE-DEMAND HAZARD RATE = ',E12.5,' 1/HR',10X,'PERIODIC T
1EST INTERVAL = ',F8.2,' HRS.')

30700 FORMAT('OFIRST TEST INTERVAL = ',F8.2,' HRS',10X,'TEST PERIOD =
1',F8.2,' HRS.')

30710 FORMAT('OREPAIR PERIOD = ',F8.2,' HRS',10X,'OVERRIDE UNAVAILABI
1LITY = ',E12.5)

30720 FORMAT('OPROBABILITY OF A TEST CAUSED FAILURE = ',E12.5,10X,'DETE
1CTION INEFFICIENCY = ',E12.5)

30730 FORMAT('OUNDETECTED HAZARD RATE = ',E12.5,' 1/HR',10X,'UNAVAILAB
1ILITY PER DEMAND = ',E12.5)

30740 FORMAT('OTHE POST-DEMAND CLASS FOR BASIC EVENT #',14,' (',13,')
1IS NOT ACCEPTABLE.')

30750 FORMAT('OBASIC EVENT POST-DEMAND CLASS: 1 (CONSTANT UNAVAILABI
1TY).')

30760 FORMAT('OBASIC EVENT POST-DEMAND CLASS: 2 (NONREPAIRABLE).')

30770 FORMAT('OBASIC EVENT POST-DEMAND CLASS : 3 (CONSTANTLY MONITORED)
1.')

30780 FORMAT('OPOST-DEMAND CONSTANT UNAVAILABILITY = ',E12.5)

30790 FORMAT('OPOST-DEMAND HAZARD RATE = ',E12.5,' 1/HR.')

30800 FORMAT('OPOST-DEMAND HAZARD RATE = ',E12.5,' 1/HR',10X,'POST-DE
1MAND REPAIR TIME = ',E12.5,' HRS.')

30810 FORMAT('OTHE BASIC EVENT IN INFORM(',12,',',13,',',12,') = ',15,
1' IS NOT ACCEPTABLE.')

30820 FORMAT('OTHE BASIC EVENT IN JNFORM(',12,',',13,',',12,') = ',15,
1' IS NOT ACCEPTABLE.')

C
C
C

4000 LEVEL

```

40500  FORMAT('OTHE "TIME" DATA GROUP IS EITHER MISSING OR DISPLACED.')
```

```

40510  FORMAT(10F8.2)
```

```

40520  FORMAT('OAN ERROR HAS BEEN DETECTED IN THE "TIME" DATA GROUP.')
```

```

40530  FORMAT('OTHE MISSION TIME FOR SYSTEM ',12,' MUST BE GREATER THAN
10R EQUAL TO ZERO.')
```

```

40540  FORMAT('OTHE MINIMAL INTEGRATION INTERVAL FOR SYSTEM ',12,' MUST
1 BE GREATER THAN ZERO.')
```

```

40550  FORMAT('OTHE "TIME" DATA GROUP MUST BE FOLLOWED BY THE NUMBER -1
1.')
```

C
C 5000 LEVEL

```

C
50500 FORMAT('0THE "PRINT" DATA GROUP IS EITHER MISSING OR DISPLACED.')
50510 FORMAT('1THE DISCONTINUITY TIME POINTS WILL NOT BE PRINTED.')
50520 FORMAT('1THE DISCONTINUITY TIME POINTS WILL BE PRINTED.')
50530 FORMAT('0THE "PRINT" DATA GROUP MUST BE FOLLOWED BY THE NUMBER -
11.')

```

C
C 6000 LEVEL

```

C
60500  FORMAT('O THE "INITIATING EVENT" DATA GROUP IS EITHER MISSING OR
        1D IS PLACED.')
```

```

60501  FORMAT(F10.2,E10.5)
60502  FORMAT(E10.5)
60510  FORMAT('1AN ERROR HAS BEEN DETECTED BY SUBROUTINE "START".')
60520  FORMAT('0THE FIRST DATA POINT FOR THE INITIATING EVENT MUST BE Z
1ERO, NOT ',E10.5)

```

```

60530  FORMAT('OTHE PROGRAM CANNOT BE EXECUTED.')
60540  FORMAT('OTHE LAST DATA POINT FOR THE INITIATING EVENT MUST BE AT
1  "TFINAL", NOT ',E10.5)
60560  FORMAT('O100 TIME POINTS HAVE BEEN ENTERED FOR THE INITIATING EV
1ENT FREQUENCY.')
```

```

60570  FORMAT('OTHE NEXT CARD MUST CONTAIN THE NUMBER -1, NOT ',F10.2)
60600  FORMAT(E10.5)
60610  FORMAT('OTHE "INITIATING EVENT" DATA GROUP MUST BE FOLLOWED BY T
      1THE NUMBER -1.')
60620  FORMAT('OTHE ROF FOR THE INITIATING EVENT IS ',E10.5,' .')
```

C
C 7000 LEVEL

```

70500  FORMAT('OTHE "RUN" DATA GROUP IS EITHER MISSING OR DISPLACED.')
70510  FORMAT('OTHE KEYWORD "',A3,'" IS NOT ACCEPTABLE.')
70520  FORMAT(1015)
70530  FORMAT('OAFTER THE DATA FOR THE "RUN" DATA GROUP, THE PROGRAM M
1ST READ A -1, NOT ',12)
70540  FORMAT(F6.5)
      END

```

```

70500  FORMAT('0THE "RUN" DATA GROUP IS EITHER MISSING OR DISPLACED.')
70510  FORMAT('0THE KEYWORD "',A3,'" IS NOT ACCEPTABLE.')
70520  FORMAT(1015)
70530  FORMAT('0AFTER THE DATA FOR THE "RUN" DATA GROUP, THE PROGRAM MU
1ST READ A -1, NOT ',12)
70540  FORMAT(F6.5)
      END

```

```

70510  FORMAT(' THE KEYWORD ---,A3,--- IS NOT ACCEPTABLE.')
70520  FORMAT(10I5)
70530  FORMAT('OAFTER THE DATA FOR THE "RUN" DATA GROUP, THE PROGRAM MU
1ST READ A -1, NOT ',I2)
70540  FORMAT(F6.5)
      END

```

```
70540  FORMAT(F6.5)
      END
```

END

```

SUBROUTINE PREPAR
COMMON  INFORM( 3, 20, 5), JNFORM(3, 20, 20), RBE( 300,12), NDP
COMMON  IBE( 300,3), MCSTYP(3, 20), NUMMCS(3), NUMMPS ( 3)
COMMON  NUMRUN(3), IHELP(1000), TRUN(3), BASE( 300 )
COMMON  MPSVCT(10, 20), ROFVCT(100,2), TFINAL
COMMON  TPRIME, DPRIME, FIRST, FINAL, NS
COMMON  DELTA1, DELTA2, BOUND , IDELTA
COMMON  DELTAP, TDIFF, DELTA, NIM, IND01
COMMON  NBE, IND02, IND03, IND04 , IND05
COMMON  IND10, IND09, IND08, IND07, IND06
COMMON  JDELTA(3), DLTPR (3)
C*****
C
C   SHOULD THE COMMON BASIC EVENTS BE DELETED BY SUBROUTINE PREPAR?*
C
C*****
      IF(( IND09.EQ.1).AND.(NS.GT.1))          GO TO 20000
      IF(NS.EQ.1)                               GO TO 10520
      WRITE(21,1010)
      WRITE(21,1011)
      GO TO 10520
20000  CONTINUE
      WRITE(21,1020)
      WRITE(21,1021)
C
C   DELETE THE COMMON BASIC EVENTS IN THE VECTOR INFORM(3,20,5).
C
C   INITIALIZE THE VECTOR IHELP(300).
C
      INDIC1=1
      IHELP(1)=INFORM(1,1,1)
      DO 20010 IMCS=1,20
        IF(INFORM(1,IMCS,1).EQ.0)          GO TO 20011
        DO 20020 IBAS=1,5
          IF(INFORM(1,IMCS,IBAS).EQ.0)      GO TO 20010
          DO 20030 II=1,INDIC1
            IF(INFORM(1,IMCS,IBAS).EQ.IHELP(II))
              GO TO 20020
          CONTINUE
          INDIC1=INDIC1+1
          IHELP(INDIC1)=INFORM(1,IMCS,IBAS)
        CONTINUE
      CONTINUE
      CONTINUE
      CONTINUE
      INDIC2=INDIC1
C
C   DELETE THE BASIC EVENTS IN SYSTEM ISYS AND IMPLEMENT THE VECTOR
C   IHELP(300).
C

```



```

DO 20040 ISYS=2,3
  IEVENT=0
  IF( INFORM( ISYS,1,1).EQ.0)
    GO TO 20041
  DO 20050 IMCS=1,20
    IF( INFORM( ISYS,IMCS,1).EQ.0)
      GO TO 20051
    DO 20060 IBAS=1,5
      CONTINUE
      IF( INFORM( ISYS,IMCS,IBAS).EQ.0)
        GO TO 20050
      DO 20070 II=1,INDIC1
        IF( INFORM( ISYS,IMCS,IBAS).EQ.IHELP(II))
          GO TO 20080
      GO TO 20070
    GO TO 20070
  GO TO 20070
C
C   THE BASIC EVENT APPEARS IN AT LEAST ONE OF THE PRECEDING
C   SYSTEMS.  DELETE IT FROM THE CURRENT SYSTEM.
C
20080      CONTINUE
          IEVENT=INFORM( ISYS,IMCS,IBAS)
          DO 21080 JJ=IBAS,4
            INFORM( ISYS,IMCS,JJ)=INFORM( ISYS,IMCS,JJ+1)
          CONTINUE
          INFORM( ISYS,IMCS,10)=0
          IF( INFORM( ISYS,IMCS,1).NE.0)
            GO TO 21060
          WRITE(21,1030)
          WRITE(21,1050)
          WRITE(21,1051)
          WRITE(21,1060) IMCS,ISYS
          WRITE(21,1070)
          WRITE(21,1080)
          STOP
          CONTINUE
21060
C
C   DELETE THE MPS'S WHICH CONTAIN THE BASIC EVENT
C   DELETED IN THE MCS 'IMCS' (INFORM( ISYS,IMCS,IBAS)).
C
          IF(IND01.NE.1)
            GO TO 21061
          DO 30000 JMPS=1,20
            IF(JNFORM( ISYS,JMPS,1).EQ.0)
              GO TO 30001
            DO 30010 JBAS=1,20
              IF(JNFORM( ISYS,JMPS,JBAS).EQ.0)
                GO TO 30011
              IF(JNFORM( ISYS,JMPS,JBAS).EQ.IEVENT)
                GO TO 30020
            CONTINUE
          CONTINUE
          CONTINUE
          THE MPS 'JMPS' DOES NOT CONTAIN THE BASIC
          EVENT INFORM( ISYS,IMCS,IBAS).  SELECT THE
          NEXT 'MPS'.
          GO TO 30000

```

```

C
C
C      THE MPS 'JMPS' CONTAINS THE BASIC EVENT
C      INFORM( ISYS, IMCS, IBAS).  DELETE 'JMPS'.
C
30020      CONTINUE
          DO 30030 LL1=JMPS,19
            IF(JNFORM( ISYS,LL1,1).EQ.0)
              GO TO 30031
            DO 30040 LL2=1,20
              JNFORM( ISYS,LL1,LL2)=JNFORM( ISYS,
                LL1+1,LL2)
              IF(JNFORM( ISYS,LL1,LL2).EQ.0)
                GO TO 30030
            CONTINUE
          CONTINUE
30030      CONTINUE
30031      CONTINUE
          JNFORM( ISYS,20,1)=0
30000      CONTINUE
30001      CONTINUE
          GO TO 21061
20070      CONTINUE
C
C      THE BASIC EVENT DOES NOT APPEAR IN ANY OF THE PRECEDING
C      SYSTEMS.
C
          INDIC2=INDIC2+1
          IHELP(INDIC2)=INFORM( ISYS, IMCS, IBAS)
20060      CONTINUE
20050      CONTINUE
20051      CONTINUE
          INDIC1=INDIC2
20040      CONTINUE
20041      CONTINUE
10520      CONTINUE
C*****
C
C      LOAD THE VECTOR MCSTYP(3,20).
C
C*****
C
C      INITIALIZE THE VECTOR MCSTYP(3,20).
C
          KOUNT=0
          DO 10500 ISYS=1,3
            DO 10510 IMCS=1,20
              MCSTYP( ISYS, IMCS)=1
            CONTINUE
          CONTINUE
10510      CONTINUE
10500      CONTINUE
C
C      CHECK FOR THE MCS'S WHICH CONTAIN BASIC EVENTS OF TYPE 2 ONLY
C      (FAILURE TO START ONLY).
C

```

```

DO 10000 ISYS=1,NS
  IF(INFORM(ISYS,1,1).EQ.0) GO TO 10001
  DO 10010 IMCS=1,NUMMCS(ISYS)
    IF(INFORM(ISYS,IMCS,1).EQ.0) GO TO 10011
    DO 10020 IBAS=1,10
      IF(INFORM(ISYS,IMCS,IBAS).EQ.0) GO TO 10021
      IF(1BE(INFORM(ISYS,IMCS,IBAS),1).EQ.1) GO TO 10010
    CONTINUE
  CONTINUE
10020 KOUNT=KOUNT+1
      MCSTYP(ISYS,IMCS)=2
10010 CONTINUE
10011 CONTINUE
      WRITE(21,1000) KOUNT,ISYS
      WRITE(21,1001)
      NUMRUN(ISYS)=NUMMCS(ISYS)-KOUNT
      KOUNT=0
10000 CONTINUE
10001 CONTINUE
      RETURN
C*****
C
C          FORMATS
C
C*****
1000 FORMAT('1 THERE ARE ',13,' MCS'S IN SYSTEM ',12,' WHICH ')
1001 FORMAT('0 REPRESENT A SYSTEM FAILURE TO START ONLY.')
```

1010 FORMAT('0 THE COMMON BASIC EVENTS HAVE NOT BEEN DELETED BY ',
1 'SUBROUTINE PREPAR.')

1011 FORMAT('0 THE RESULT IS A LOWER BOUND TO THE "ENF".')

1020 FORMAT('0 THE COMMON BASIC EVENTS HAVE BEEN DELETED BY ',
1 'SUBROUTINE PREPAR.')

1021 FORMAT('0 THE RESULT IS AN UPPER BOUND TO THE "ENF".')

1030 FORMAT('1')

1040 FORMAT('0')

1050 FORMAT(' THE DELETING OF THE BASIC EVENTS WHICH ARE SHARED '
1 ', 'BY TWO OR MORE FAULT TREES HAS ')

1051 FORMAT('0 CAUSED ONE OF THE TOP EVENTS TO EXIST.')

1060 FORMAT('0 THE MCS # ',13,' OF THE FAULT TREE # ',12,' IS DOWN.')

1070 FORMAT('0 EITHER THE FAULT TREE ORDER MUST BE CHANGED OR THE ',
1 'FAULT TREE MUST NOT APPEAR IN THE INPUT DATA.')

1080 FORMAT('0 THE PROGRAM WILL NOT BE EXECUTED.')

END

SUBROUTINE TIMES (IN)

THE SUBROUTINE "TIMES" CALCULATES AND STORES ALL THE TIME POINTS AT WHICH THE ACCIDENT SEQUENCE UNDEPENDABILITY EXPERIENCES A DISCONTINUITY. "TIMES" ALSO SELECTS THE NUMERICAL INTEGRATION METHOD TO BE USED IN THE COMPUTATION OF THE EXPECTED NUMBER OF FAILURES IN THE MAIN PROGRAM. IF THE NUMERICAL METHOD IS SIMPSON'S RULE, "TIMES" COMPUTES THE NUMBER OF DATA POINTS TO BE USED IN THE INTEGRATION. THE VARIABLES USED IN THIS SUBROUTINE ARE THE FOLLOWING:

DISDAT(1)	THIS VECTOR STORES THE TIME POINTS AT WHICH THE SYSTEM UNDEPENDABILITY EXPERIENCES A DISCONTINUITY.
MOD	THE DISCONTINUITY TIME POINTS FOR EACH BASIC EVENT REPEAT THEMSELVES PERIODICALLY STARTING ON THE SECOND TEST INTERVAL. "MOD" CONTAINS THE MAXIMUM NUMBER OF SUCH REPETITIONS.
HELP	THIS IS AN AUXILIARY VARIABLE USED TO STORE THE DISCONTINUITY TIME POINTS WHEN THE VECTOR "DISDAT(1)" IS ORDERED TO FORM AN INCREASING SET OF DATA POINTS.
KFINAL	THE NUMBER OF NON-ZERO POINTS IN THE VECTOR "DISDAT(1)".
IHELP, AHELP, AND RHELP	THESE ARE AUXILIARY VARIABLES USED TO DETERMINE IF "NDP" IS ODD.
MM	A COUNTER USED WHEN LOADING DISDAT(1).

ALL OTHER VARIABLES AND VECTORS USED IN THIS SUBROUTINE HAVE BEEN DEFINED IN THE MAIN PROGRAM.

```
COMMON INFORM( 3, 20, 5), JNFORM(3, 20, 20), RBE( 300,12), NDP
COMMON IBE( 300,3), MCSTYP(3, 20), NUMMCS(3), NUMMPS ( 3)
COMMON NUMRUN(3), IHELP(1000), TRUN(3), BASE( 300 )
COMMON MPSVCT(10, 20), ROFVCT(100,2), TFINAL
COMMON TPRIME, DPRIME, FIRST, FINAL, NS
COMMON DELTA1, DELTA2, BOUND , IDELTA
```

```

COMMON          DELTAP, TDIFF, DELTA, NIM, IND01
COMMON          NBE, IND02, IND03, IND04, IND05
COMMON          IND10, IND09, IND08, IND07, IND06
COMMON          JDELTA(3),          DLTPR (3)
DIMENSION DISDAT(1000)
IF(IN.NE.1) GO TO 10000

C
C
C
C
C
C
C          INITIALIZE THE VECTOR DISDAT(I)
C
C          DO 15 I=1,1000
C          DISDAT(I)=0.0
15          CONTINUE
C
C          LOAD THE VECTOR DISDAT(I) WITH THE FIRST TEST INTERVAL
C
C          J=1
C          DO 1000 I=1,NBE
C          IF(IBE(I,2).NE.4) GO TO 1000
C          DISDAT(J)=RBE(I,3)
C          DISDAT(J+1)=RBE(I,3)+RBE(I,4)
C          DISDAT(J+2)=RBE(I,3)+RBE(I,4)+RBE(I,5)
C          J=J+3
1000         CONTINUE
C          IF(J.EQ.1)          GO TO 80000
C
C          IMPLEMENT THE VECTOR DISDAT(I)
C
C          MM=1
C          DO 20 I=1,10
C          IF(IBE(I,2).NE.4) GO TO 20
C          DISDAT( J)=DISDAT( MM)+RBE(I,2)
C          DISDAT(J+1)=DISDAT(MM+1)+RBE(I,2)
C          DISDAT(J+2)=DISDAT(MM+2)+RBE(I,2)
C          MM=MM+3
C          J= J+3
C          MOD=INT((TFINAL-RBE(I,3))/RBE(I,2))
C          IF(MOD.LE.1) GO TO 20
C          DO 30 K=1,MOD-1
C          DISDAT( J)=RBE(I,2)+DISDAT(J-3)
C          DISDAT(J+1)=RBE(I,2)+DISDAT(J-2)
C          DISDAT(J+2)=RBE(I,2)+DISDAT(J-1)
C          J=J+3
30          CONTINUE
20          CONTINUE
C
C          SET TO ZERO THE UNNECESSARY TIME POINTS
C

```

```

DO 40 I=1,J-1
DO 50 II=I+1,J-1
IF(DISDAT(II).NE.DISDAT(I)) GO TO 50
DISDAT(II)=0.0
CONTINUE
CONTINUE
50
40
C
C   DELETE DATA POINTS GREATER THAN OR EQUAL TO TFINAL
C
DO 9000 K1=1,J
IF(DISDAT(K1).LT.TFINAL) GO TO 9000
DISDAT(K1)=0.0
CONTINUE
9000
C
C   COUNT THE NUMBER OF TIME POINTS
C
KK=0
DO 70 I=1,J-1
IF(DISDAT(I).EQ.0.0) GO TO 70
KK=KK+1
CONTINUE
70
C
C   DISREGARD THE ZEROS IN THE VECTOR
C
DO 80 I=1,J
IF(I.GE.KK) GO TO 80
IF(DISDAT(I).NE.0.0) GO TO 80
DO 90 II=I,J
DISDAT(II)=DISDAT(II+1)
CONTINUE
GO TO 81
80
CONTINUE
C
C   REORDER THE TIME POINTS TO FORM AN INCREASING SET
C
100
L=0
JJ=KK-1
DO 110 I=1,JJ
IF(DISDAT(I).LT.DISDAT(I+1)) GO TO 110
HELP=DISDAT(I)
DISDAT(I)=DISDAT(I+1)
DISDAT(I+1)=HELP
L=L+1
CONTINUE
110
IF(L.NE.0) GO TO 100
C
C   INPUT THE LAST ELEMENT IN VECTOR DISDAT(I)
C
DISDAT(KK+1)=TFINAL
KFINAL=KK+1
GO TO 80100
80000 CONTINUE

```

```

DISDAT(1)=TFINAL
80100 CONTINUE
C
C PRINT THE VECTOR DISDAT(1) (IF ASKED).
C
IF(IND10.NE.1) GO TO 10600
WRITE(21,10090)
WRITE(21,10100)
WRITE(21,10110)
WRITE(21,10120)
WRITE(21,10100)
WRITE(21,10130)
DO 10500 LL=1,KFINAL
WRITE(21,10140) DISDAT(LL)
10500 CONTINUE
10600 CONTINUE
C
C SELECT THE FIRST INTEGRATION INTERVAL
C
FIRST=0.0
FINAL=DISDAT(1)
GO TO 115
C
C "TIMES" HAS BEEN CALLED AT LEAST TWO "TIMES"
C
10000 CONTINUE
FIRST=DISDAT(IN-1)
FINAL=DISDAT(IN )
115 CONTINUE
C
C SELECT THE NUMERICAL INTEGRATION METHOD
C
DELTA=(FINAL-FIRST)
IF(DELTA.LE.DELTA1) GO TO 120
IF(DELTA.LE.DELTA2) GO TO 130
C*****
C
C SIMPSON'S RULE
C
C*****
NIM=3
C
C SELECT THE NUMBER OF DATA POINTS
C
NDP=INT(DELTA/DELTA2)+1
AHELP=FLOAT(INT(NDP/2.))
RHELP=NDP/2.
IF(RHELP.NE.AHELP) GO TO 140
NDP=NDP+1
140 CONTINUE
RETURN

```

```

C*****
C
C                                RECTANGULAR RULE                                *
C                                                                *
C*****
120                                CONTINUE
                                NIM=1
                                RETURN
C*****
C
C                                TRAPEZOIDAL RULE                                *
C                                                                *
C*****
130                                CONTINUE
                                NIM=2
                                RETURN

C
C    FORMATS
C
10090  FORMAT('1')
10100  FORMAT('0-----')
10110  FORMAT('0 THE DISCONTINUITY TIME POINTS')
10120  FORMAT('0 ( TIME IN HOURS )')
10130  FORMAT('0')
10140  FORMAT(1X,F10.5)
END

```


SUBROUTINE UNDEPE(1SYS,UI)

THE SUBROUTINE "UNDEPE" CONTROLS THE COMPUTATION OF THE TIME-DEPENDENT UNDEPENDABILITY FOR EACH SYSTEM IN THE ACCIDENT SEQUENCE. THIS IS ACCOMPLISHED BY CALLING SUBROUTINES "CUTS" AND "RECKON" AND BY PERFORMING A NUMERICAL INTEGRATION USING SIMPSON'S RULE. THE NOTATION USED IN THIS SUBROUTINE IS THE FOLLOWING:

1SYS THE SYSTEM IDENTIFICATION NUMBER (1,...,NS).
 UI THE SYSTEM UNDEPENDABILITY AT "TPRIME".
 SUM THIS VARIABLE HAS BEEN DEFINED IN SUBROUTINE "CUTS."
 PDF(1) THE PROBABILITY DENSITY FUNCTION FOR THE TIME TO FIRST SYSTEM FAILURE (SYSTEM "1SYS")
 PFRO AUXILIARY VARIABLES USED IN THE NUMERICAL AND INTEGRATION OF PDF(1).
 PFR THE PROBABILITY OF A SYSTEM FAILURE TO RUN GIVEN THAT A DEMAND OCCURS AT "TPRIME" AND THAT THE SYSTEM STARTS.
 PFS THE PROBABILITY OF A SYSTEM FAILURE TO START ON DEMAND AT "TPRIME".

COMMON INFORM(3, 20, 5), JNFORM(3, 20, 20), RBE(300,12), NDP
 COMMON IBE(300,3), MCSTYP(3, 20), NUMMCS(3), NUMMPS (3)
 COMMON NUMRUN(3), IHELP(1000), TRUN(3), BASE(300)
 COMMON MPSVCT(10, 20), ROFVCT(100,2), TFINAL
 COMMON TPRIME, DPRIME, FIRST, FINAL, NS
 COMMON DELTA1, DELTA2, BOUND, IDELTA
 COMMON DELTAP, TDIFF, DELTA, NIM, IND01
 COMMON NBE, IND02, IND03, IND04, IND05
 COMMON IND10, IND09, IND08, IND07, IND06
 COMMON JDELTA(3), DLTPR (3)
 DIMENSION PDF(101)
 EPS=.001

IF((TPRIME+EPS).NE.8403.).AND.
 ((TPRIME+EPS).NE.8038.).AND.

1

```

2          ((TPRIME+EPS).NE.7673.).AND.
3          ((TPRIME-EPS).NE.8403.).AND.
4          ((TPRIME-EPS).NE.8038.).AND.
5          ((TPRIME+EPS).NE.7308.).AND.
6          ((TPRIME-EPS).NE.7308.).AND.
7          ((TPRIME+EPS).NE.6578.).AND.
8          ((TPRIME-EPS).NE.6578.).AND.
9          ((TPRIME-EPS).NE.7673.)) GO TO 44447
          IF(TPRIME.LT.7670) GO TO 44447
          DO 44444 I=1,NBE
              WRITE(21,44445) I,BASE(I)
44444      CONTINUE
44447      CONTINUE
44445  FORMAT('O      BASE ( ',14,' ) = ',E12.7)
C
C          INITIALIZATION:
C
C          PFS=0.0
C          PFR=0.0
C          DO 20000 LL=1,101
C              PDF(LL)=0.0
20000      CONTINUE
C
C          COMPUTE THE PROBABILITY THAT THE SYSTEM FAILS TO START
C          AT T'. THIS IS ACCOMPLISHED BY CALLING SUBROUTINE "CUTS."
C
C          IF(IND08.NE.1)                                GO TO 1000
C          CALL CUTS (ISYS,SUM)
C          PFS=SUM
C          IF(IND05.EQ.1)                                GO TO 1000
C              UI=PFS
C              RETURN
1000      CONTINUE
C
C          COMPUTE THE VALUE OF THE DENSITY FUNCTION AT EACH ONE OF
C          THE IDELTA TIME POINTS.
C
C          DO 2000 I=1, IDELTA
C              TDIFF=(I-1)*DELTAP
C              IF(I.NE. IDELTA)                            GO TO 2001
C              TDIFF=TRUN(ISYS)
2001      CONTINUE
C          CALL RECKON (SUM,ISYS)
C          PDF(I)=SUM
2000      CONTINUE
C
C          IMPLEMENTATION OF SIMPSON'S RULE
C
C          PFRO=0.0
C          PFRE=0.0
C          DO 3000 LL=2, IDELTA-1,2
C              PFRE=PFRE+PDF(LL)

```

```

3000          CONTINUE
              IF(IDELTA.LT.5)
              DO 3010 LL=3, IDELTA-2, 2
              PFRQ=PFRQ+PDF(LL)
3010          CONTINUE
3011          CONTINUE
C
C          COMPUTE THE PROBABILITY THAT THE SYSTEM FAILS TO RUN
C          DURING THE MISSION GIVEN THAT A DEMAND OCCURS AT T',
C          AND THE SYSTEM STARTS AT T'.
C
          PFR=(DELTAP/3.)*(PDF(1)+4.*PFRE+2.*PFRQ+PDF(IDELTA))
C
C          COMPUTE THE UNDEPENDABILITY AT T'.
C
          UI=PFS+PFR
          WRITE(21,55501) TPRIME,PFS,PFR
55501        FORMAT(' PFS AND PFR AT TIME ',F8.2,'=', E12.7,5X,E12.7)
          RETURN
          END

```

```

C      SUBROUTINE BASIC1
C          SUBROUTINE "BASIC1" CONTROLS THE COMPUTATION OF THE
C
C      THE BASIC EVENT UNAVAILABILITIES AT TIME "TPRIME" (T'). ALL
C
C      THE VARIABLES USED IN THIS SUBROUTINE HAVE ALREADY BEEN
C
C      DEFINED IN THE MAIN PROGRAM.
C
C      COMMON INFORM( 3, 20, 5), JNFORM(3, 20, 20), RBE( 300,12), NDP
C      COMMON IBE( 300,3), MCSTYP(3, 20), NUMMCS(3), NUMMPS ( 3)
C      COMMON NUMRUN(3), IHELP(1000), TRUN(3), BASE( 300 )
C      COMMON MPSVCT(10, 20), ROFVCT(100,2), TFINAL
C      COMMON TPRIME, DPRIME, FIRST, FINAL, NS
C      COMMON DELTA1, DELTA2, BOUND, IDELTA
C      COMMON DELTAP, TDIFF, DELTA, NIM, IND01
C      COMMON NBE, IND02, IND03, IND04, IND05
C      COMMON IND10, IND09, IND08, IND07, IND06
C      COMMON JDELTA(3), DLTPR (3)
C
C          INITIALIZE THE VECTOR BASE(1000).
C
C          DO 10000 I=1,NBE
C          BASE(I)=0.0
C          CONTINUE
10000
C
C      SELECT THE BASIC EVENT (K).
C
C      DO 20000 K=1,NBE
C          IF(IBE(K,2).EQ.1) GO TO 20100
C          IF(IBE(K,2).EQ.2) GO TO 20200
C          IF(IBE(K,2).EQ.3) GO TO 20300
C          IF(IBE(K,2).EQ.4) GO TO 20400
C
C      K IS A CONSTANT UNAVAILABILITY BASIC EVENT.
C
C      20100          CONTINUE
C                   BASE(K)=RBE(K,10)
C                   GO TO 20000
C
C      K IS A NONREPAIRABLE BASIC EVENT.
C
C      20200          CONTINUE
C                   BASE(K)=FNRA(RBE(K,1),TPRIME,RBE(K,10))
C                   GO TO 20000
C
C      K IS A CONSTANTLY MONITORED BASIC EVENT.
C
C      20300          CONTINUE
C                   BASE(K)=FCMA(RBE(K,1),RBE(K,5),RBE(K,10))
C                   GO TO 20000

```

```

C
C      K IS A PERIODICALLY TESTED BASIC EVENT.
C
20400      CONTINUE
          BASE(K)=FPTA(RBE(K,1),RBE(K,2),RBE(K,3),RBE(K,4),
1          RBE(K,5),RBE(K,6),RBE(K,7),RBE(K,8),RBE(K,9),
2          RBE(K,10),TPRIME)
C
20000 CONTINUE
C
C      THE UNAVAILABILITY HAS BEEN COMPUTED FOR 'NBE' BASIC EVENTS.
C      RETURN TO THE MAIN PROGRAM.
C
      RETURN
      END

```

```

SUBROUTINE BASIC2 (NUMBER,BEUNAV)

C      THE SUBROUTINE "BASIC2" CONTROLS THE COMPUTATION OF
C      THE BASIC EVENT UNAVAILABILITIES AT TIME "DPRIME"      (T")
C      FOLLOWING THE OCCURRENCE OF THE INITIATING EVENT AT     TIME
C      "TPRIME" (T'). ALL THE VARIABLES AND VECTORS USED IN THIS
C      SUBROUTINE HAVE ALREADY BEEN DEFINED IN THE MAIN PROGRAM.
C
COMMON  INFORM( 3, 20, 5), JNFORM(3, 20, 20), RBE( 300,12), NDP
COMMON  IBE( 300,3), MCSTYP(3, 20), NUMMCS(3), NUMMPS ( 3)
COMMON  NUMRUN(3), IHELP(1000), TRUN(3), BASE( 300 )
COMMON  MPSVCT(10, 20), ROFVCT(100,2), TFINAL
COMMON  TPRIME, DPRIME, FIRST, FINAL, NS
COMMON  DELTA1, DELTA2, BOUND , IDELTA
COMMON  DELTAP, TDIFF, DELTA, NIM, IND01
COMMON  NBE, IND02, IND03, IND04 , IND05
COMMON  IND10, IND09, IND08, IND07, IND06
COMMON  JDELTA(3),          DLTPR (3)

C      WHAT IS THE TYPE OF BASIC EVENT?
C
C      IF(IBE(NUMBER,1).NE.1)                      GO TO 11000
C
C      THE BASIC EVENT IS OF TYPE 1. WHAT IS THE BASIC EVENT POST-
C      DEMAND CLASS?
C
C      IF(IBE(NUMBER,3).EQ.2)                      GO TO 20000
C
C      THE BASIC EVENT POSTDEMAND CLASS IS 3:
C
C      THE BASIC EVENT IS REPAIRABLE (CONSTANTLY MONITORED).
C
C      BEUNAV=FCME(RBE(NUMBER,11),RBE(NUMBER,12),BASE(NUM
1      BER))
C      RETURN
20000    CONTINUE
C
C      THE BASIC EVENT POSTDEMAND CLASS IS 2:
C
C      THE BASIC EVENT IS NONREPAIRABLE.
C
C      BEUNAV=FNRE(RBE(NUMBER,11),TDIFF,BASE(NUMBER))
C      RETURN
11000    CONTINUE
C
C      THE BASIC EVENT IS OF TYPE 2.
C

```

```
BEUNAV=BASE( NUMBER )  
RETURN  
END
```



```

C
C THE PROBABILITY THAT THE BASIC EVENT INFORM(1SYS,J,K) FAILS
C IN DT" GIVEN THAT IT IS UP AT T".
C
PUNA=PUNA*RBE(INFORM(1SYS,J,K),11)
C
C THE PROBABILITY THAT ALL THE REMAINING BASIC EVENTS IN MCS
C J ARE DOWN AT T".
C
DO 1050 KP=1,5
IF(KP.EQ.K) GO TO 1050
IF(INFORM(1SYS,J,KP).EQ.0) GO TO 1060
CALL BASIC2(INFORM(1SYS,J,KP),BEUNAV)
PUNA=PUNA*BEUNAV
1050 CONTINUE
1060 CONTINUE
C
C COMPUTE THE PROBABILITY THAT THE SYSTEM IS UP AT T".
C
IF(IND03.EQ.1.AND.IND01.EQ.1.AND.NUMRUN(1SYS).GT.1) GO TO 1070
GO TO 1080
1070 CONTINUE
C
C SELECT THE MPS'S WHICH CONTAIN THE BASIC EVENT INFORM(1SYS,J,K).
C
C
C INITIALIZE THE VECTOR MPSVCT(10,20):
C
DO 10705 INIT1=1,10
DO 10706 INIT11=1,20
MPSVCT(INIT1,INIT11)=0
10706 CONTINUE
10705 CONTINUE
DO 10710 LL2=1,NUMMPS(1SYS)
DO 10720 LL3=1,20
IF(JNFORM(1SYS,LL2,LL3).EQ.0) GO TO 10710
IF(JNFORM(1SYS,LL2,LL3).NE.INFORM(1SYS,J,K)) GO TO 10720
C
C THE MPS 'LL2' CONTAINS THE BASIC EVENT INFORM(1SYS,J,K).
C
C
C IS THE VECTOR MPSVCT(10,20) OVERLOADED?
C
IF(111.GT.10) GO TO 1080
C
C DOES THE MPS CONTAIN ANY OF THE REMAINING BASIC EVENTS IN
C MCS 'J'?
C
DO 10730 LL4=1,5
IF(INFORM(1SYS,J,LL4).EQ.0) GO TO 10731
IF(LL4.EQ.K) GO TO 10730
DO 10740 LL5=1,20

```

```

      IF(INFORM(ISYS,J,LL4).NE.JNFORM(ISYS,LL2,LL5)) GO TO 10740
C
C      MPS LL2 IS DOWN AT T". SELECT THE NEXT MPS.
C
      GO TO 10710
10740 CONTINUE
10730 CONTINUE
10731 CONTINUE
C
C      IS THE MPS LL2 A 1 BASIC EVENT MPS?
C
      INTAR=0
      DO 10753 LLL6=1,20
        IF(JNFORM(ISYS,LL2,LLL6).EQ.0) GO TO 10754
        INTAR=INTAR+1
10753 CONTINUE
10754 CONTINUE
      IF(INTAR.EQ.1) GO TO 1080
C
C      MPS LL2 DOES NOT CONTAIN ANY OF THE REMAINING BASIC EVENTS
C      IN MCS 'J'. INSERT MPS LL2 IN THE VECTOR MPSVCT(10,20) AND
C      DELETE THE BASIC EVENT INFORM(ISYS,J,K).
C
      IDUMMY=0
      DO 10750 LL6=1,19
        IF(JNFORM(ISYS,LL2,LL6).EQ.0) GO TO 10709
        IF(IDUMMY.EQ.1) GO TO 10760
        IF(JNFORM(ISYS,LL2,LL6).EQ.INFORM(ISYS,J,K)) GO TO 10760
        MPSVCT(111,LL6)=JNFORM(ISYS,LL2,LL6)
        GO TO 10750
10760 CONTINUE
      IDUMMY=1
      MPSVCT(111,LL6)=JNFORM(ISYS,LL2,LL6+1)
10750 CONTINUE
      111=111+1
      GO TO 10710
10720 CONTINUE
10709 CONTINUE
      111=111+1
10710 CONTINUE
      IF(111.EQ.1) GO TO 1080
C
C      CALL SUBROUTINE "PATHS."
C
C      CALL PATHS(PROB,111-1)
      PUNA=PUNA*PROB
1080 CONTINUE
      111=1
      UNAMCS=UNAMCS+PUNA
1030 CONTINUE
1040 CONTINUE
      SUM1=SUM1+UNAMCS

```

146

```

GO TO 2030
2040 CONTINUE
2030 CONTINUE
2031 CONTINUE
C
C          COUNT THE NUMBER OF COMMON BASIC EVENTS
C
          NUMBER=0
          DO 2050 KK=1,5
            IF(IHELP(KK).EQ.0) GO TO 2051
            NUMBER=NUMBER+1
2050 CONTINUE
2051 CONTINUE
C
C          CHECK THE NUMBER OF COMMON BASIC EVENTS.
C
          IF(NUMBER.NE.0) GO TO 2060
C
          THE MCS'S 11 AND 12 SHARE NO BASIC EVENTS.
C
          GO TO 2010
2060 CONTINUE
C
C          THE MCS'S 11 AND 12 SHARE 'NUMBER' BASIC EVENTS.  LOAD THE
C          REMAINING PART OF THE VECTOR IHELP(6-15)
C
          KK=6
C
C          TAKE ALL THE BASIC EVENTS IN 11 WHICH DO NOT SHOW IN 12.
C
          DO 2070 K1=1,5
            IF(INFORM(ISYS,11,K1).EQ.0) GO TO 2071
            DO 2080 K2=1,NUMBER
              IF(INFORM(ISYS,11,K1).EQ.IHELP(K2)) GO TO 2070
2080 CONTINUE
              IHELP(KK)=INFORM(ISYS,11,K1)
              KK=KK+1
2070 CONTINUE
2071 CONTINUE
C
C          TAKE ALL THE BASIC EVENTS IN 12 WHICH DO NOT SHOW IN 11.
C
          DO 2090 K1=1,5
            IF(INFORM(ISYS,12,K1).EQ.0) GO TO 2091
            DO 2100 K2=1,NUMBER
              IF(INFORM(ISYS,12,K1).EQ.IHELP(K2)) GO TO 2090
2100 CONTINUE
              IHELP(KK)=INFORM(ISYS,12,K1)
              KK=KK+1
2090 CONTINUE
2091 CONTINUE

```

```

C
C
C      INITIALIZE THE UNAVAILABILITY OF THE
C      INTERSECTION OF THE MCS'S 11 AND 12.
C
C      UNAINTE=0.0
C
C      DO 2110 NC=1,NUMBER
C
C      SKIP THE BASIC EVENTS OF TYPE 2.  THEY WILL NOT FAIL IN DT".
C
C      IF(IBE(IHELP(NC),1).EQ.2)          GO TO 2110
C
C      THE PROBABILITY THAT THE COMMON BASIC EVENT 'NC' IS UP AT T".
C
C      CALL BASIC2(IHELP(NC),BEUNAV)
C      IF(BEUNAV.EQ.1.) GO TO 2110
C      PUNA=1.-BEUNAV
C
C      THE PROBABILITY THAT THE BASIC EVENT IHELP(NC) FAILS IN DT"
C      GIVEN THAT IT IS WORKING AT T".
C
C      PUNA=PUNA*RBE(IHELP(NC),11)
C
C      THE PROBABILITY THAT ALL THE REMAINING BASIC EVENTS IN
C      IHELP(15) ARE DOWN AT T".
C
C      DO 2120 NCP=1,15
C      IF(NCP.EQ.NC) GO TO 2120
C      IF(IHELP(NCP).EQ.0) GO TO 2120
C      CALL BASIC2(IHELP(NCP),BEUNAV)
C      PUNA=PUNA*BEUNAV
2120  CONTINUE
C
C      THE PROBABILITY THAT THE SYSTEM IS UP AT T".
C
C      IF(IND03.EQ.1.AND.IND01.EQ.1.AND.NUMRUN(ISYS).GT.2) GO TO 2130
C      GO TO 2140
2130  CONTINUE
C
C      SELECT THE MPS'S WHICH CONTAIN THE BASIC EVENTS 'NC'.
C
C      DO 20000 LL1=1,NUMMPS(ISYS)
C      DO 20010 LL2=1,20
C      IF(JNFORM(ISYS,LL1,LL2).EQ.0) GO TO 20000
C      IF(JNFORM(ISYS,LL1,LL2).NE.IHELP(NC)) GO TO 20010
C
C      THE MPS 'LL1' CONTAINS THE BASIC EVENT 'NC'.
C
C
C      IS THE VECTOR MPSVCT(10,20) OVERLOADED?
C

```

```

                IF(III.GT.10) GO TO 2140
C
C      DOES THE MPS 'LL1' CONTAINS ANY OF THE REMAINING BASIC
C      EVENTS IN IHELP(30)?
C
      DO 20020 LL4=1,15
      IF(LL4.EQ.NC) GO TO 20020
      DO 20030 LL5=1,20
      IF(IHELP(LL4).NE.JNFORM(ISYS,LL1,LL5)) GO TO 20030
C
C      THE MPS 'LL1' IS DOWN AT T".  SELECT THE NEXT MPS.
C
      GO TO 20000
20030  CONTINUE
20020  CONTINUE
C
C      THE MPS 'LL1' DOES NOT CONTAIN ANY OF THE REMAINING BASIC
C      EVENTS IN IHELP(15).  INSERT MPS 'LL1' IN THE VECTOR
C      MPSVCT(10,20) AND DELETE THE BASIC EVENT IHELP(NC).
C
      IDUMMY=0
      DO 20040 LL6=1,19
      IF(JNFORM(ISYS,LL1,LL6).EQ.0) GO TO 20000
      IF(IDUMMY.EQ.1) GO TO 20060
      IF(JNFORM(ISYS,LL1,LL6).EQ.IHELP(NC)) GO TO 20060
      MPSVCT(111,LL6)=JNFORM(ISYS,LL1,LL6)
      GO TO 20040
20060  CONTINUE
      IDUMMY=1
      MPSVCT(111,LL6)=JNFORM(ISYS,LL1,LL6+1)
20040  CONTINUE
      111=111+1
      GO TO 20000
20010  CONTINUE
20000  CONTINUE
C
C      CALL SUBROUTINE PATHS
C
C      CALL PATHS(PROB,111-1)
      PUNA=PUNA*PROB
2140  CONTINUE
      UNAINTE=UNAINTE+PUNA
2110  CONTINUE
      SUM2=SUM2+UNAINTE
2010  CONTINUE
2000  CONTINUE
      IF(NUMRUN(ISYS).NE.2) GO TO 2002
      SUM=SUM1-SUM2
      RETURN
2002  CONTINUE
C
C      IS THE THIRD SUMMATION NECESSARY?
C

```

```

BOUNDP=(SUM2/(SUM1-SUM2))*100.
IF(BOUNDP.GT.BOUND.AND.BOUNDP.GT.0.)          GO TO 3000
SUM=SUM1
RETURN
C
C*****
C
C      'NUMRUN(ISYS)' MCS'S TAKEN THREE AT A TIME
C
C*****
3000  CONTINUE
      SUM3=0.0
C
C      SELECT THE MCS'S I1, I2, AND I3.
C
      DO 3010 I1=1,NUMRUN(ISYS)-2
      IF(MCSTYP(ISYS,I1).EQ.2) GO TO 3010
      DO 3020 I2=I1+1,NUMRUN(ISYS)-1
      IF(MCSTYP(ISYS,I2).EQ.2) GO TO 3020
      DO 3030 I3=I2+1,NUMRUN(ISYS)
      IF(MCSTYP(ISYS,I3).EQ.2) GO TO 3030
C
C      LOAD THE VECTOR IHELP(0-5) WITH THE BASIC EVENTS COMMON
C
C      TO MCS'S I1, I2, AND I3:
C
C
C      INITIALIZATION
C
C      DO 3040 KK=1,20
C      IHELP(KK)=0
3040  CONTINUE
      IIV=0
C
      DO 3050 M1=1,5
      IF(INFORM(ISYS,I1,M1).EQ.0) GO TO 3051
      DO 3060 M2=1,5
      IF(INFORM(ISYS,I2,M2).EQ.0) GO TO 3050
      IF(INFORM(ISYS,I1,M1).NE.INFORM(ISYS,I2,M2)) GO TO 3060
      DO 3070 M3=1,5
      IF(INFORM(ISYS,I3,M3).EQ.0) GO TO 3050
      IF(INFORM(ISYS,I1,M1).NE.INFORM(ISYS,I3,M3)) GO TO 3070
      IIV=IIV+1
      IHELP(IIV)=INFORM(ISYS,I1,M1)
      GO TO 3050
3070  CONTINUE
      GO TO 3050
3060  CONTINUE
3050  CONTINUE
3051  CONTINUE
C
C      COUNT THE NUMBER OF COMMON BASIC EVENTS.
C

```

```

                                NUMBER=0
                                DO 3080 KK=1,5
                                IF(IHELP(KK).EQ.0) GO TO 3081
                                NUMBER=NUMBER+1
3080                                CONTINUE
3081                                CONTINUE
C
C      CHECK THE  NUMBER OF COMMON BASIC EVENTS.
C
C      IF(NUMBER.NE.0) GO TO 3090
C
C      THE MCS'S I1, I2, AND I3 SHARE NO BASIC EVENTS.
C
C      GO TO 3030
3090 CONTINUE
C
C      THE MCS'S I1, I2, AND I3 SHARE 'NUMBER' BASIC EVENTS.  LOAD
C      THE REMAINING PART OF THE VECTOR IHELP(20).
C
C      DO 3100 K1=1,5
C          IHELP(K1+ 5)=INFORM( ISYS, I1, K1)
C          IHELP(K1+10)=INFORM( ISYS, I2, K1)
C          IHELP(K1+15)=INFORM( ISYS, I3, K1)
3100 CONTINUE
C
C      DELETE ALL THE REDUNDANT BASIC EVENTS IN THE VECTOR
C      IHELP(20).
C
C      DO 3110 L1=1,19
C          IF(IHELP(L1).EQ.0) GO TO 3110
C          DO 3120 L2=L1+1,20
C              IF(IHELP(L2).EQ.0) GO TO 3120
C              IF(IHELP(L1).NE.IHELP(L2)) GO TO 3120
C              IHELP(L2)=0
1          CONTINUE
3120 CONTINUE
3110 CONTINUE
C
C          INITIALIZE THE UNAVAILABILITY  OF  THE
C          INTERSECTION OF THE MCS'S I1, I2, AND I3.
C
C          UNAINI=0.0
C
C      DO 3180 NC=1,NUMBER
C          IF(IHELP(NC).EQ.0) GO TO 3180
C
C      SKIP THE BASIC EVENTS OF TYPE 2.  THEY WILL NOT FAIL IN DT".
C
C      IF(IBE(IHELP(NC),1).EQ.2) GO TO 3180
C
C      THE PROBABILITY THAT THE COMMON BASIC EVENT 'NC' IS WORKING
C      AT T".
C

```



```

CALL BASIC2(IHELP(NC),BEUNAV)
IF(BEUNAV.EQ.1.) GO TO 3180
PUNA=1.-BEUNAV
C
C THE PROBABILITY THAT THE BASIC EVENT IHELP(NC) FAILS IN DT"
C GIVEN THAT IT IS WORKING AT T".
C
PUNA=PUNA*RBE(IHELP(NC),11)
C
C THE PROBABILITY THAT ALL THE REMAINING BASIC EVENTS IN
C IHELP(20) ARE DOWN AT T".
C
DO 3190 NCP=1,20
IF(NCP.EQ.NC) GO TO 3190
IF(IHELP(NCP).EQ.0) GO TO 3190
CALL BASIC2(IHELP(NCP),BEUNAV)
PUNA=PUNA*BEUNAV
3190 CONTINUE
C
C THE PROBABILITY THAT THE SYSTEM IS WORKING AT T".
C
IF(IND03.EQ.1.AND.IND01.EQ.1.AND.NUMRUN(ISYS).GT.3) GO TO 3200
GO TO 3210
3200 CONTINUE
C
C SELECT THE MPS'S WHICH CONTAIN THE BASIC EVENT 'NC'.
C
III=1
DO 30000 LL1=1,NUMMPS(ISYS)
DO 30010 LL2=1,20
IF(JNFORM(ISYS,LL1,LL2).EQ.0) GO TO 30000
IF(JNFORM(ISYS,LL1,LL2).NE.IHELP(NC)) GO TO 30010
C
C THE MPS 'LL1' CONTAINS THE BASIC EVENT 'NC'.
C
C
C IS THE VECTOR MPSVCT(10,20) OVERLOADED?
C
IF(III.GT.10) GO TO 3210
C
C DOES MPS 'LL1' CONTAIN ANY OF THE REMAINING BASIC EVENTS IN
C IHELP(20)?
C
DO 30020 LL4=1,20
IF(LL4.EQ.NC) GO TO 30020
IF(IHELP(LL4).EQ.0) GO TO 30020
DO 30030 LL5=1,20
IF(JNFORM(ISYS,LL1,LL5).EQ.0) GO TO 30020
IF(IHELP(LL4).NE.JNFORM(ISYS,LL1,LL5)) GO TO 30030
C
C THE MPS 'LL1' IS DOWN AT T". SELECT THE NEXT MPS.
C

```

```

GO TO 30000
30030 CONTINUE
30020 CONTINUE
C
C THE MPS 'LL1' DOES NOT CONTAIN ANY OF THE REMAINING BASIC
C EVENTS IN IHELP(20). INSERT MPS 'LL1' IN THE VECTOR
C MPSVCT(10,20) AND DELETE THE BASIC EVENT IHELP(NC).
C
IDUMMY=0
DO 30040 LL6=1,19
IF(JNFORM(1SYS,LL1,LL6).EQ.0) GO TO 30000
IF(IDUMMY.EQ.1) GO TO 30060
IF(JNFORM(1SYS,LL1,LL6).EQ.IHELP(NC)) GO TO 30060
MPSVCT(111,LL6)=JNFORM(1SYS,LL1,LL6)
GO TO 30040
30060 CONTINUE
IDUMMY=1
MPSVCT(111,LL6)=JNFORM(1SYS,LL1,LL6+1)
30040 CONTINUE
111=111+1
GO TO 30000
30010 CONTINUE
30000 CONTINUE
C
C CALL SUBROUTINE "PATHS."
C
CALL PATHS (PROB,111-1)
PUNA=PUNA*PROB
3210 CONTINUE
UNAJNT=UNAJNT+PUNA
3180 CONTINUE
SUM3=SUM3+UNAJNT
3030 CONTINUE
3020 CONTINUE
3010 CONTINUE
3011 CONTINUE
C
C COMPUTE THE SECOND UPPER BOUND ( IT INCLUDES THE FIRST THREE
C SUMMATIONS SUM1, SUM2, AND SUM3 ).
C
1022 CONTINUE
SUM=SUM1-SUM2+SUM3
RETURN
END

```

```

SUBROUTINE PATHS (PROB,NMPS)
COMMON INFORM( 3, 20, 5), JNFORM(3, 20, 20), RBE( 300,12), NDP
COMMON IBE( 300,3), MCSTYP(3, 20), NUMMCS(3), NUMMPS ( 3)
COMMON NUMRUN(3), IHELP(1000), TRUN(3), BASE( 300 )
COMMON MPSVCT(10, 20), ROFVCT(100,2), TFINAL
COMMON TPRIME, DPRIME, FIRST, FINAL, NS
COMMON DELTA1, DELTA2, BOUND , IDELTA
COMMON DELTAP, TDIFF, DELTA, NIM, IND01
COMMON NBE, IND02, IND03, IND04 , IND05
COMMON IND10, IND09, IND08, IND07, IND06
COMMON JDELTA(3), DLTPR (3)
DIMENSION IPATH(200)
DOUBLE PRECISION SUM1, SUM2, SUM3, SUM4, SUM5, SUM6, SUM7
DOUBLE PRECISION PROB, SUM8, SUM9, SUM10

C
C
C      INITIALIZATION OF THE SUMMATIONS

      SUM1=0.0
      SUM2=0.0
      SUM3=0.0
      SUM4=0.0
      SUM5=0.0
      SUM6=0.0
      SUM7=0.0
      SUM8=0.0
      SUM9=0.0
      SUM10=.0

C
C
C      INITIALIZE THE COUNTER IND

      IND=1
      CONTINUE

C
C
C      SELECT THE MINIMAL PATH SETS

DO 100 I1=1 , (NMPS-(IND-1))
IF(IND.EQ.1) GO TO 1100
DO 200 I2=I1+1, (NMPS-(IND-2))
IF(IND.EQ.2) GO TO 2100
DO 300 I3=I2+1, (NMPS-(IND-3))
IF(IND.EQ.3) GO TO 3100
DO 400 I4=I3+1, (NMPS-(IND-4))
IF(IND.EQ.4) GO TO 4100
DO 500 I5=I4+1, (NMPS-(IND-5))
IF(IND.EQ.5) GO TO 5100
DO 600 I6=I5+1, (NMPS-(IND-6))
IF(IND.EQ.6) GO TO 6100
DO 700 I7=I6+1, (NMPS-(IND-7))
IF(IND.EQ.7) GO TO 7100
DO 800 I8=I7+1, (NMPS-(IND-8))
IF(IND.EQ.8) GO TO 8100
DO 900 I9=I8+1, (NMPS-(IND-9))

```

```

      IF(IND.EQ.9) GO TO 9100
      I10=10
C*****
C
C      THE MPS'S TAKEN TEN AT A TIME
C
C*****
C
C      LOAD THE VECTOR IPATH(200).
C
C
C          DO 10200 K=1,20
C              IPATH(K)=MPSVCT(11,K)
C              IPATH(K+20)=MPSVCT(12,K)
C              IPATH(K+40)=MPSVCT(13,K)
C              IPATH(K+60)=MPSVCT(14,K)
C              IPATH(K+80)=MPSVCT(15,K)
C              IPATH(K+100)=MPSVCT(16,K)
C              IPATH(K+120)=MPSVCT(17,K)
C              IPATH(K+140)=MPSVCT(18,K)
C              IPATH(K+160)=MPSVCT(19,K)
C              IPATH(K+180)=MPSVCT(110,K)
10200      CONTINUE
C
C      SET TO ZERO THE REDUNDANT BASIC EVENTS
C
C          DO 10300 L1=1,199
C              IF(IPATH(L1).EQ.0) GO TO 10300
C              DO 10400 L2=L1+1,200
C                  IF(IPATH(L1).NE.IPATH(L2)) GO TO 10400
C                  IPATH(L2)=0
10400      CONTINUE
10300      CONTINUE
C
C      COMPUTE THE AVAILABILITY OF THE INTERSECTION OF MPS'S 11,12,
C      13,14,15,16,17,18,19, AND 110
C
C          AV=1.
C          DO 10500 M1=1,200
C              IF(IPATH(M1).EQ.0) GO TO 10500
C              CALL BASIC2(IPATH(M1),BEUNAV)
C              AV=AV*(1.-BEUNAV)
10500      CONTINUE
C
C      COMPUTE THE TENTH SUMMATION
C
C          SUM10=SUM10+AV
C          GO TO 900
C*****
C
C      THE MPS'S TAKEN NINE AT A TIME
C
C

```

```

C*****
9100  CONTINUE
C
C      LOAD THE VECTOR IPATH(180)
C
C          DO 9200 K=1,20
C              IPATH(K)=MPSVCT(11,K)
C              IPATH(K+20)=MPSVCT(12,K)
C              IPATH(K+40)=MPSVCT(13,K)
C              IPATH(K+60)=MPSVCT(14,K)
C              IPATH(K+80)=MPSVCT(15,K)
C              IPATH(K+100)=MPSVCT(16,K)
C              IPATH(K+120)=MPSVCT(17,K)
C              IPATH(K+140)=MPSVCT(18,K)
C              IPATH(K+160)=MPSVCT(19,K)
9200      CONTINUE
C
C      SET TO ZERO THE REDUNDANT BASIC EVENTS
C
C          DO 9300 L1=1,179
C              IF(IPATH(L1).EQ.0) GO TO 9300
C              DO 9400 L2=L1+1,180
C                  IF(IPATH(L1).NE.IPATH(L2)) GO TO 9400
C                  IPATH(L2)=0
9400      CONTINUE
9300      CONTINUE
C
C      COMPUTE THE AVAILABILITY OF THE INTERSECTION OF MPS'S 11,12,
C      13,14,15,16,17,18, AND 19
C
C          AV=1.
C          DO 9500 M1=1,180
C              IF(IPATH(M1).EQ.0) GO TO 9500
C              CALL BASIC2(IPATH(M1),BEUNAV)
C              AV=AV*(1.-BEUNAV)
9500      CONTINUE
C
C      COMPUTE THE NINTH SUMMATION
C
C          SUM9=SUM9+AV
900      CONTINUE
GO TO 800
C*****
C          *
C      THE MPS'S TAKEN EIGHT AT A TIME          *
C          *
C*****
8100  CONTINUE
C
C      LOAD THE VECTOR IPATH(160)
C

```

```

DO 8200 K=1,20
  IPATH(K)=MPSVCT(11,K)
  IPATH(K+ 20)=MPSVCT(12,K)
  IPATH(K+ 40)=MPSVCT(13,K)
  IPATH(K+ 60)=MPSVCT(14,K)
  IPATH(K+ 80)=MPSVCT(15,K)
  IPATH(K+100)=MPSVCT(16,K)
  IPATH(K+120)=MPSVCT(17,K)
  IPATH(K+140)=MPSVCT(18,K)
8200 CONTINUE
C
C SET TO ZERO THE REDUNDANT BASIC EVENTS
C
      DO 8300 L1=1,159
      IF(IPATH(L1).EQ.0) GO TO 8300
      DO 8400 L2=L1+1,160
      IF(IPATH(L1).NE.IPATH(L2)) GO TO 8400
      IPATH(L2)=0
8400 CONTINUE
8300 CONTINUE
C
C COMPUTE THE AVAILABILITY OF THE INTERSECTION OF MPS'S 11,12,
C 13,14,15,16,17, AND 18.
      AV=1.
      DO 8500 M1=1,160
      IF(IPATH(M1).EQ.0) GO TO 8500
      CALL BASIC2(IPATH(M1),BEUNAV)
      AV=AV*(1.-BEUNAV)
8500 CONTINUE
C
C COMPUTE THE EIGHTH SUMMATION
C
      SUM8=SUM8+AV
800 CONTINUE
GO TO 700
C*****
C
C THE MPS'S TAKEN SEVEN AT A TIME
C
C*****
7100 CONTINUE
C
C LOAD THE VECTOR IPATH(140)
C
      DO 7200 K=1,20
      IPATH(K)=MPSVCT(11,K)
      IPATH(K+ 20)=MPSVCT(12,K)
      IPATH(K+ 40)=MPSVCT(13,K)
      IPATH(K+ 60)=MPSVCT(14,K)
      IPATH(K+ 80)=MPSVCT(15,K)
      IPATH(K+100)=MPSVCT(16,K)
      IPATH(K+120)=MPSVCT(17,K)

```

```

7200                                CONTINUE
C
C      SET TO ZERO THE REDUNDANT BASIC EVENTS
C
C      DO 7300 L1=1,139
C      IF(IPATH(L1).EQ.0) GO TO 7300
C      DO 7400 L2=L1+1,140
C      IF(IPATH(L1).NE.IPATH(L2)) GO TO 7400
C      IPATH(L2)=0
7400                                CONTINUE
7300                                CONTINUE
C
C      COMPUTE THE AVAILABILITY OF THE INTERSECTION OF MPS'S 11,12,
C      13,14,15,16, AND 17.
C
C      AV=1.
C      DO 7500 M1=1,140
C      IF(IPATH(M1).EQ.0) GO TO 7500
C      CALL BASIC2(IPATH(M1),BEUNAV)
C      AV=AV*(1.-BEUNAV)
7500                                CONTINUE
C
C      COMPUTE THE SEVENTH SUMMATION
C
C      SUM7=SUM7+AV
700                                CONTINUE
GO TO 600
C*****
C
C      THE MPS'S TAKEN SIX AT A TIME
C
C*****
6100 CONTINUE
C
C      LOAD THE VECTOR IPATH(120)
C
C      DO 6200 K=1,20
C      IPATH(K)=MPSVCT(11,K)
C      IPATH(K+ 20)=MPSVCT(12,K)
C      IPATH(K+ 40)=MPSVCT(13,K)
C      IPATH(K+ 60)=MPSVCT(14,K)
C      IPATH(K+ 80)=MPSVCT(15,K)
C      IPATH(K+100)=MPSVCT(16,K)
6200                                CONTINUE
C
C      SET TO ZERO THE REDUNDANT BASIC EVENTS
C
C      DO 6300 L1=1,119
C      IF(IPATH(L1).EQ.0) GO TO 6300
C      DO 6400 L2=L1+1,120
C      IF(IPATH(L1).NE.IPATH(L2)) GO TO 6400
C      IPATH(L2)=0

```

```

6400          CONTINUE
6300          CONTINUE
C
C      COMPUTE THE AVAILABILITY OF THE INTERSECTION OF MPS'S 11,12,
C      13,14,15, AND 16.
C
          AV=1.
          DO 6500 M1=1,120
            IF(IPATH(M1).EQ.0) GO TO 6500
            CALL BASIC2(IPATH(M1),BEUNAV)
            AV=AV*(1.-BEUNAV)
6500          CONTINUE
C
C      COMPUTE THE SIXTH SUMMATION
C
          SUM6=SUM6+AV
600          CONTINUE
          GO TO 500
C*****
C      THE MPS'S TAKEN FIVE AT A TIME
C      *
C      *
C*****
5100          CONTINUE
C
C      LOAD THE VECTOR IPATH(100)
C
          DO 5200 K=1,20
            IPATH(K)=MPSVCT(11,K)
            IPATH(K+20)=MPSVCT(12,K)
            IPATH(K+40)=MPSVCT(13,K)
            IPATH(K+60)=MPSVCT(14,K)
            IPATH(K+80)=MPSVCT(15,K)
5200          CONTINUE
C
C      SET TO ZERO THE REDUNDANT BASIC EVENTS
C
          DO 5300 L1=1,99
            IF(IPATH(L1).EQ.0) GO TO 5300
            DO 5400 L2=L1+1,100
              IF(IPATH(L1).NE.IPATH(L2)) GO TO 5400
              IPATH(L2)=0
5400          CONTINUE
5300          CONTINUE
C
C      COMPUTE THE AVAILABILITY OF THE INTERSECTION OF THE MPS'S
C      11,12,13,14, AND 15
C
          AV=1.
          DO 5500 M1=1,100
            IF(IPATH(M1).EQ.0) GO TO 5500
            CALL BASIC2(IPATH(M1),BEUNAV)

```



```

                    AV=AV*(1.-BEUNAV)
5500                CONTINUE
C
C                COMPUTE THE FIFTH SUMMATION
C                SUM5=SUM5+AV
500                CONTINUE
                    GO TO 400
C*****
C                THE MPS'S TAKEN FOUR AT A TIME
C*****
4100              CONTINUE
C
C                LOAD THE VECTOR IPATH(80)
C
C                                DO 4200 K=1,20
C                                IPATH(K)=MPSVCT(11,K)
C                                IPATH(K+20)=MPSVCT(12,K)
C                                IPATH(K+40)=MPSVCT(13,K)
C                                IPATH(K+60)=MPSVCT(14,K)
4200              CONTINUE
C
C                SET TO ZERO THE REDUNDANT BASIC EVENTS
C
C                                DO 4300 L1=1,79
C                                IF(IPATH(L1).EQ.0) GO TO 4300
C                                DO 4400 L2=L1+1,80
C                                IF(IPATH(L1).NE.IPATH(L2)) GO TO 4400
C                                IPATH(L2)=0
4400              CONTINUE
4300              CONTINUE
C
C                COMPUTE THE AVAILABILITY OF THE INTERSECTION OF THE MPS'S
C                11,12,13, AND 14
C
C                                AV=1.
C                                DO 4500 M1=1,80
C                                IF(IPATH(M1).EQ.0) GO TO 4500
C                                CALL BASIC2(IPATH(M1),BEUNAV)
C                                AV=AV*(1.-BEUNAV)
4500              CONTINUE
C
C                COMPUTE THE FOURTH SUMMATION
C
C                SUM4=SUM4+AV
400              CONTINUE
                    GO TO 300

```

```

C*****
C
C      THE MPS'S TAKEN THREE AT A TIME
C
C*****
3100  CONTINUE
C
C      LOAD THE VECTOR IPATH(60)
C
C          DO 3200 K=1,20
C          IPATH(K)=MPSVCT(11,K)
C          IPATH(K+ 20)=MPSVCT(12,K)
C          IPATH(K+ 40)=MPSVCT(13,K)
3200  CONTINUE
C
C      SET TO ZERO THE REDUNDANT BASIC EVENTS
C
C          DO 3300 L1=1,59
C          IF(IPATH(L1).EQ.0) GO TO 3300
C          DO 3400 L2=L1+1,60
C          IF(IPATH(L1).NE.IPATH(L2)) GO TO 3400
C          IPATH(L2)=0
3400  CONTINUE
3300  CONTINUE
C
C      COMPUTE THE AVAILABILITY OF THE INTERSECTION OF THE MPS'S
C      11,12, AND 13.
C
C          AV=1.
C          DO 3500 M1=1,60
C          IF(IPATH(M1).EQ.0) GO TO 3500
C          CALL BASIC2(IPATH(M1),BEUNAV)
C          AV=AV*(1.-BEUNAV)
3500  CONTINUE
C
C      COMPUTE THE THIRD SUMMATION
C
C          SUM3=SUM3+AV
300  CONTINUE
GO TO 200
C*****
C
C      THE MPS'S TAKEN TWO AT A TIME
C
C*****
2100  CONTINUE
C
C      LOAD THE VECTOR IPATH(40)
C
C          DO 2200 K=1,20
C          IPATH(K)=MPSVCT(11,K)
C          IPATH(K+ 20)=MPSVCT(12,K)

```

```

2200                                CONTINUE
C
C      SET TO ZERO THE REDUNDANT BASIC EVENTS
C
          DO 2300 L1=1,39
          IF(IPATH(L1).EQ.0) GO TO 2400
          DO 2500 L2=21,40
          IF(IPATH(L2).EQ.0) GO TO 2300
          IF(IPATH(L1).NE.IPATH(L2)) GO TO 2500
          IPATH(L2)=0
2500                                CONTINUE
2300                                CONTINUE
2400      CONTINUE
C
C      COMPUTE THE AVAILABILITY OF THE INTERSECTION OF THE MPS'S
C      I1 AND I2.
C
          AV=1.
          DO 2600 M1=1,40
          IF(IPATH(M1).EQ.0) GO TO 2600
          CALL BASIC2(IPATH(M1),BEUNAV)
          AV=AV*(1.-BEUNAV)
2600                                CONTINUE
C
C      COMPUTE THE SECOND SUMMATION
C
          SUM2=SUM2+AV
200      CONTINUE
          GO TO 100
C*****
C
C      THE MPS'S TAKEN ONE AT A TIME
C
C*****
1100      CONTINUE
C
C      LOAD THE VECTOR IPATH(20)
C
          DO 1200 K=1,20
          IF(MPSVCT(I1,K).EQ.0) GO TO 1300
          IPATH(K)=MPSVCT(I1,K)
1200                                CONTINUE
1300                                CONTINUE
C
C      COMPUTE THE AVAILABILITY OF THE MPS I1
C
          AV=1.
          DO 1400 M1=1,20
          IF(IPATH(M1).EQ.0) GO TO 1500
          CALL BASIC2(IPATH(M1),BEUNAV)
          AV=AV*(1.-BEUNAV)

```

```

1400             CONTINUE
1500             CONTINUE
C
C      COMPUTE THE FIRST SUMMATION
C
      SUM1=SUM1+AV
100    CONTINUE
      IND=IND+1
      IF(IND.LE.NMPS) GO TO 10
C
C      COMPUTE THE PROBABILITY THAT THE SYSTEM IS WORKING AT T" GIVEN
C      THAT THE BASIC EVENT K CAUSES A SYSTEM FAILURE IN DT".
C
      PROB=SUM1-SUM2+SUM3-SUM4+SUM5-SUM6+SUM7-SUM8+SUM9-SUM10
      IF(PROB.GT.1.)          GO TO 101
      RETURN
101    CONTINUE
      WRITE(21,1000) TPRIME,TDIFF
      WRITE(21,1010) PROB
      PROB=1.
      RETURN
1000   FORMAT('1THE PROBABILITY THAT THE SYSTEM IS UP HAS EXCEEDED THE
1      LIMIT 1. ( TPRIME=',F10.3,' AND TDIFF=',F10.5)
1010   FORMAT('0THE PROBABILITY THAT THE SYSTEM IS UP AT THE GIVEN TIME
1S IS ',E10.5)
      END

```

```

SUBROUTINE CUTS (ISYS,SUM)
COMMON  INFORM( 3, 20, 5), JNFORM(3, 20, 20), RBE( 300,12), NDP
COMMON  IBE( 300,3), MCSTYP(3, 20), NUMMCS(3), NUMMPS ( 3)
COMMON  NUMRUN(3), IHELP(1000), TRUN(3), BASE( 300 )
COMMON  MPSVCT(10, 20), ROFVCT(100,2), TFINAL
COMMON  TPRIME, DPRIME, FIRST, FINAL, NS
COMMON  DELTA1, DELTA2, BOUND , IDELTA
COMMON  DELTAP, TDIFF, DELTA, NIM, IND01
COMMON  NBE, IND02, IND03, IND04 , IND05
COMMON  IND10, IND09, IND08, IND07,IND06
COMMON  JDELTA(3), DLTPR (3)

C
C      INITIALIZE THE SUMMATIONS.
C
      SUM1=0.0
      SUM2=0.0
      SUM3=0.0
      SUM4=0.0
      SUM5=0.0

C
C
C*****
C      'NUMMCS(ISYS)' MCS'S TAKEN ONE AT A TIME
C
C*****
      DO 120 J=1,NUMMCS(ISYS)
        UNAMCS=1.
        DO 130 K=1,5
          IF(INFORM(ISYS,J,K).EQ.0) GO TO 140
          UNAMCS=UNAMCS*BASE( INFORM( ISYS,J,K))
130      CONTINUE
140      CONTINUE
77770  IF((TPRIME+.001).NE.8038.) GO TO 77770
        CONTINUE
        SUM1=SUM1+UNAMCS
120    CONTINUE
C
C      FIRST UPPER BOUND
C
      SUM=SUM1
      IF(NUMMCS(ISYS).EQ.1)
C
C      ARE THE SECOND AND THIRD SUMMATIONS REQUESTED?
C
        IF(IND02.EQ.1) GO TO 150
        GO TO 251
C
C      ARE THE SECOND AND THIRD SUMMATIONS FEASIBLE?
C
150    CONTINUE
        IF(NUMMCS(ISYS).LE.20)
C
C      GO TO 160
        GO TO 251

```

```

C*****
C
C      'NUMMCS(ISYS)' MCS'S TAKEN TWO AT A TIME
C
C*****
160  CONTINUE
C
C      SELECT THE MCS'S 'I1' AND 'I2'.
C
      DO 170 I1=1,NUMMCS(ISYS)-1
      DO 180 I2=I1+1,NUMMCS(ISYS)
C
C
C          LOAD THE VECTOR IHELP(10).
C
C          DO 190 I3=1,5
C          IHELP(I3)=INFORM(ISYS,I1,I3)
C          IHELP(I3+5)=INFORM(ISYS,I2,I3)
C          CONTINUE
190
C
C      SET TO ZERO THE REDUNDANT BASIC EVENTS
C
      DO 200 J1=1,5
      DO 210 J2=6,10
      IF(IHELP(J1).EQ.0) GO TO 220
      IF(IHELP(J1).NE.IHELP(J2)) GO TO 210
      IHELP(J2)=0
210      CONTINUE
200      CONTINUE
220      CONTINUE
C
C      COMPUTE THE UNAVAILABILITY OF THE INTERSECTION OF MCS'S I1
C      AND I2 -- UNAINT
C
      UNAINT=1.
      DO 230 L1=1,10
      IF(IHELP(L1).EQ.0) GO TO 230
      UNAINT=UNAINT*BASE(IHELP(L1))
230      CONTINUE
      IF((TPRIME+.001).NE.8038.) GO TO 77771
77771  CONTINUE
C
C      COMPUTE THE UNAVAILABILITY OF THE INTERSECTION OF THE MCS'S
C      TAKEN TWO AT A TIME.
C
      SUM2=SUM2+UNAINT
180  CONTINUE
170  CONTINUE
      IF(NUMMCS(ISYS).NE.2)
      SUM=SUM1-SUM2
      GO TO 251
      GO TO 171
171  CONTINUE

```

```

C
C      IS THE THIRD SUMMATION NECESSARY?
C
      IF(SUM1.NE.SUM2)                                GO TO 239
      BOUNDP=100.0
      GO TO 238
239    CONTINUE
      BOUNDP=(SUM2/(SUM1-SUM2))*100.
238    CONTINUE
      IF((BOUNDP.GT.BOUND).AND.(BOUNDP.GT.0.))        GO TO 240
      GO TO 251
C*****
C      'NUMMCS(ISYS)' MCS'S TAKEN THREE AT A TIME      *
C      *
C      *
C*****
240    CONTINUE
C
C      SELECT THE MCS'S 'M1', 'M2', AND 'M3'.
C
      DO 250 M1=1,NUMMCS( ISYS)-2
      DO 260 M2=M1+1,NUMMCS( ISYS)-1
      DO 270 M3=M2+1,NUMMCS( ISYS)
C
C
C      LOAD THE VECTOR IHELP(15).
C
      DO 280 M4=1,5
      IHELP(M4)=INFORM( ISYS,M1,M4)
      IHELP(M4+5)=INFORM( ISYS,M2,M4)
      IHELP(M4+10)=INFORM( ISYS,M3,M4)
280    CONTINUE
C
C      SET TO ZERO THE REDUNDANT BASIC EVENTS
C
      DO 290 N1=1,5
      IF(IHELP(N1).EQ.0) GO TO 310
      DO 300 N2=6,15
      IF(IHELP(N1).NE.IHELP(N2)) GO TO 300
      IHELP(N2)=0
300    CONTINUE
290    CONTINUE
310    CONTINUE
      DO 320 N3=6,10
      DO 330 N4=11,15
      IF(IHELP(N3).NE.IHELP(N4)) GO TO 330
      IHELP(N4)=0
330    CONTINUE
320    CONTINUE
C
C      COMPUTE THE UNAVAILABILITY OF THE INTERSECTION OF MCS'S
C      M1,M2, AND M3 -- UNAINIT
C

```

```

        UNAINT=1.
        DO 350 N5=1,15
        IF(IHELP(N5).EQ.0) GO TO 350
        UNAINT=UNAINT*BASE(IHELP(N5))
350      CONTINUE
        IF((TPRIME).NE.8038.) GO TO 77772
77772    CONTINUE
C
C      COMPUTE THE UNAVAILABILITY OF THE INTERSECTION OF THE MCS'S
C      TAKEN THREE AT A TIME.
C
        SUM3=SUM3+UNAINT
270      CONTINUE
260      CONTINUE
250      CONTINUE
251      CONTINUE
C
C      SECOND UPPER BOUND ( THIRD SUMMATION )
C
        SUM=SUM1-SUM2+SUM3
        RETURN
        END

```



```

SUBROUTINE ROFIE(ROF)

C
C
C      THIS SUBROUTINE COMPUTES THE RATE OF FAILURE OF THE
C      INITIATING EVENT AS A FUNCTION OF TIME. IT PERFORMS A LINEAR
C      INTERPOLATION BETWEEN THE DATA POINTS PROVIDED. THE NOTATION
C      USED IN THIS SUBROUTINE IS AS FOLLOWS:
C
C      ROFVCT(I,J)  THIS VECTOR STORES THE MAGNITUDE OF
C                   THE RATE OF FAILURE OF THE
C                   INITIATING EVENT IN (1/HR.) AS A
C
C      I - DATA POINT IDENTIFICATION.
C
C      J - =1 TIME, HRS.
C          =2 MAGNITUDE OF THE ROF (T).
C              IE
C
C      DUMMY1,      THESE ARE AUXILIARY VARIABLES USED TO
C      DUMMY2,AND    PERFORM INTERMEDIATE CALCULATIONS.
C      DYMM3
C
COMMON  INFORM( 3, 20, 5), JNFORM(3, 20, 20), RBE( 300,12), NDP
COMMON  IBE( 300,3), MCSTYP(3, 20), NUMMCS(3), NUMMPS ( 3)
COMMON  NUMRUN(3), IHELP(1000), TRUN(3), BASE( 300 )
COMMON  MPSVCT(10, 20), ROFVCT(100,2), TFINAL
COMMON  TPRIME, DPRIME, FIRST, FINAL, NS
COMMON  DELTA1, DELTA2, BOUND , IDELTA
COMMON  DELTAP, TDIFF, DELTA, NIM, IND01
COMMON  NBE, IND02, IND03, IND04 , IND05
COMMON  IND10, IND09, IND08, IND07,IND06
COMMON  JDELTA(3),      DLTPR (3)

C
C*****
C      SELECT THE TIME INTERVAL WHICH CONTAINS T'
C*****
DO 10000 I=1,100
      IF(ROFVCT(I,1).EQ.TPRIME)          GO TO 20000
      IF(ROFVCT(I,1).GT.TPRIME)          GO TO 30000
10000 CONTINUE

```

```

C*****
C
C      THE VALUE OF 'ROF' IS AVAILABLE AT T'.
C
C      NO INTERPOLATION IS REQUIRED.
C
C*****
20000  CONTINUE
      ROF=ROFVCT(1,2)
      RETURN
C*****
C
C      THE VALUE OF 'ROF' IS NOT AVAILABLE AT T'.  A LINEAR
C
C      INTERPOLATION WILL BE USED TO ESTIMATE 'ROF(TPRIME)'.
C
C*****
30000  CONTINUE
      DUMMY1= ROFVCT (1,2) - ROFVCT(1-1,2)
      DUMMY2= ROFVCT (1,1) - TPRIME
      DUMMY3= ROFVCT (1,1) - ROFVCT(1-1,1)
      ROF = ROFVCT (1,2) - DUMMY1 * DUMMY2 / DUMMY3
      RETURN
      END

```

```

C*****
C
C      F U N C T I O N           S U B R O U T I N E S
C
C*****
C
C      FUNCTION FNRA(X1,X2,X3)
C
C      THIS FUNCTION COMPUTES THE UNAVAILABILITY UPPER BOUND
C      APPLICABLE TO NONREPAIRABLE BASIC EVENTS.
C
C      THE NOTATION USED HERE IS THE FOLLOWING:
C
C          X1 -- HAZARD RATE,  $HR^{-1}$ .
C          X2 -- TIME, HR.
C          X3 -- UNAVAILABILITY PER DEMAND, RBE(1,10).
C
C      FNRA=X1*X2
C      FNRA=FNRA+(1.-FNRA)*X3
C      RETURN
C      END
C
C
C      FUNCTION FNRE(X1,X2,X3)
C
C      THIS FUNCTION COMPUTES THE EXACT VALUE OF THE BASIC EVENT
C      UNAVAILABILITY FOR NONREPAIRABLE BASIC EVENTS.
C
C      THE NOTATION USED HERE IS THE FOLLOWING:
C
C          X1 -- HAZARD RATE,  $HR^{-1}$ .
C          X2 -- TIME INTERVAL,  $(T''-T')$ , HR.
C          X3 -- UNAVAILABILITY AT  $T'$ .
C
C      DUMMY1=1.-X3
C      DUMMY2=EXP(-X1*X2)
C      FNRE=1.-DUMMY1*DUMMY2
C      RETURN
C      END
C
C
C      FUNCTION FCMA(X1,X2,X3)

```

```

C
C
C      THIS FUNCTION COMPUTES THE UNAVAILABILITY UPPER BOUND
C      APPLICABLE TO CONSTANTLY MONITORED BASIC EVENTS.
C
C      THE NOTATION USED HERE IS THE FOLLOWING:
C
C          X1  -- HAZARD RATE,  $HR^{-1}$ .
C          X2  -- THE AVERAGE TIME TO REPAIR, HR.
C          X3  -- UNAVAILABILITY PER DEMAND,  $RBE(1,10)$ .
C
C      FCMA=X1*X2
C      FCMA=FCMA+(1.-FCMA)*X3
C      RETURN
C      END
C
C
C      FUNCTION FCME(X1,X2,X3,X4)
C
C      THIS FUNCTION COMPUTES THE UNAVAILABILITY OF CONSTANTLY
C      MONITORED BASIC EVENTS.
C
C      THE NOTATION USED HERE IS THE FOLLOWING:
C
C          X1  -- HAZARD RATE,  $HR^{-1}$ .
C          X2  -- THE AVERAGE TIME TO REPAIR, HR.
C          X3  -- TIME INTERVAL,  $(T''-T')$ , HR.
C          X4  -- UNAVAILABILITY AT  $T'$ .
C
C      DUMMY1=(X1+1./X2)
C      DUMMY2=X1/DUMMY1
C      DUMMY3=EXP(-DUMMY1*X3)
C      FCME=DUMMY2+(X4-DUMMY2)*DUMMY3
C      RETURN
C      END
C
C
C      FUNCTION FPTA(X1,X2,X3,X4,X5,X6,X7,X8,X9,X10,X11)
C
C      THIS FUNCTION COMPUTES AN APPROXIMATION TO THE UNAVAILABILITY
C      OF PERIODICALLY TESTED BASIC EVENTS.

```



```

15010 CONTINUE
      IF(INDIC1.EQ.0) GO TO 15030
      Q=HAZ1*(X2-X4)
      GO TO 15040
15030 CONTINUE
      Q=HAZ1*X3
15040 CONTINUE
      FPTA=X7+(1.-X7)*X6+(1.-X7)*(1.-X6)*Q
      FPTA=FPTA+(1.-FPTA)*HAZ2*X11
      FPTA=FPTA+(1.-FPTA)*X10
      RETURN
C
C      BASIC EVENT UNDERGOING REPAIR
C
15020 CONTINUE
      IF(INDIC1.EQ.0) GO TO 15050
      Q=HAZ1*(X2-X4)
      GO TO 15060
15050 CONTINUE
      Q=HAZ1*X3
15060 CONTINUE
      FPTA=X7+(1.-X7)*Q+(1.-X7)*(1.-Q)*.5*HAZ1*X5
      FPTA=FPTA+(1.-FPTA)*HAZ2*X11
      FPTA=FPTA+(1.-FPTA)*X10
      RETURN
      END

```

VITA

Henrique Martini Paula was born in the city of Campinas, Brazil on June 17, 1956. He is the son of the late Camilo Marques Paula and Esmeralda Martini Paula. He attended elementary and high schools in the city of Indaiatuba, Brazil.

Henrique had his college education at the "Instituto Nacional de Telecomunicações (INATEL)," from which he graduated with a major in Electrical Engineering in December 1977. He entered the graduate program in Nuclear Engineering at the "Universidade de São Paulo" in March 1978 and received a Master of Science degree in November 1979. During the year of 1979, Henrique has also worked at the "Instituto de Pesquisas Energéticas e Nucleares" in the city of São Paulo, Brazil.

Henrique married Célia Maria on December 1, 1979 and moved to Knoxville, Tennessee. He entered the graduate program in Nuclear Engineering at The University of Tennessee, Knoxville on January 4, 1980. He has recently joined JBF Associates, Inc. of Knoxville, Tennessee, as a research engineer. After receiving the Doctor of Philosophy degree in 1984, Henrique will continue his work in the field of Nuclear Systems Reliability and Risk.